

NATIONAL BUREAU OF STANDARDS REPORT

6190

**Current-Intensity, Voltage-Intensity, and Current-Voltage
of Airfield Lighting Lamps**

By
**Photometry and Colorimetry Section
Optics and Metrology Division**



**U. S. DEPARTMENT OF COMMERCE
NATIONAL BUREAU OF STANDARDS**

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October 1958

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Prepared For
Ship Installations Division
Bureau of Aeronautics
Department of the Navy
and
Aeronautical Accessories Laboratory
Wright Air Development Center
Department of the Air Force

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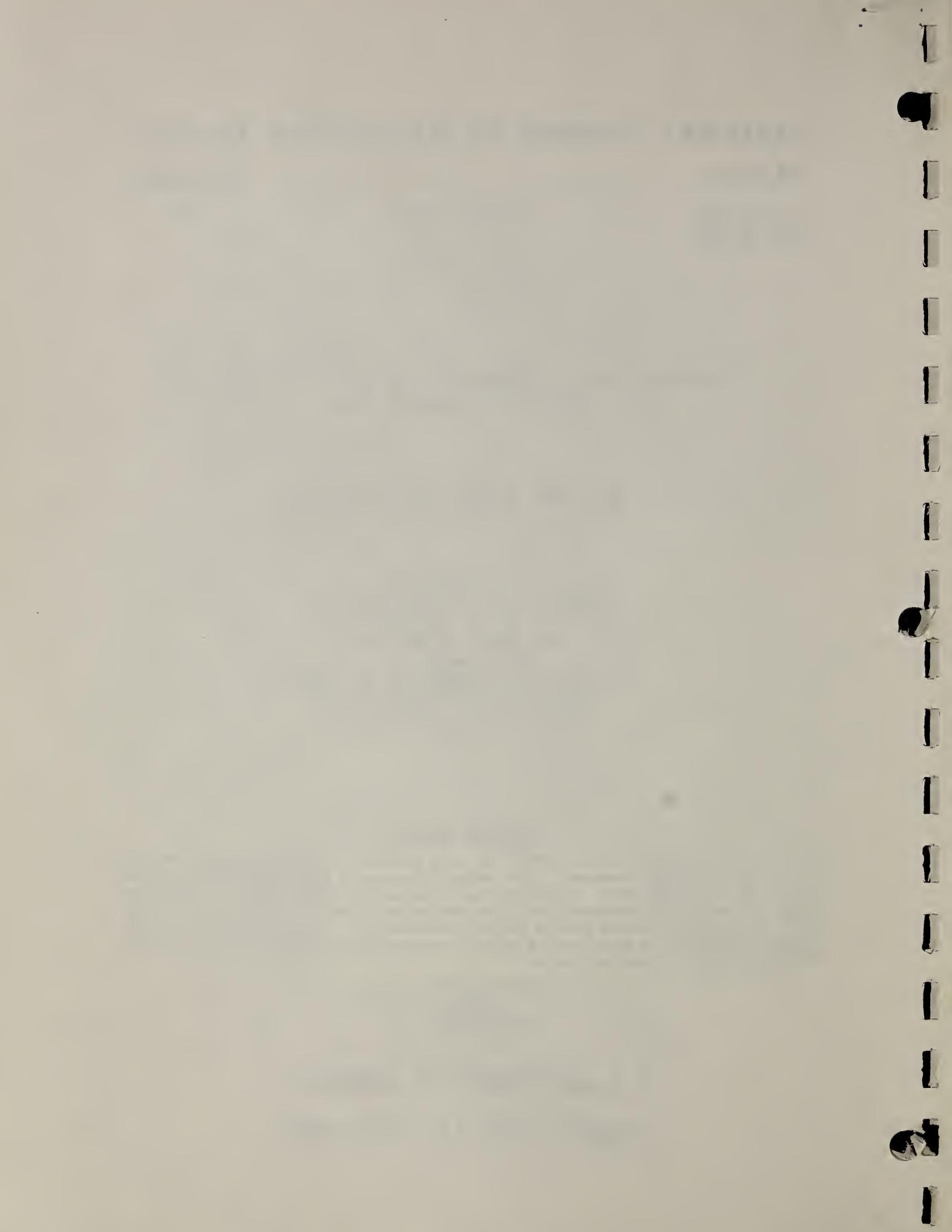
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Current-Intensity, Voltage-Intensity, and Current-Voltage Characteristics
of
Airfield Lighting Lamps

SUMMARY

This report is an expansion of National Bureau of Standards Report 4463 and contains a compilation of measurements of the intensity-current-voltage characteristics of lamps of the types generally used in approach-, runway-, and taxiway-light systems. The results of a study of the effects of color filters on the relative intensity of the lamps are included. This report includes all data given in NBS Report 4463 in addition to the data obtained subsequent to the preparation of that report.

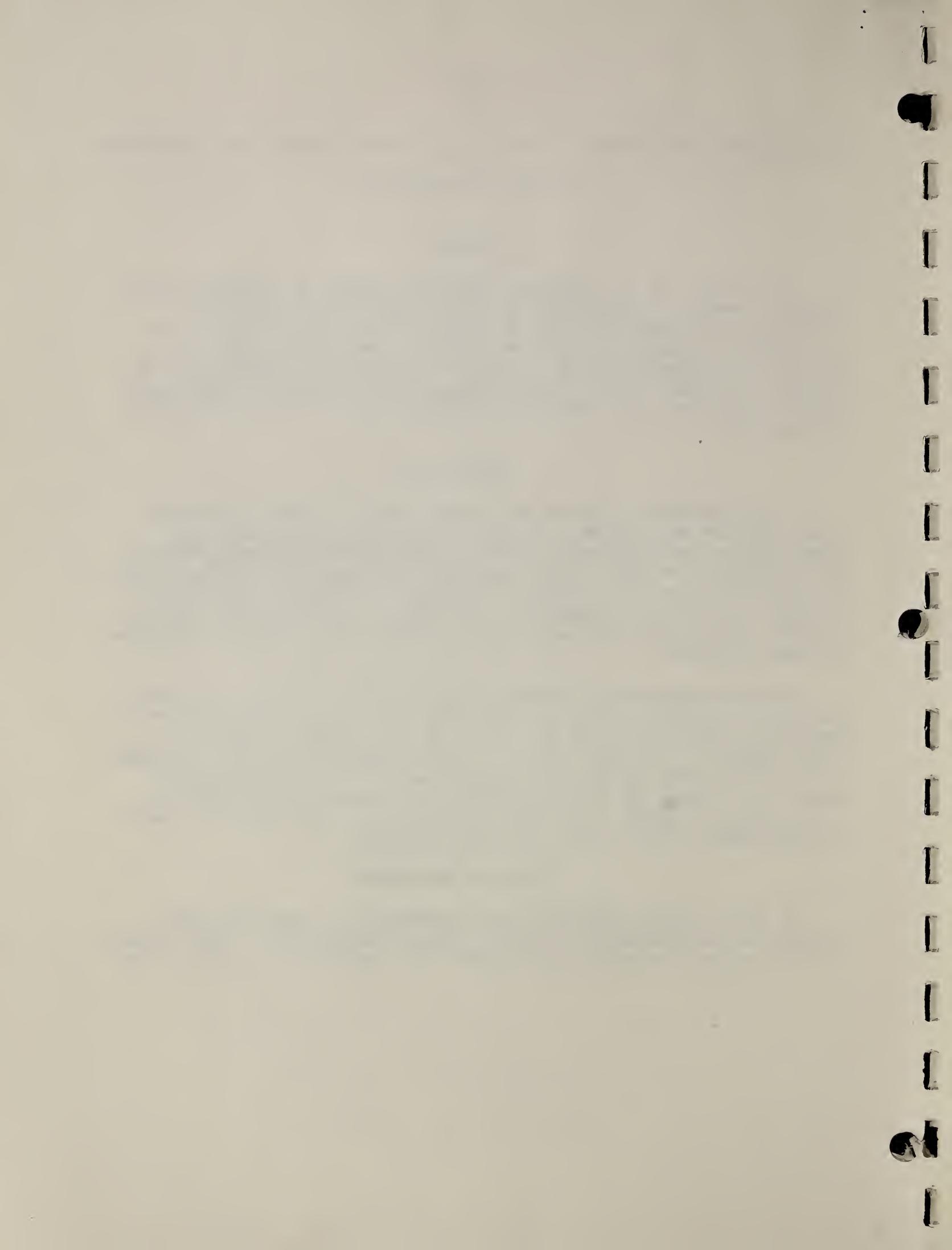
1. INTRODUCTION

Intensity control is now used on nearly all runway- and approach-light systems and on some taxiway-light systems. The increasing complexity of the problems of intensity control has increased the need for information on the relative intensity characteristics of lamps used in approach, runway, and taxiway lighting as a function of the applied current or voltage. In addition, information on the effect of color filters upon the relative intensity is needed. This report was prepared to meet this need.

Relative intensity is defined as the ratio, in percent, of the intensity of a lighting unit or lamp operated at a given current or voltage to the intensity of the same lighting unit or lamp operated at rated current or voltage. Note that in obtaining the relative intensity of a colored light, measurements of the intensity at both the given current or voltage and the rated current or voltage are made with the color filter in place. Thus, the transmittance of the filter has only a second-order effect on the relative intensity.

2. METHOD OF MEASUREMENT

A color-corrected barrier-layer photocell in a zero-resistance circuit was used in making relative intensity measurements. The response of this photometric system was checked. No significant deviations from



linearity were found. When reflector-type lamps were tested, the peak of the beam was directed at the photocell. The relative intensities of lamps other than the reflector type (325-lumen; 200-watt, T-14; etc.) were obtained by measuring the relative horizontal intensity in a given direction. Previous tests have shown that the relative intensity of the clear units in which these lamps are used does not differ significantly from the relative horizontal intensity of the lamps used. Voltage and current measurements were corrected for losses in the measuring circuits. Whenever possible several lamps of a given type were used, and the results of measurements of individual lamps were averaged.

3. LAMP CHARACTERISTICS

The characteristics of each lamp are given as three curves: a, relative intensity-current; b, relative intensity-voltage; and c, voltage-current. Curves for lamps with similar characteristics have been grouped on the same figures. In addition, relative intensity-voltage characteristics of all 25- and 12.5-volt lamps, the relative intensity-current characteristics of all 20- and 10-ampere lamps and of all 6.6-ampere lamps have been grouped. The lamp types studied and the figures showing their characteristics are listed in table I.

Differences in relative intensity between lamps of the same type may become large when the relative intensity becomes less than 1%. The relative intensities may differ by as much as a factor of 2 when the relative intensity is about 0.2%.

4. EFFECTS OF COLOR FILTERS

Because the transmittance of color filters is a function of the color temperature of the source, the relative intensity characteristics of colored lights will differ from those of similar lights which are "white." The determination and presentation of the relative intensity characteristics of each type of lamp for each aviation color would be unduly expensive. Therefore a study has been made to determine representative correction curves. Relative intensity characteristics were determined for several of the types of lamps listed in Table I in combination with filters representative of the limits of the aviation colors. It was found that the data were adequately represented by the lines plotted on figure 22. These lines show the relative intensity of lights meeting the specification requirements for aviation colors as a function of the relative intensity of the same light used without a filter. The lines are

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Table 1

Lamp Type	Designation	Filament	Type	Figure
100-watt, 4.17-ampere, sealed reflector, elevated runway light	7656 F/01	C-6	c	la, b, c
35-watt, 5.83-ampere, sealed reflector, aerodrome light	6298 X/01	CC-6	c	2a, b, c
325-lumen, 6.6-ampere, airport marker	325/6.6/A21	C-8	c	3a, b, c
1020-lumen, 6.6-ampere, airport marker	1020/6.6/A21	C-8	c	3a, b, c
30-watt, 6.6-ampere, T-10, runway, medium intensity	6.6A/T10/1P	C-2V	c	3a, b, c
45-watt, 6.6-ampere, T-10, runway, medium intensity	6.6/T10P	C-2V	c	3a, b, c
45-watt, 6.6-ampere, PAR38, airport flood	45PAR38/6.6	C-6	c	3a, b, c
200-watt, 6.6-ampere, T-14, runway, high intensity	6.6A/T14P	C-13	c	4a, b, c
200-watt, 6.6-ampere, PAR46, special	-----	CC-6	c	4a, b, c
200-watt, 6.6-ampere, PAR56, airport approach, high intensity	6.6A/PAR56/2	C-13	c	4a, b, c
500-watt, 6.6-ampere, T-20, runway, high intensity	6.6A/T20P	C-13D	c	5a, b, c
250-watt, 10-ampere, T-14, airport marker	-----	C-13	c	6a, b, c
100-watt, 20-ampere, PAR36, flush approach and runway transmissometer	20A/PAR36	C-6	c	7a, b, c
120-watt, 20-ampere, PAR64, transmissometer	120PAR	C-6	c	8a, b, c
300-watt, 20-ampere, PAR56, airport approach, high intensity	20A/PAR56	C-6	c	9a, b, c
500-watt, 20-ampere, T-20, runway threshold, high intensity	20A/T20/5	C-13	c	10a, b, c
500-watt, 20-ampere, PAR56, seadrome, pile mounted	20A/PAR56/1	C-6	c	10a, b, c
500-watt, 20-ampere, T-24, seadrome, buoy mounted	20A/T24/3	C-8	c	10a, b, c
A11 6.6-ampere lamps	-----	---	---	11
A11 20-ampere and 10-ampere lamps	-----	12	---	12
50-watt, 6-volt, PAR36, marine light	4588	C-6	c	13a, b, c
75-watt, 30-volt, PAR38, floodlight	75PAR/FL	C-6	c	14a, b, c
75-watt, 75-volt, PAR38, floodlight	75PAR/FL	CC-6	d	14a, b, d
100-watt, 6.5-volt, PAR36, marine light	4586	C-6	c	15a, b, c
100-watt, 12.5-volt, PAR56, marine searchlight	4545	C-6	c	16a, b, c
100-watt, 13-volt, PAR36, marine light	4519	C-6	c	16a, b, c
200-watt, 30-volt, PAR56, locomotive headlight	200PAR	C-13	c	17a, b, c
200-watt, 30-volt, PAR56, locomotive headlight	200PAR	CC-8	c	17a, b, c
250-watt, 12.5-volt, T-10, airport approach	20A/T10/P	C-8	c	18a, b, c
250-watt, 12.5-volt, PAR56, airport approach	250PAR	C-6	c	18a, b, c
300-watt, 25-volt, PAR56, airport approach	300PAR56	C-13	c	19a, b, c
350-watt, 25-volt, PAR56, airport approach	350PAR	C-13	c	19a, b, c
399-watt, 115-volt, PAR56, airport approach	399PAR	CC-13	c	20a, b, c
500-watt, 120-volt, T-20, airport approach	500T20/25	C-13	c	20a, b, c
All 25-volt and 12.5-volt lamps	-----	21	---	21

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representative of "average" filters. The relative intensity of lights with filters near the specification limits may differ from that indicated by the lines by about ten percent at the lowest relative intensities shown. The difference will, of course, be less at higher relative intensities.

5. DISCUSSION

Differences in the change of relative intensity with change in current or voltage for different lamps are significantly large so that generalized lamp-characteristic exponents cannot be satisfactorily used for all lamp types when the relative intensity is varied over a wide range.

For series lamps with the same rated current and of similar design wattage (within 25%), the relative intensity-current characteristics are similar. See the curves on figures 11 and 12. The data shown on figure 21 indicate that relative intensity-voltage characteristics are similar for multiple lamps of similar design wattage.

The data shown in figures 18a, 18b, and 18c indicate that the characteristics of reflector-type lamps are not significantly different from those of other lamp types of the same rated wattage and voltage or current.

November 1958

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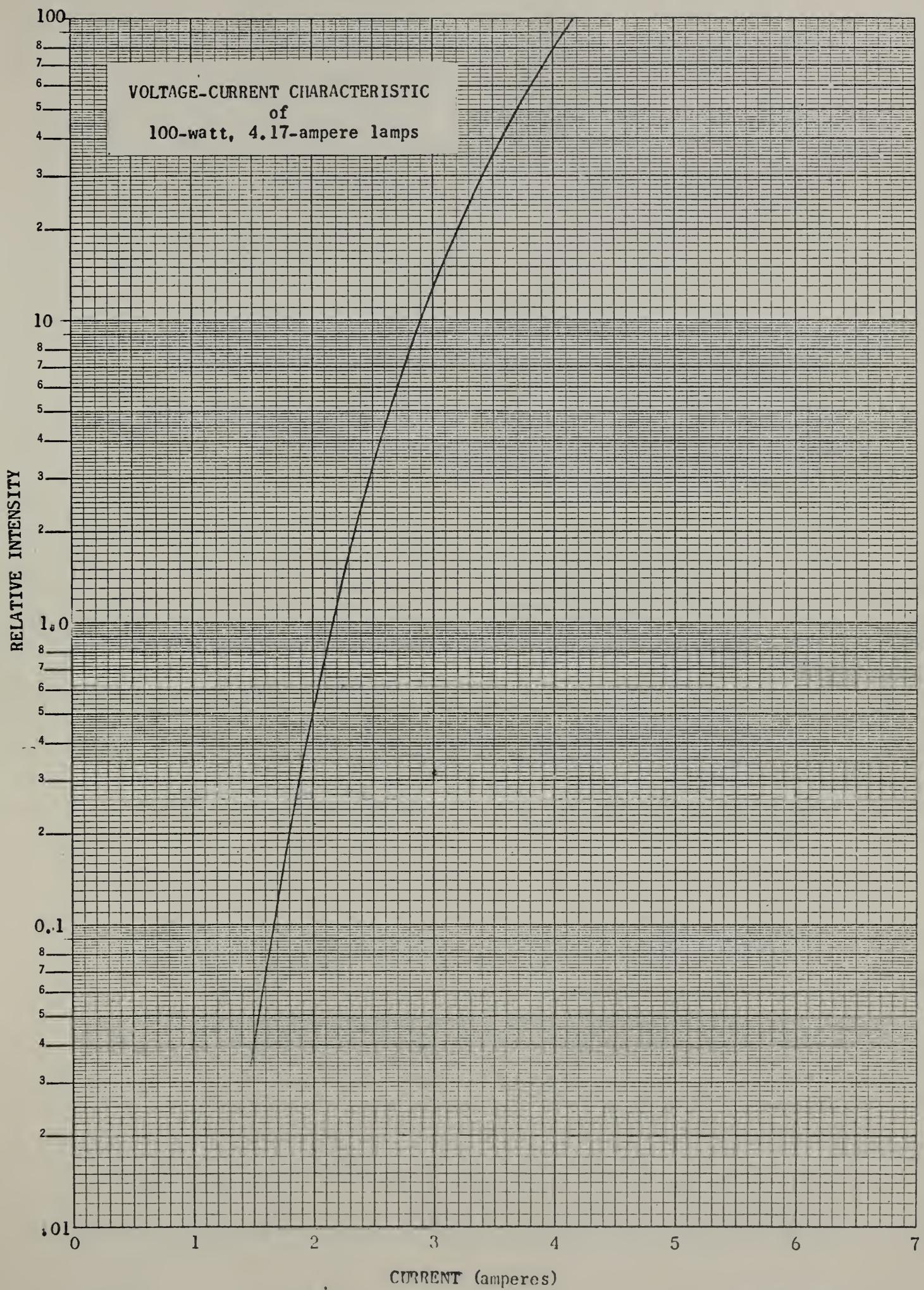


Figure 1a

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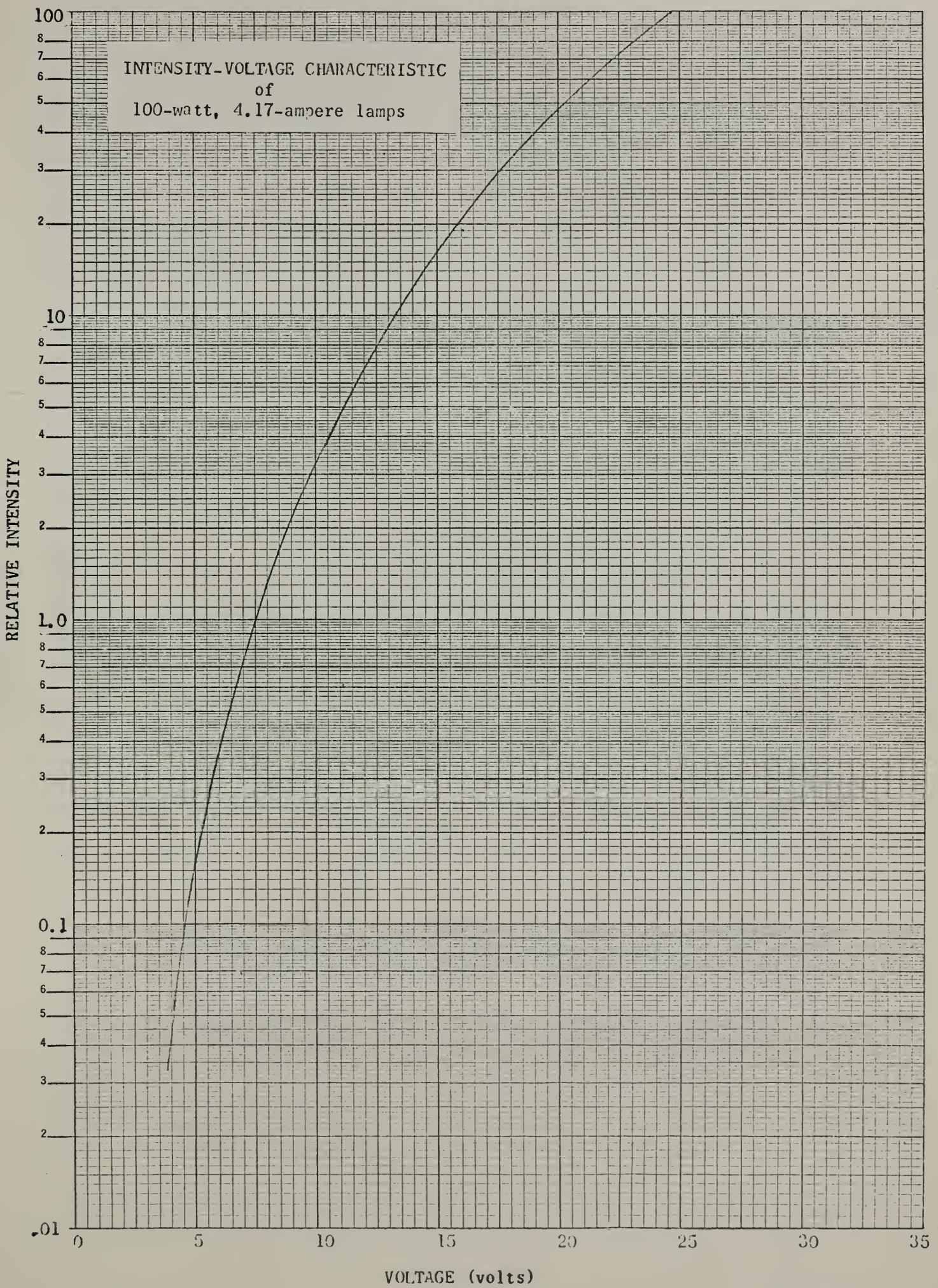


Figure 1b

8

VOLTAGE-CURRENT CHARACTERISTIC
of
100-watt, 4.17-ampere lamps

VOLTAGE (volts)

28

24

20

16

12

8

4

0

1

2

3

4

5

CURRENT (amperes)

Figure 1c

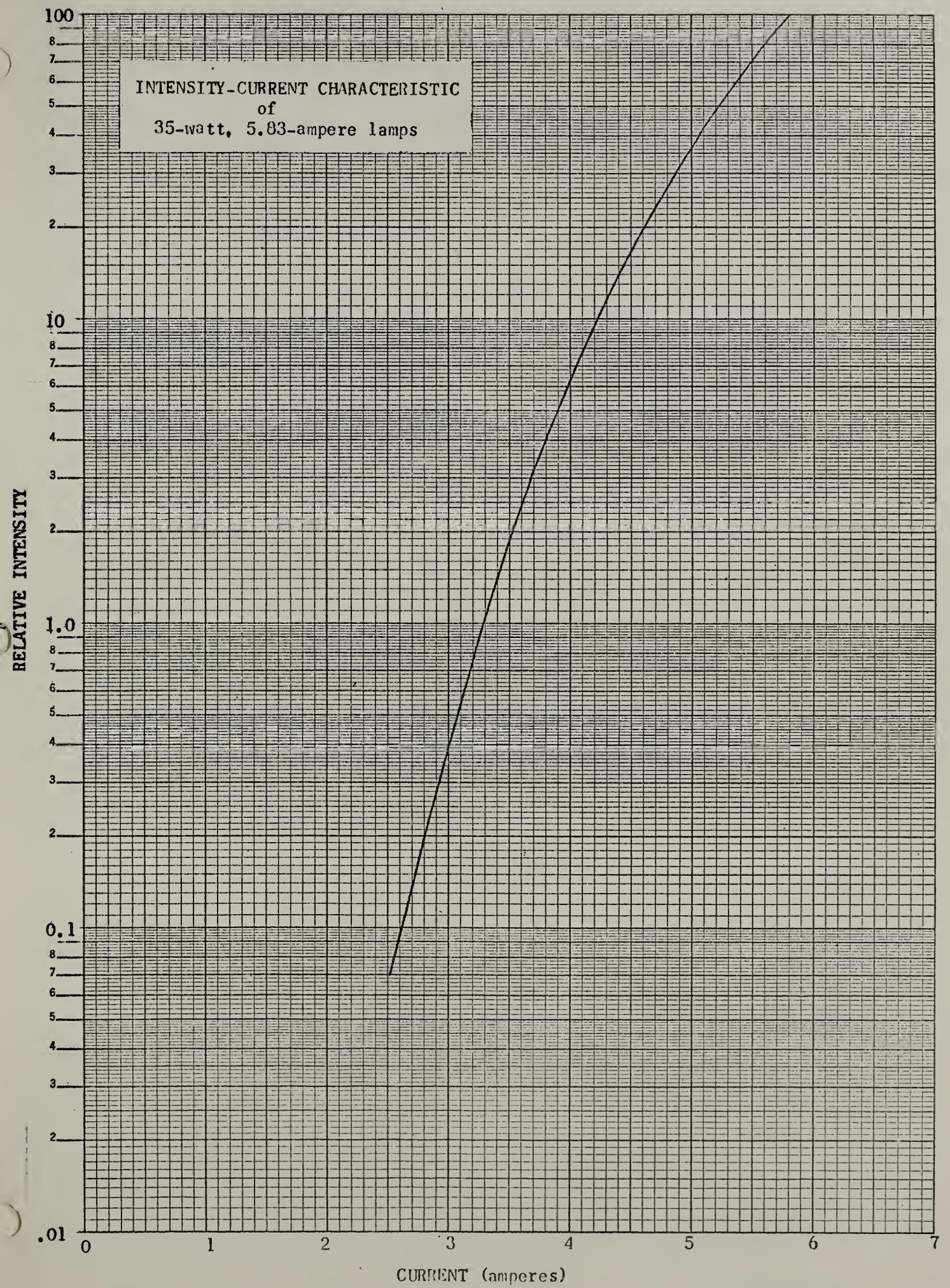
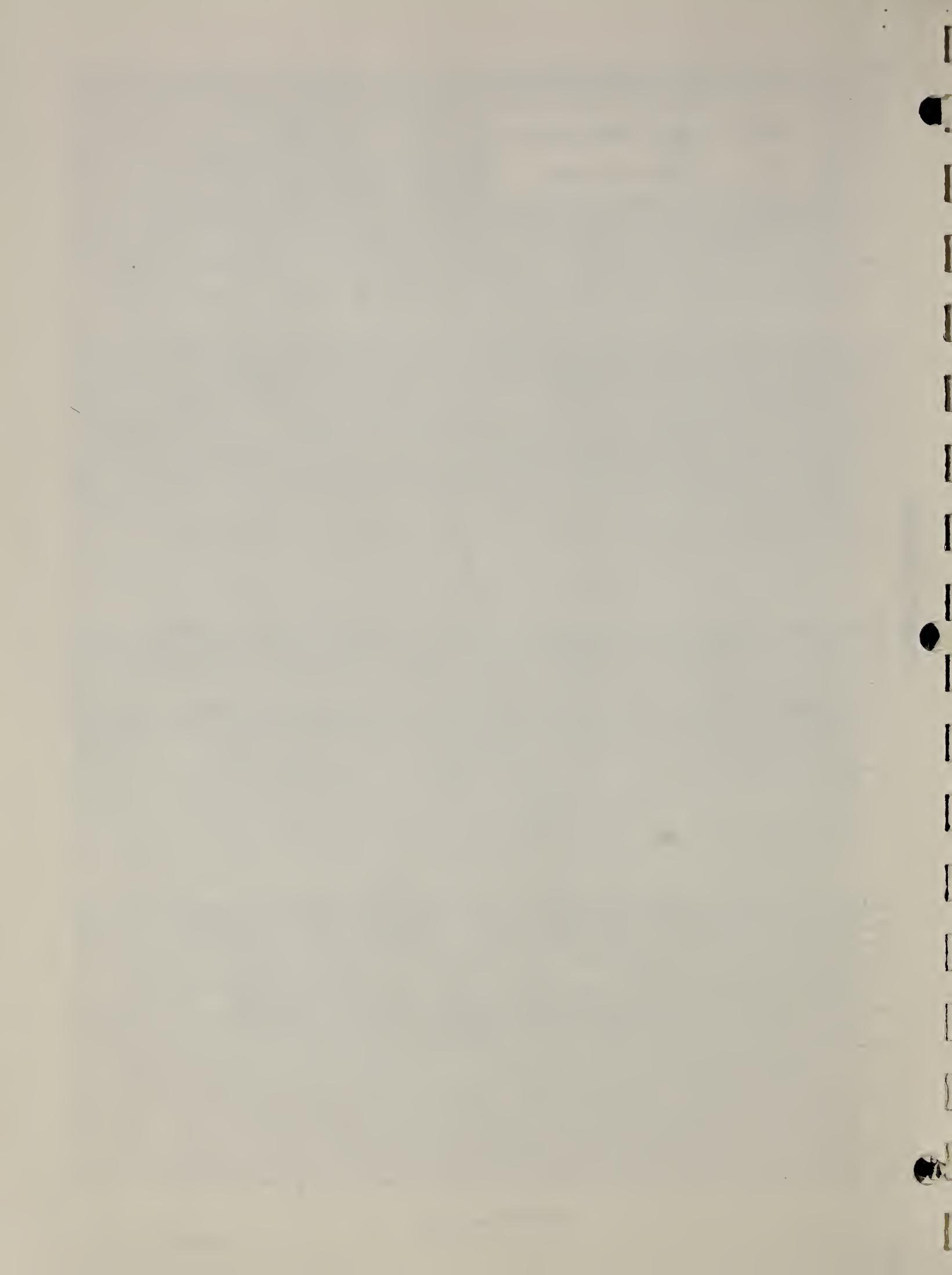


Figure 2a



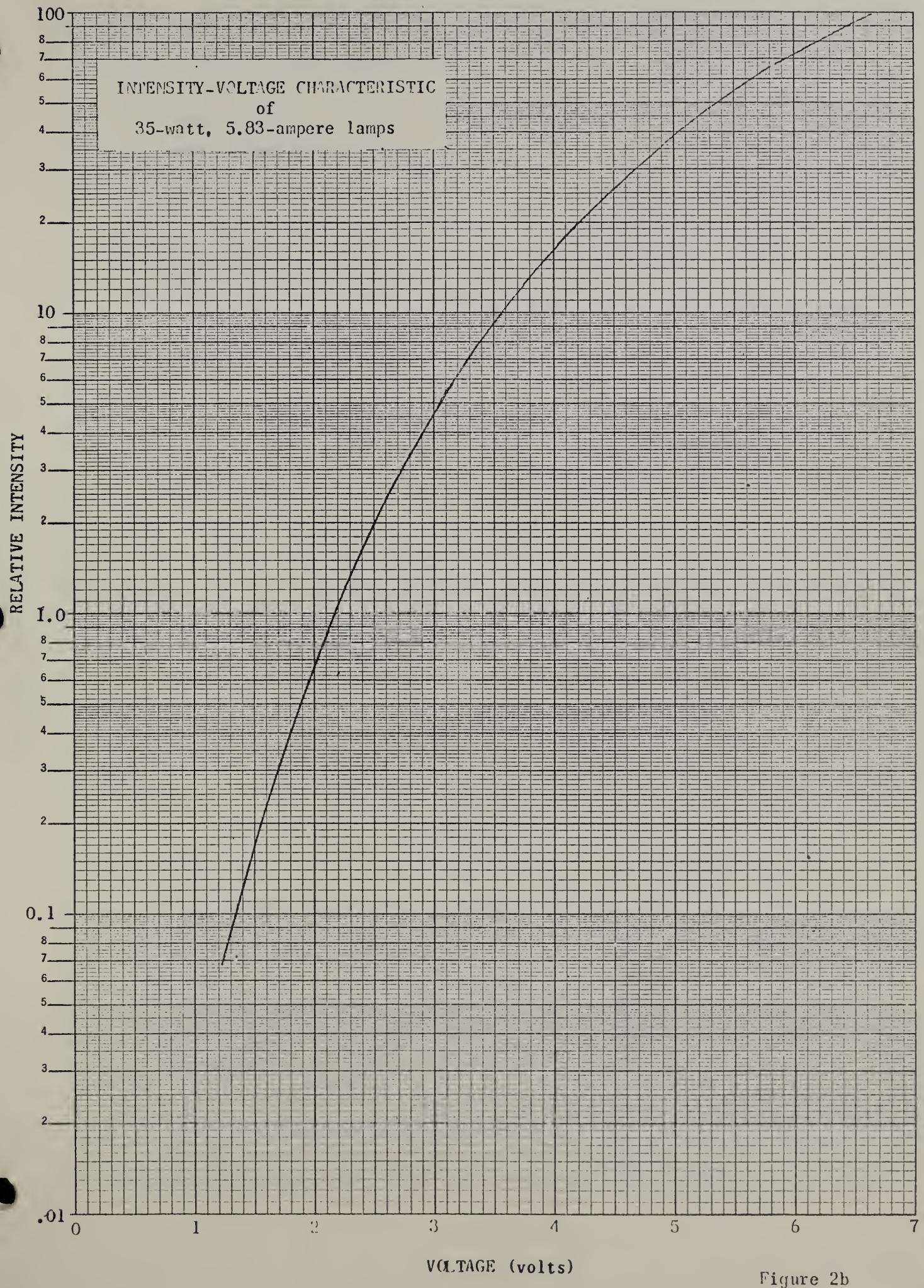


Figure 2b



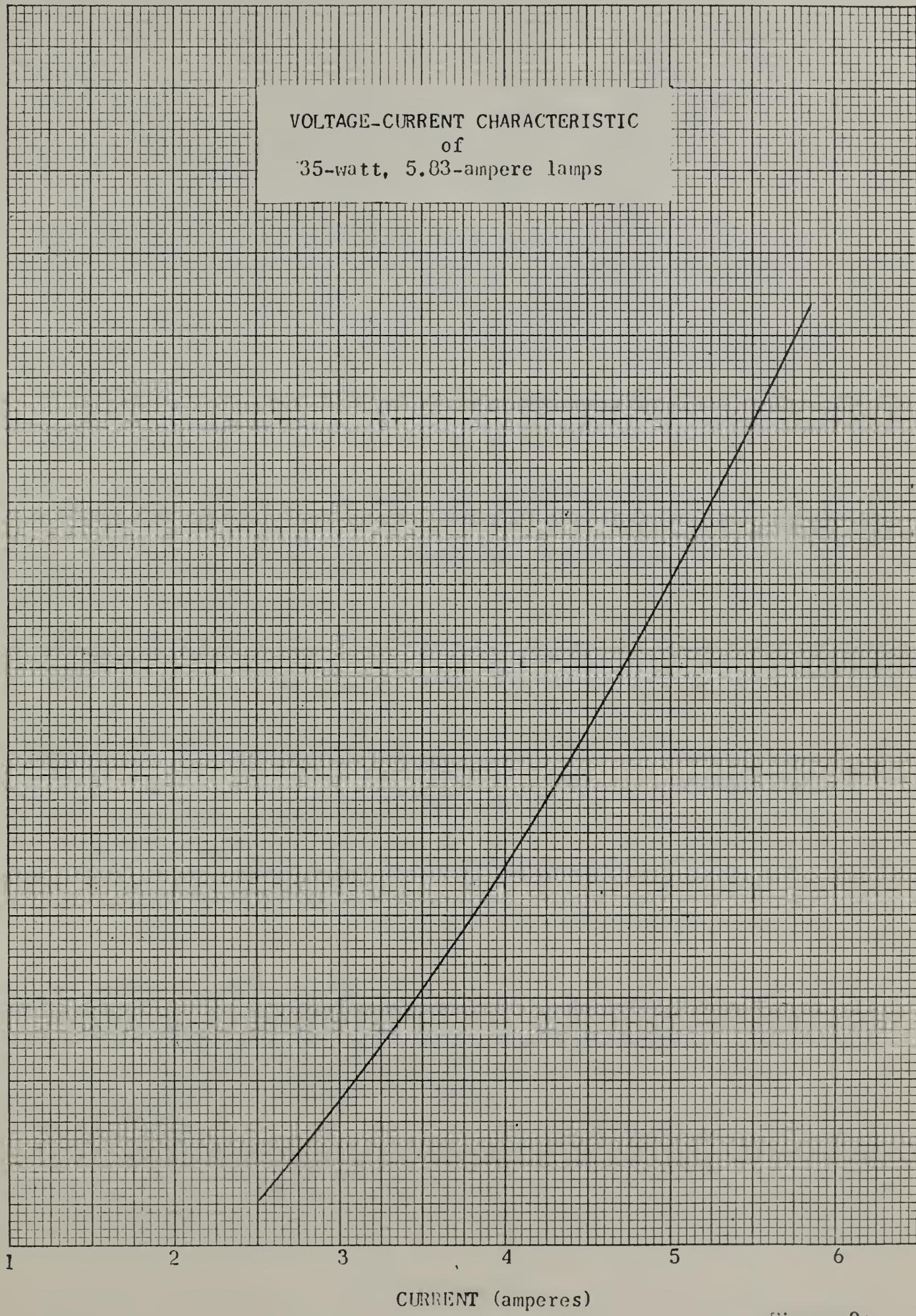


Figure 2c



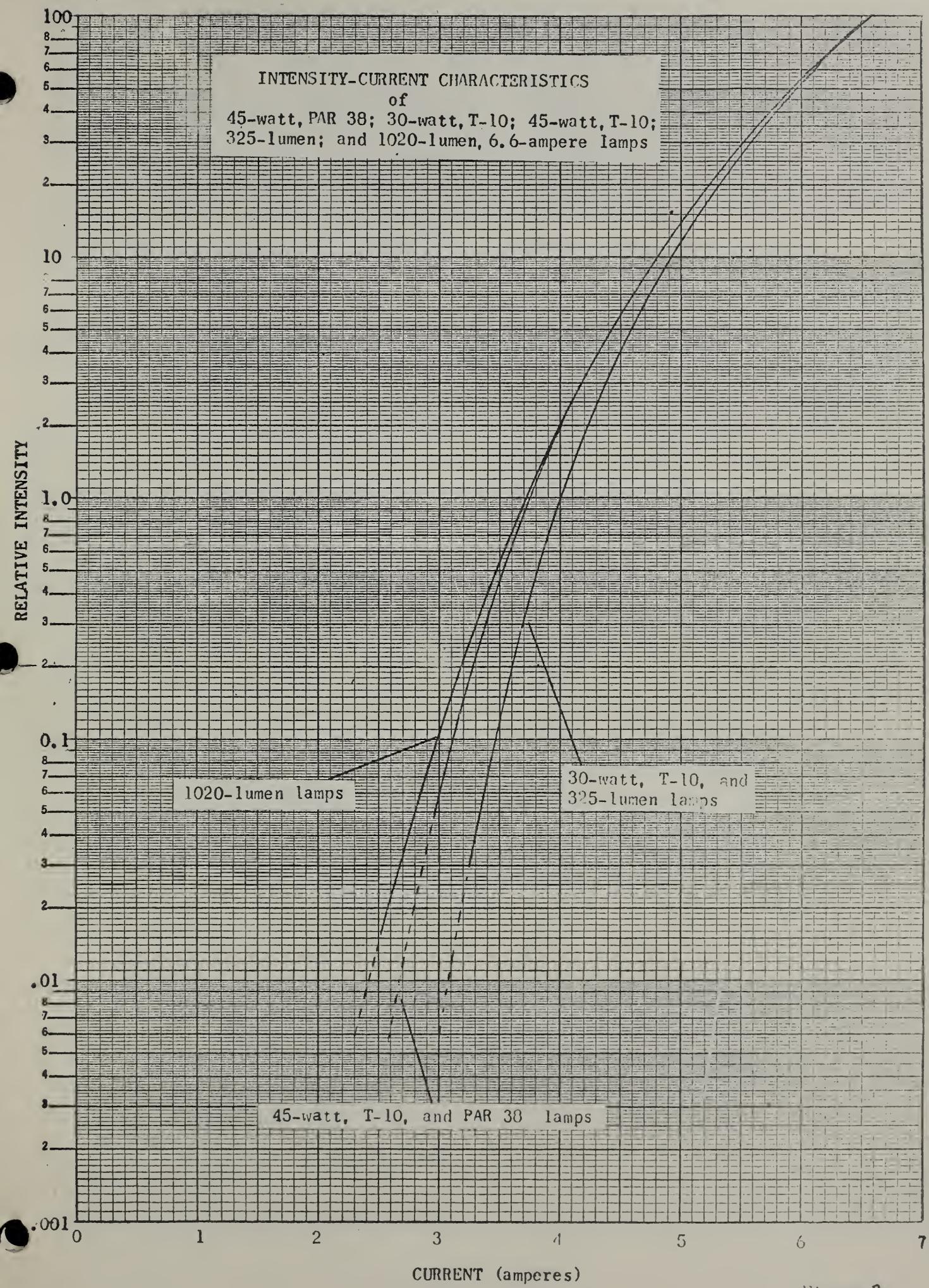
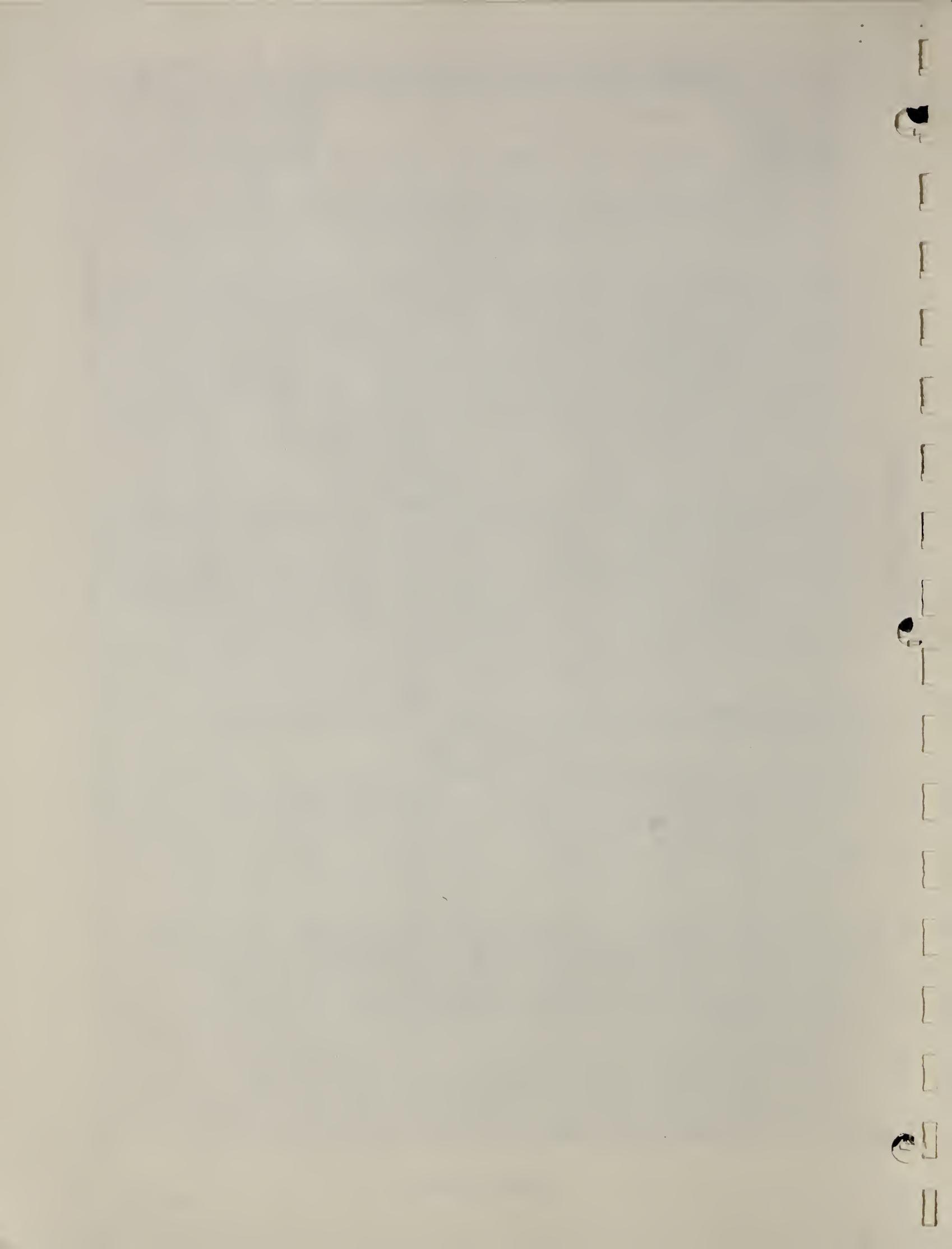


Figure 3a



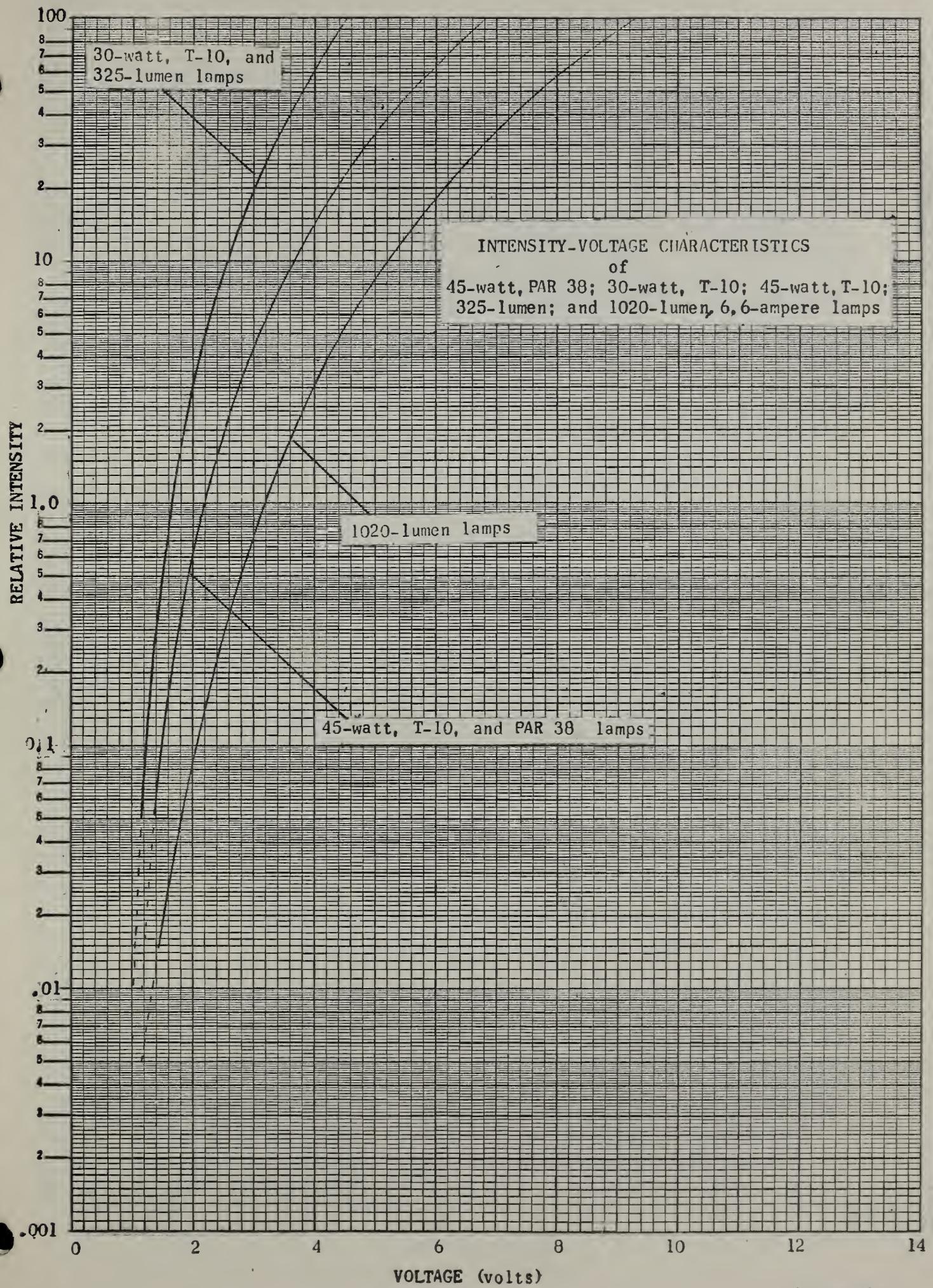
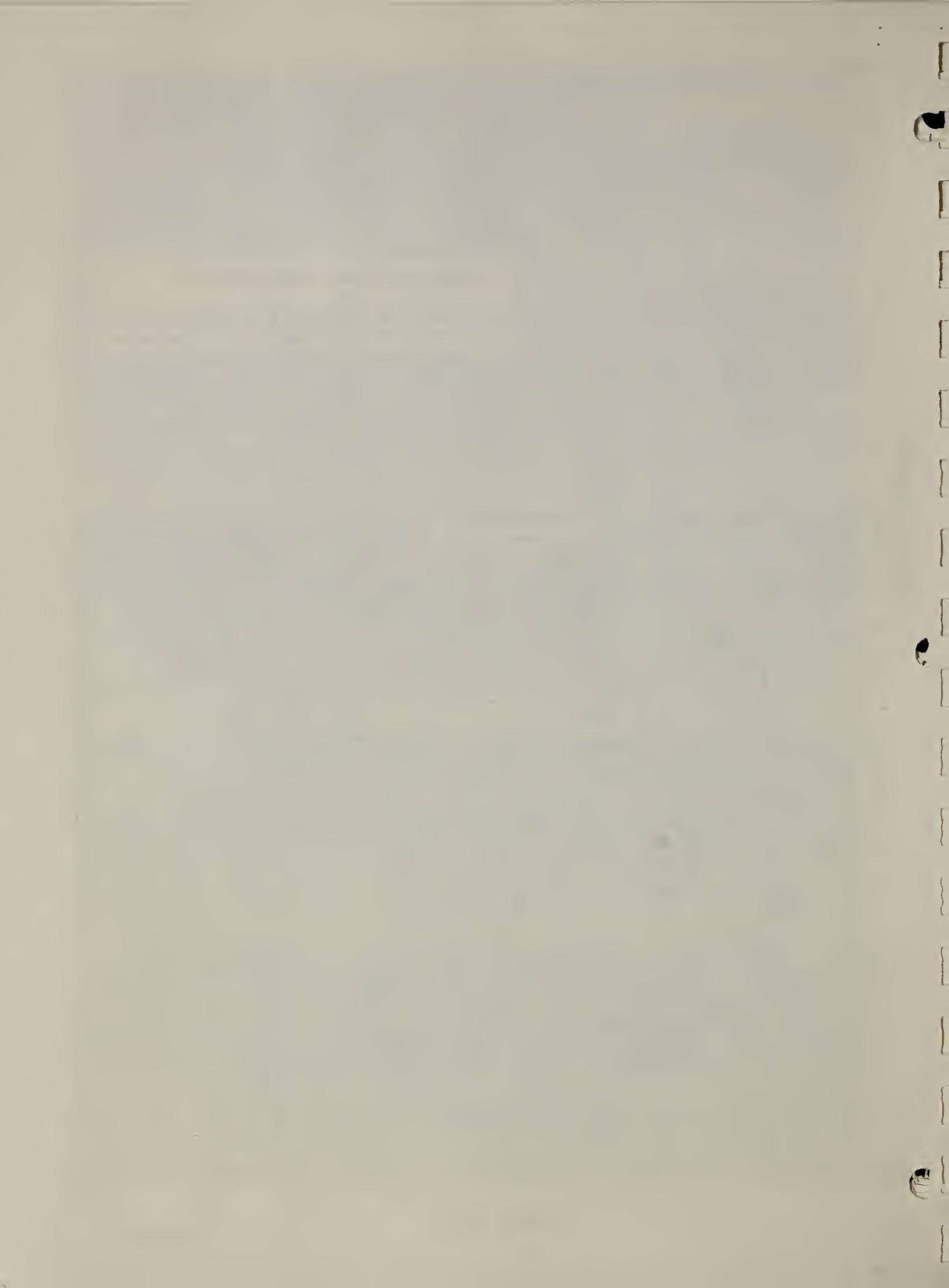
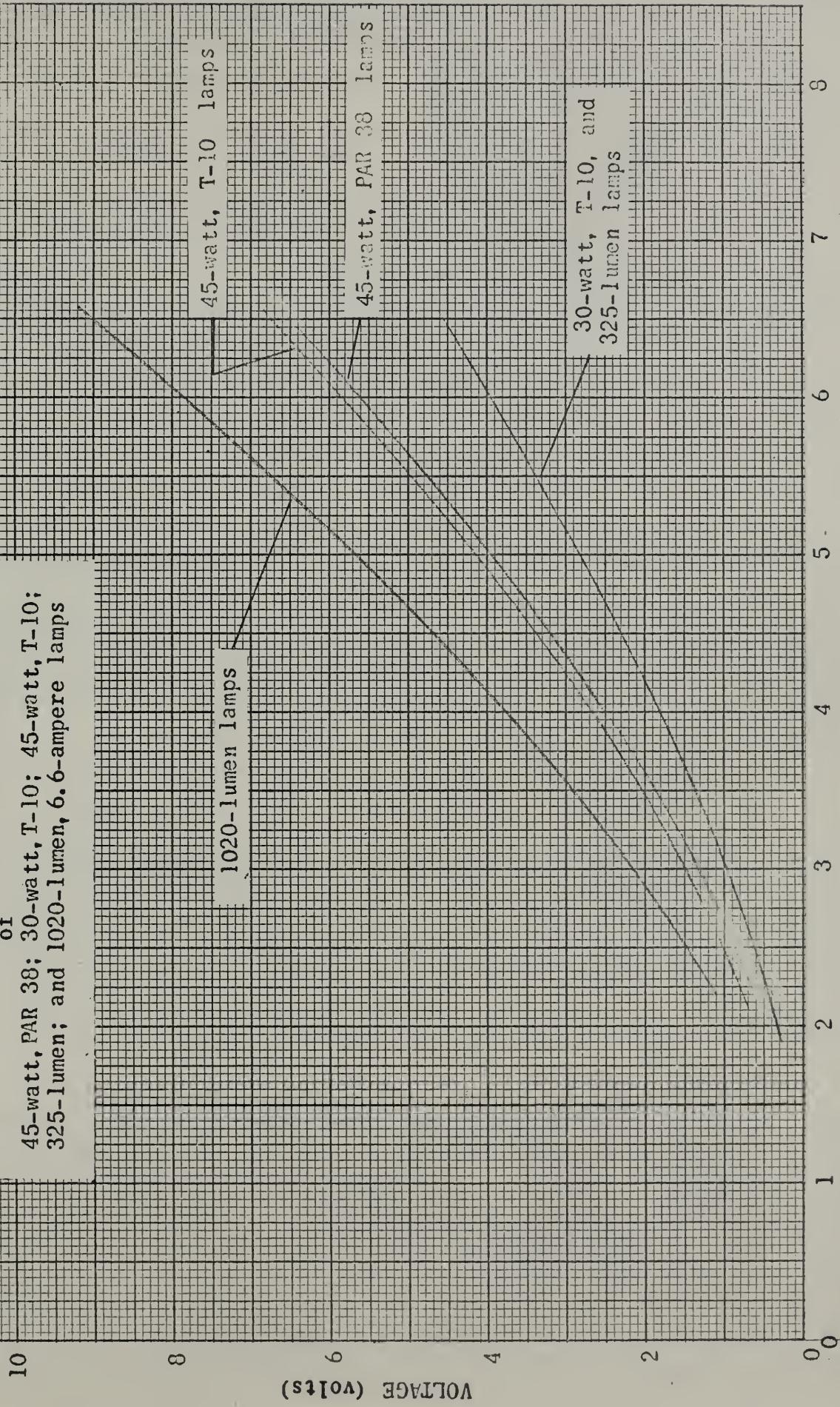


Figure 3b



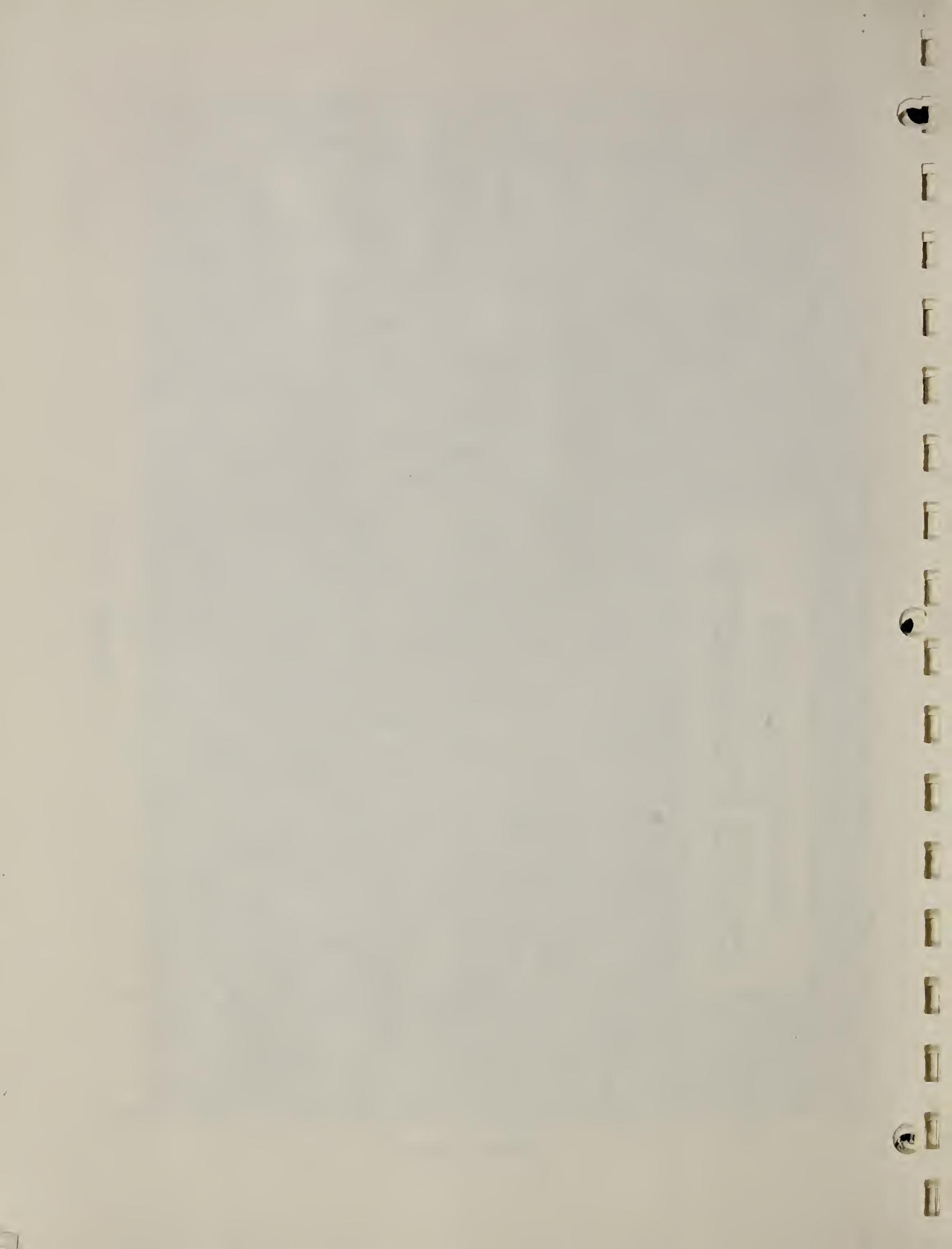
VOLTAGE-CURRENT CHARACTERISTICS
of

45-watt, PAR 38; 30-watt, T-10; 45-watt, T-10;
325-lumen; and 1020-lumen, 6.6-ampere lamps



CURRENT (amperes)

Figure 3c



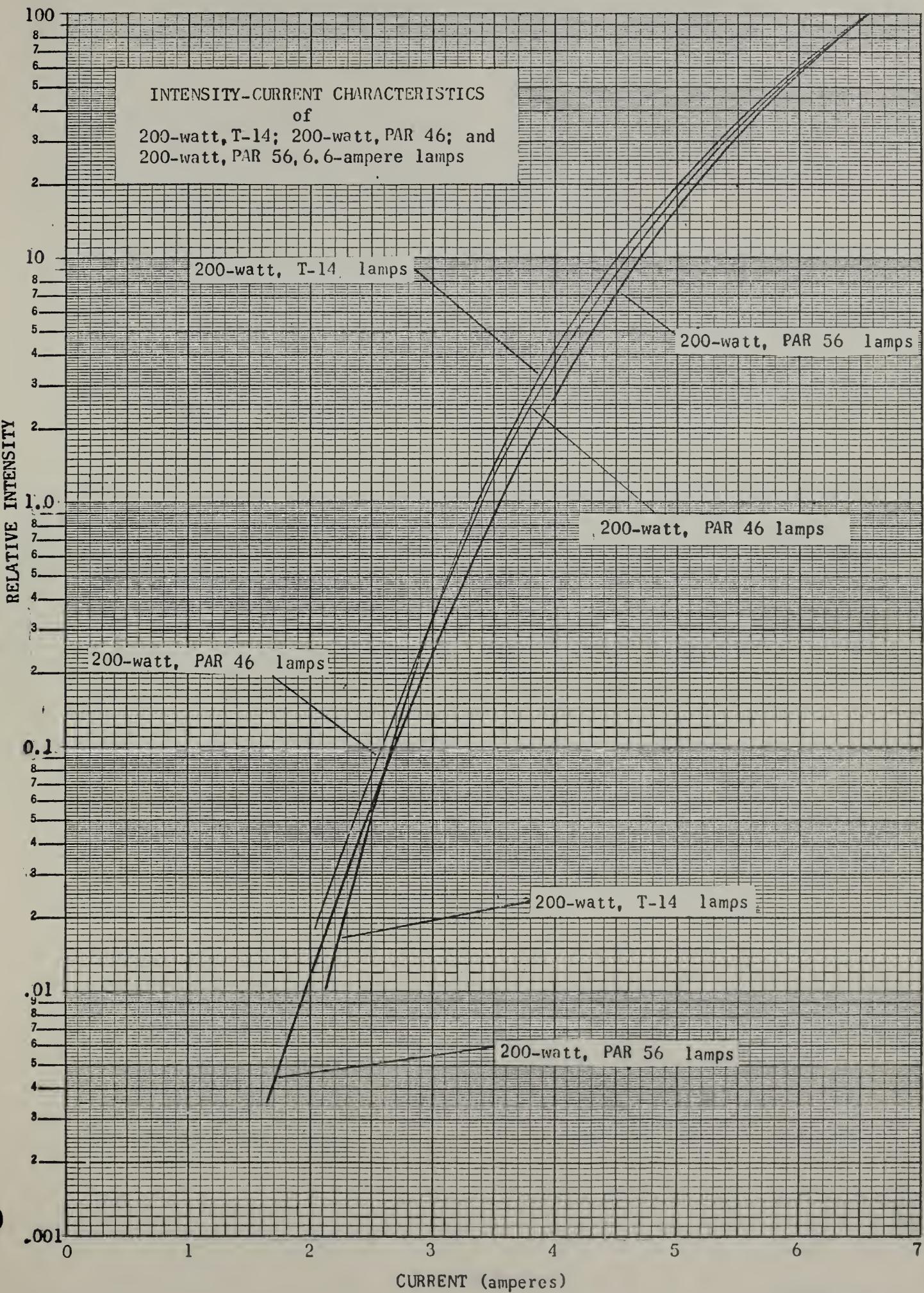
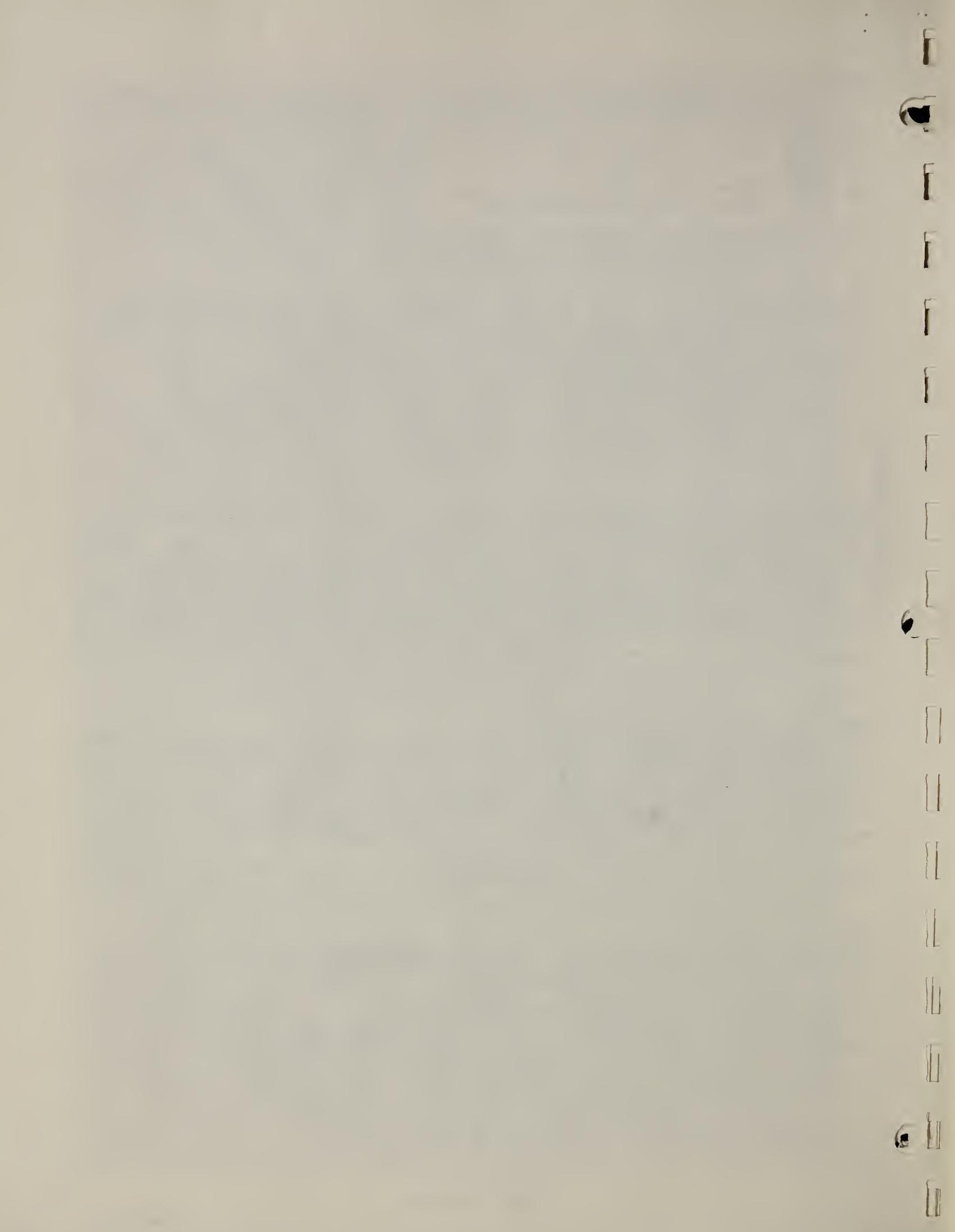


Figure 4a



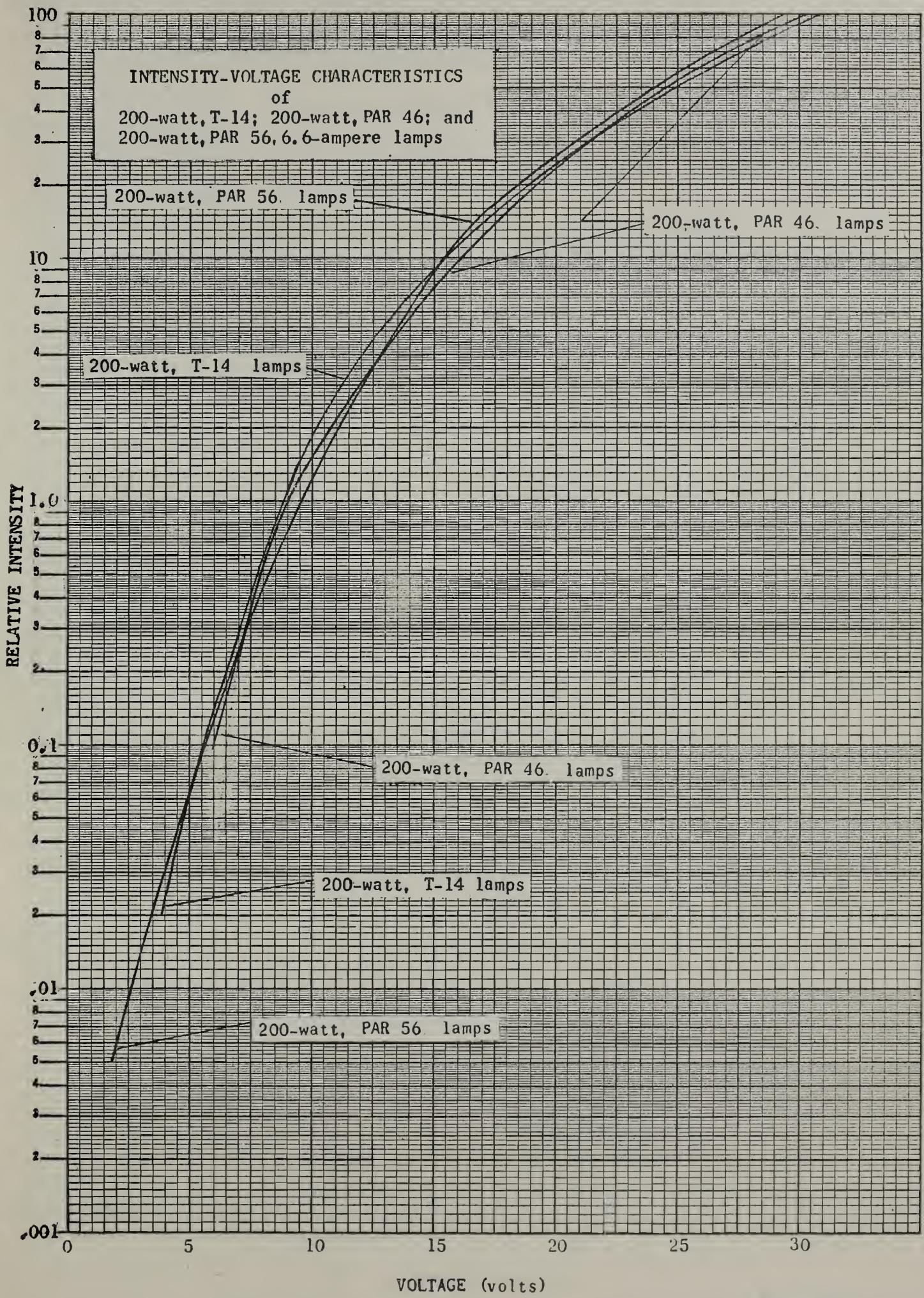


Figure 4b

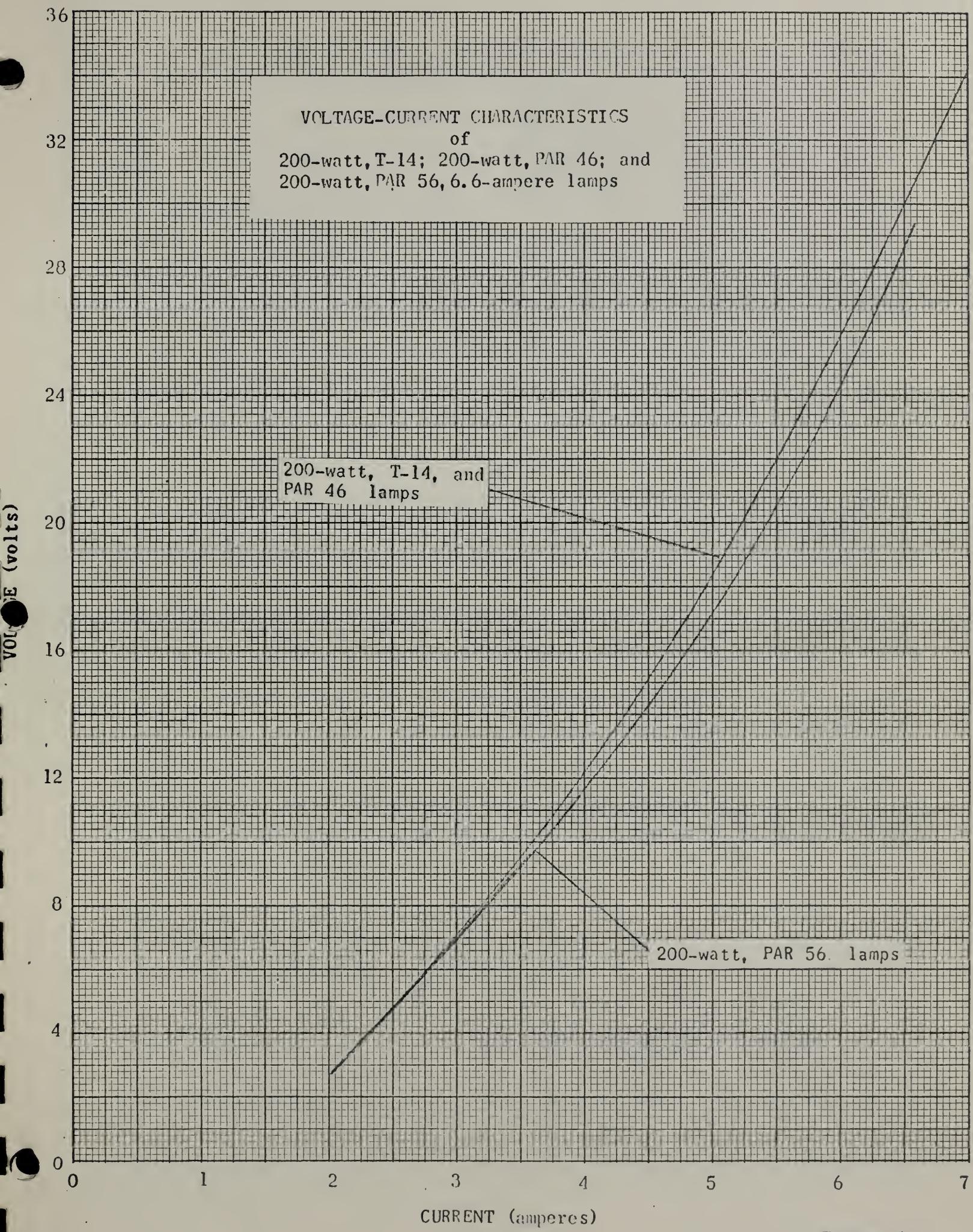
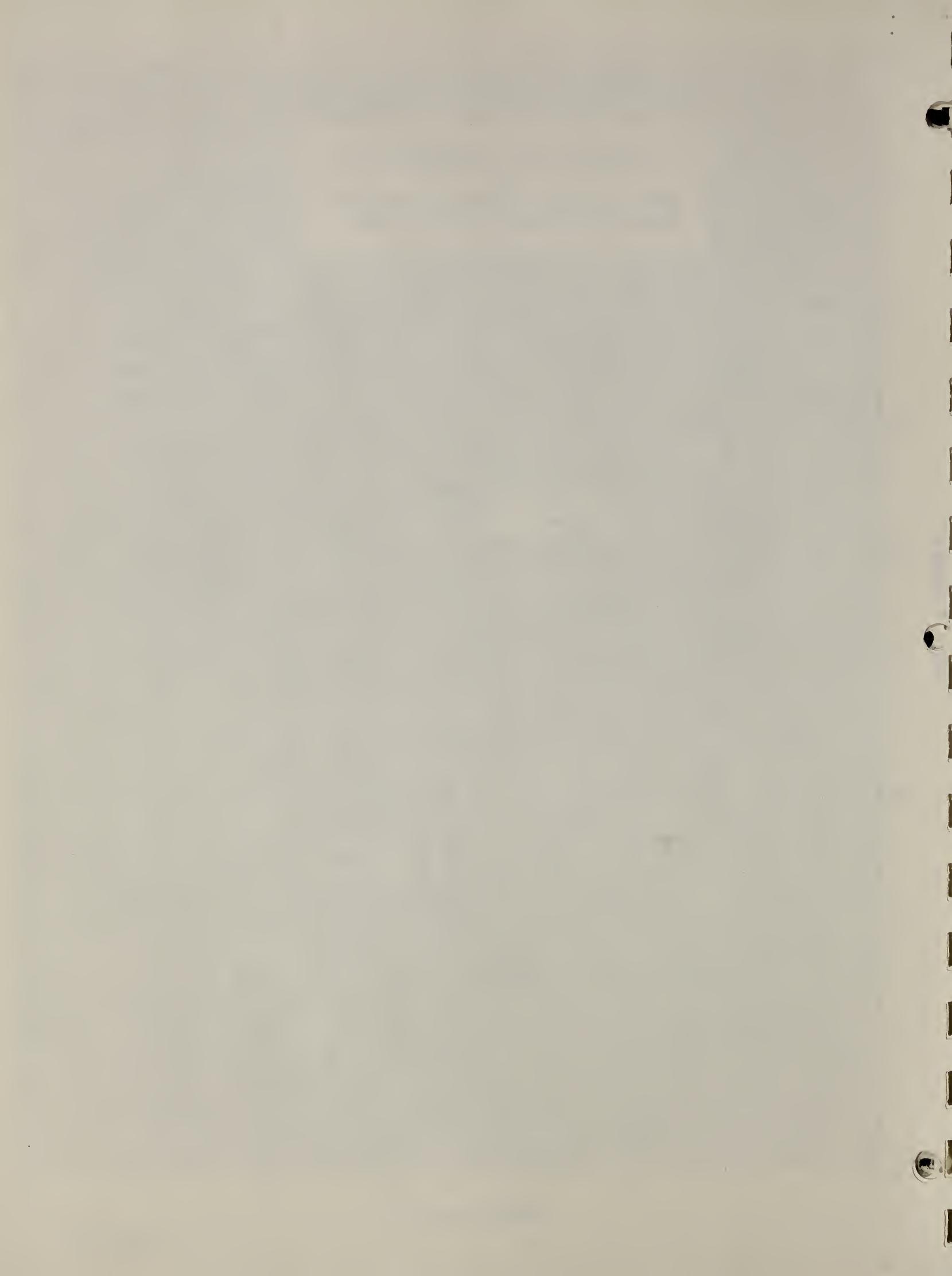


Figure 4c



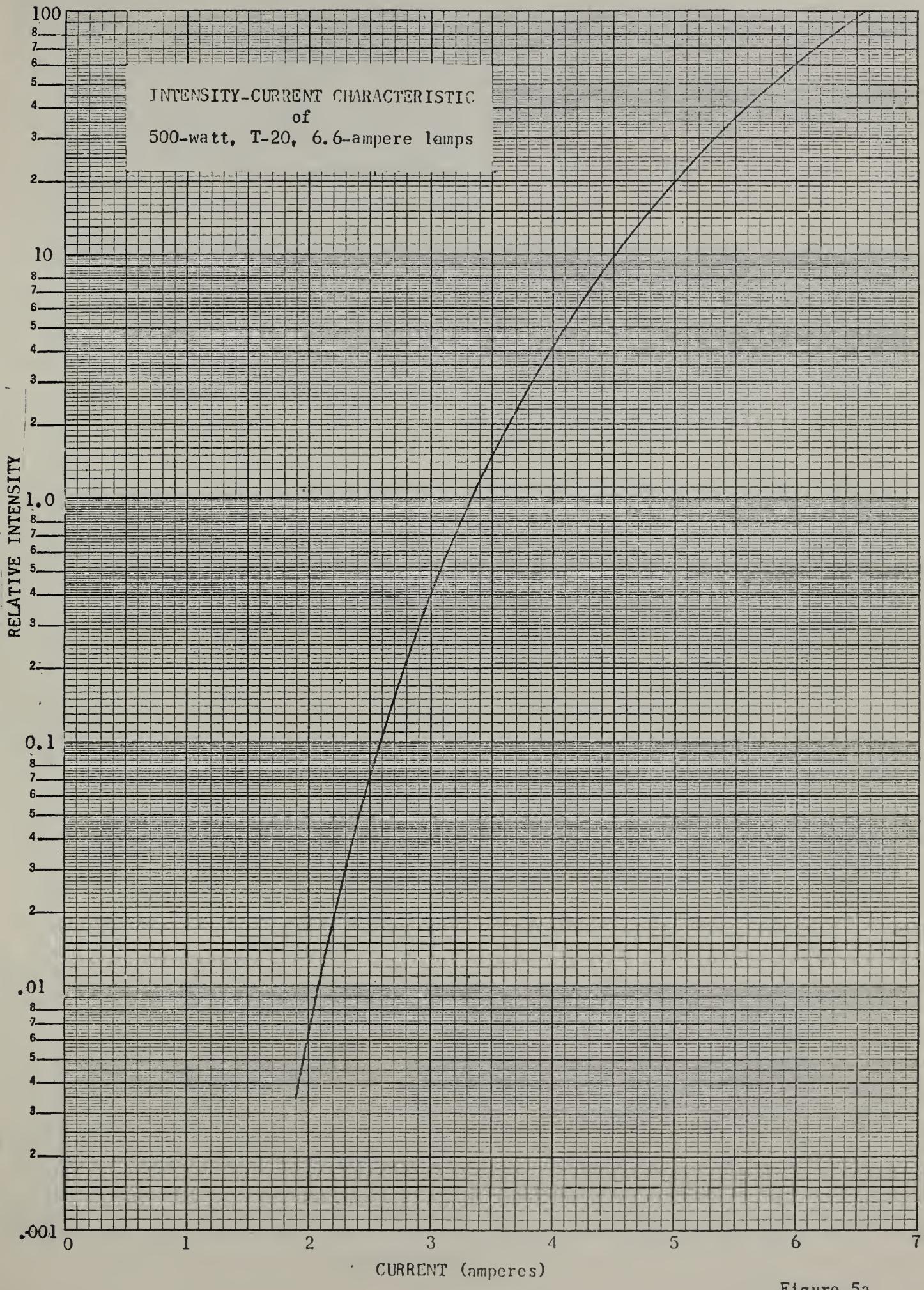
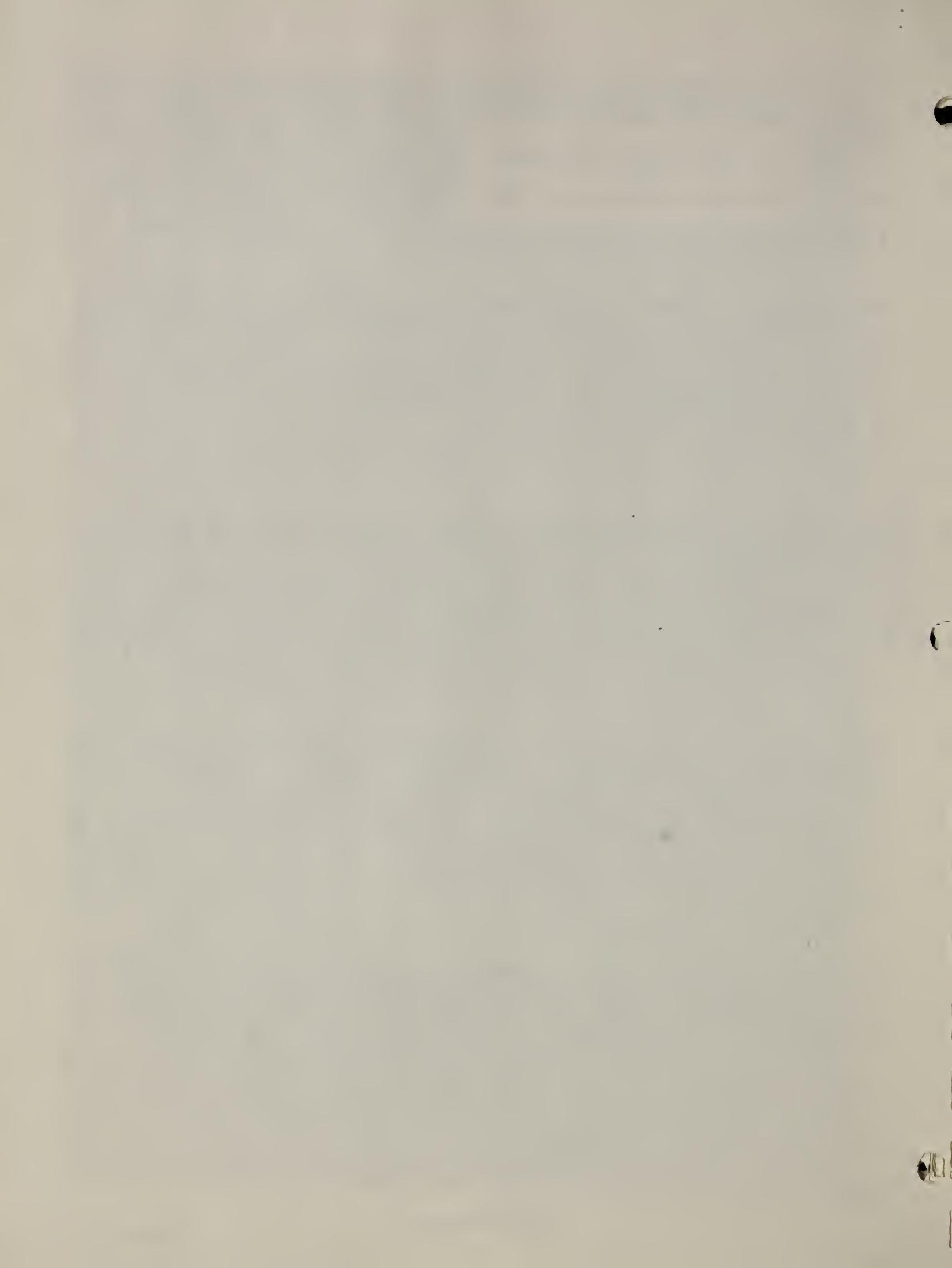


Figure 5a



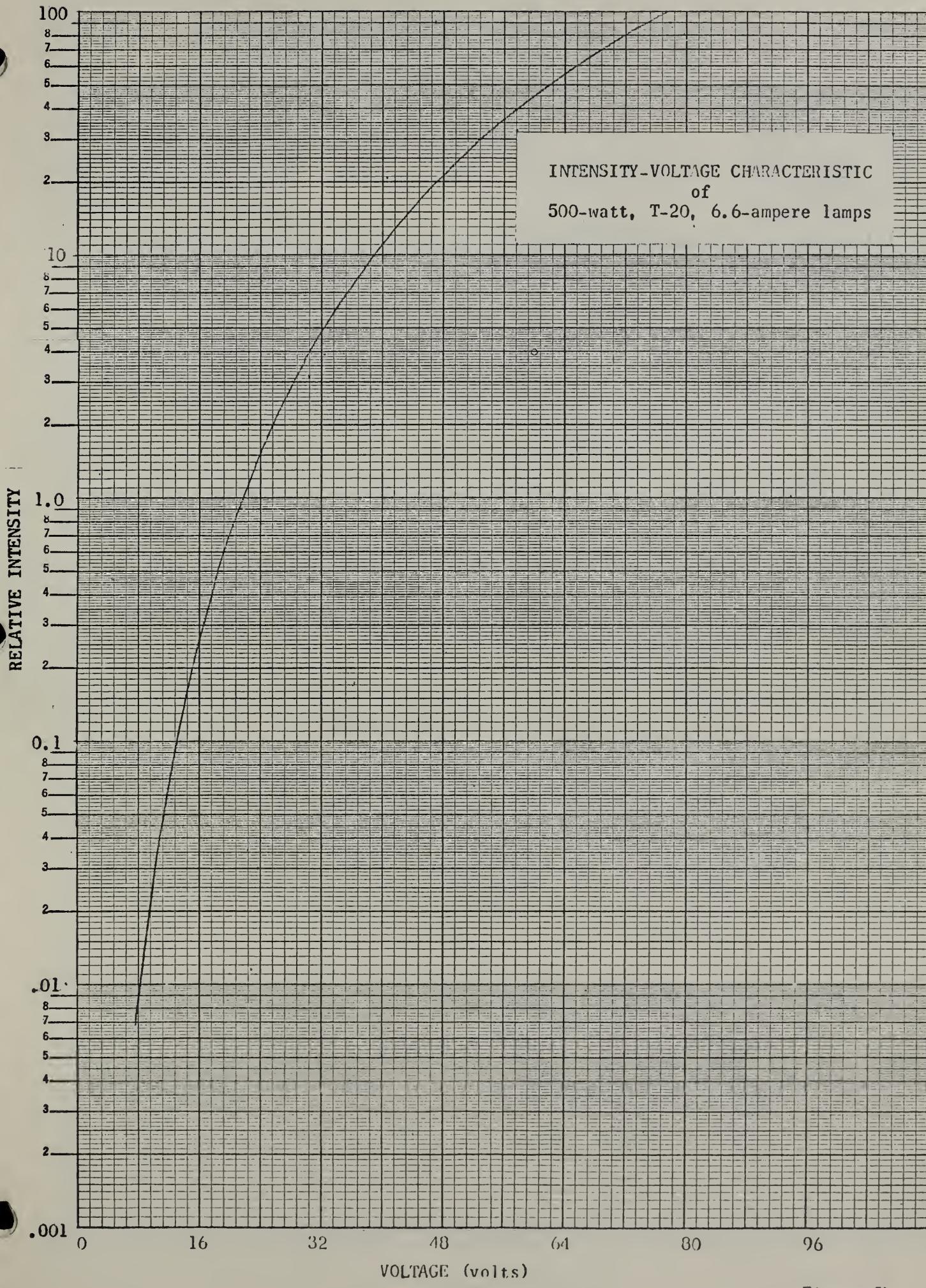


Figure 5b



VOLTAGE-CURRENT CHARACTERISTIC
of
500-watt, T-20, 6.6-ampere lamps

VOLTAGE (volts)

80
70
60
50
40
30
20
10
0

CURRENT (amperes)

0 1 2 3 4 5 6 7

Figure 5c



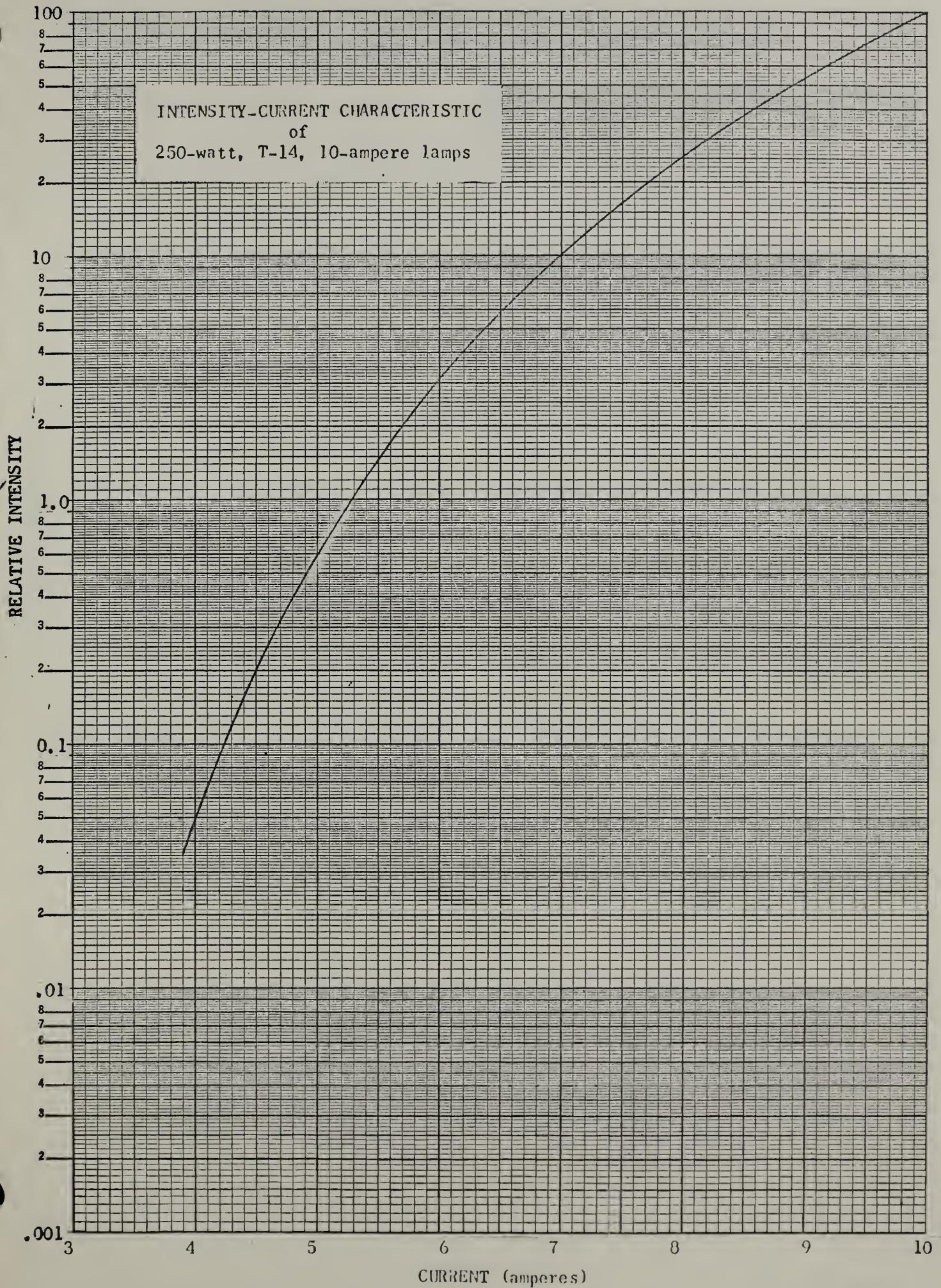
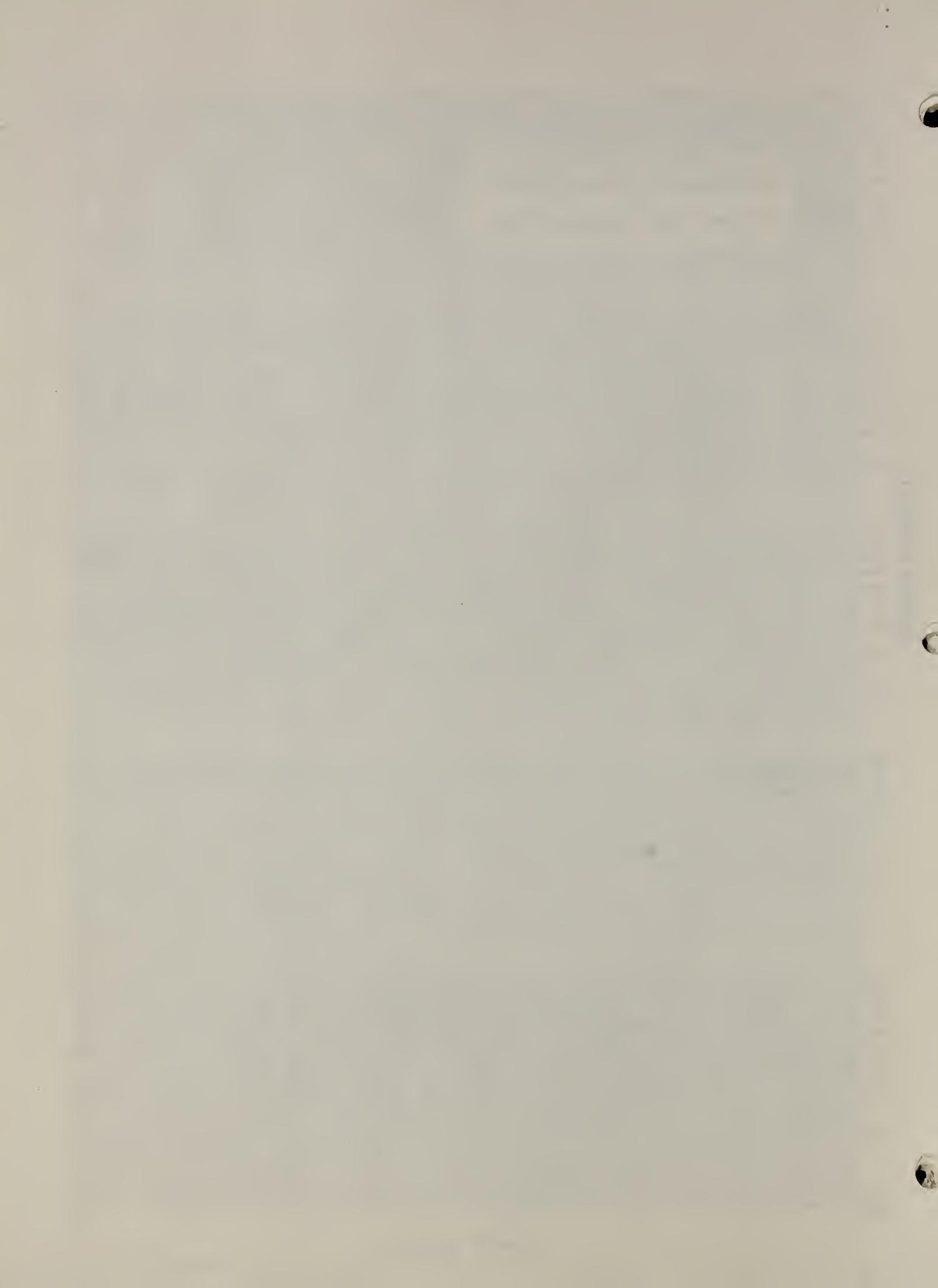


Figure 6a



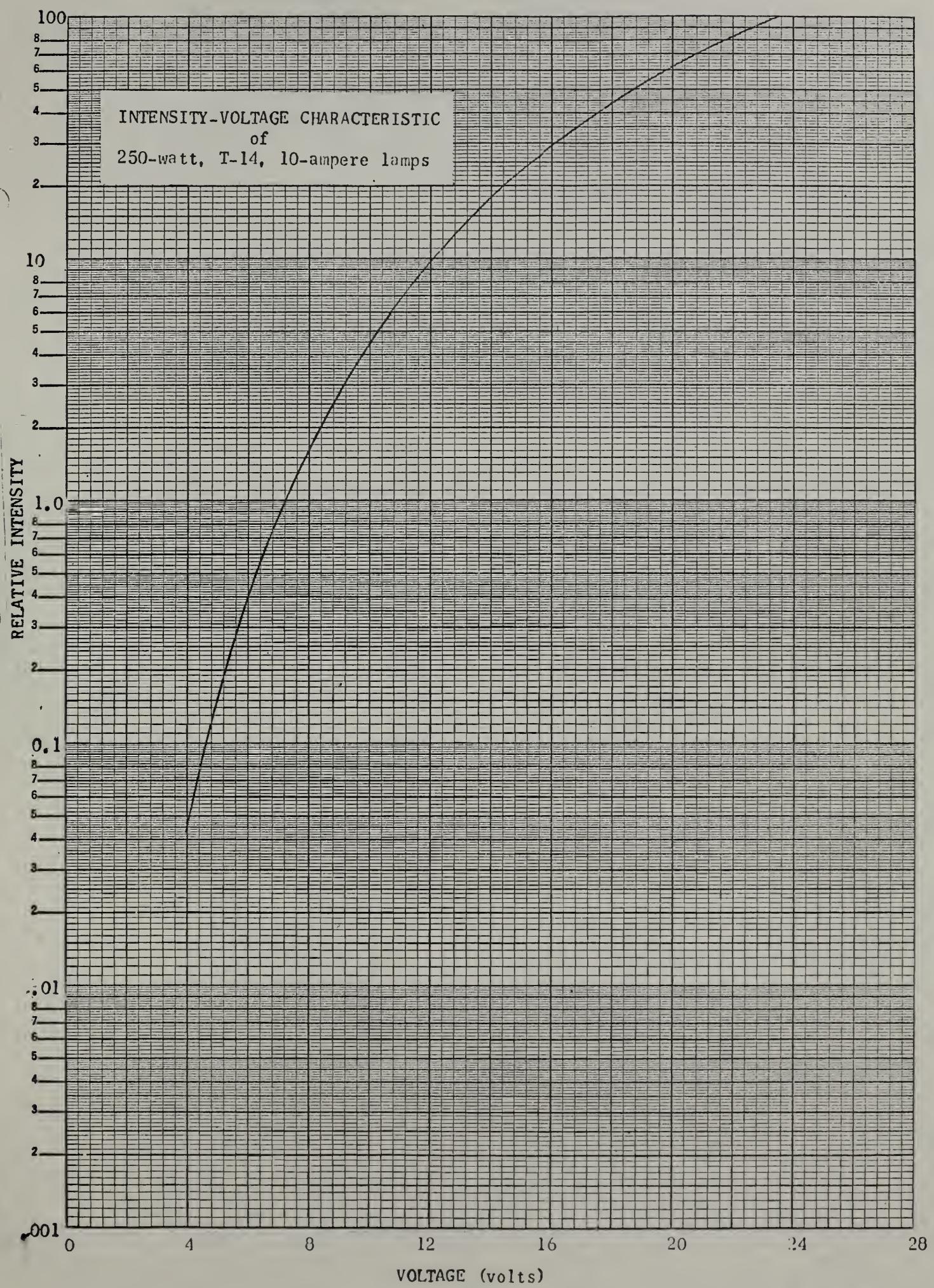


Figure 6b

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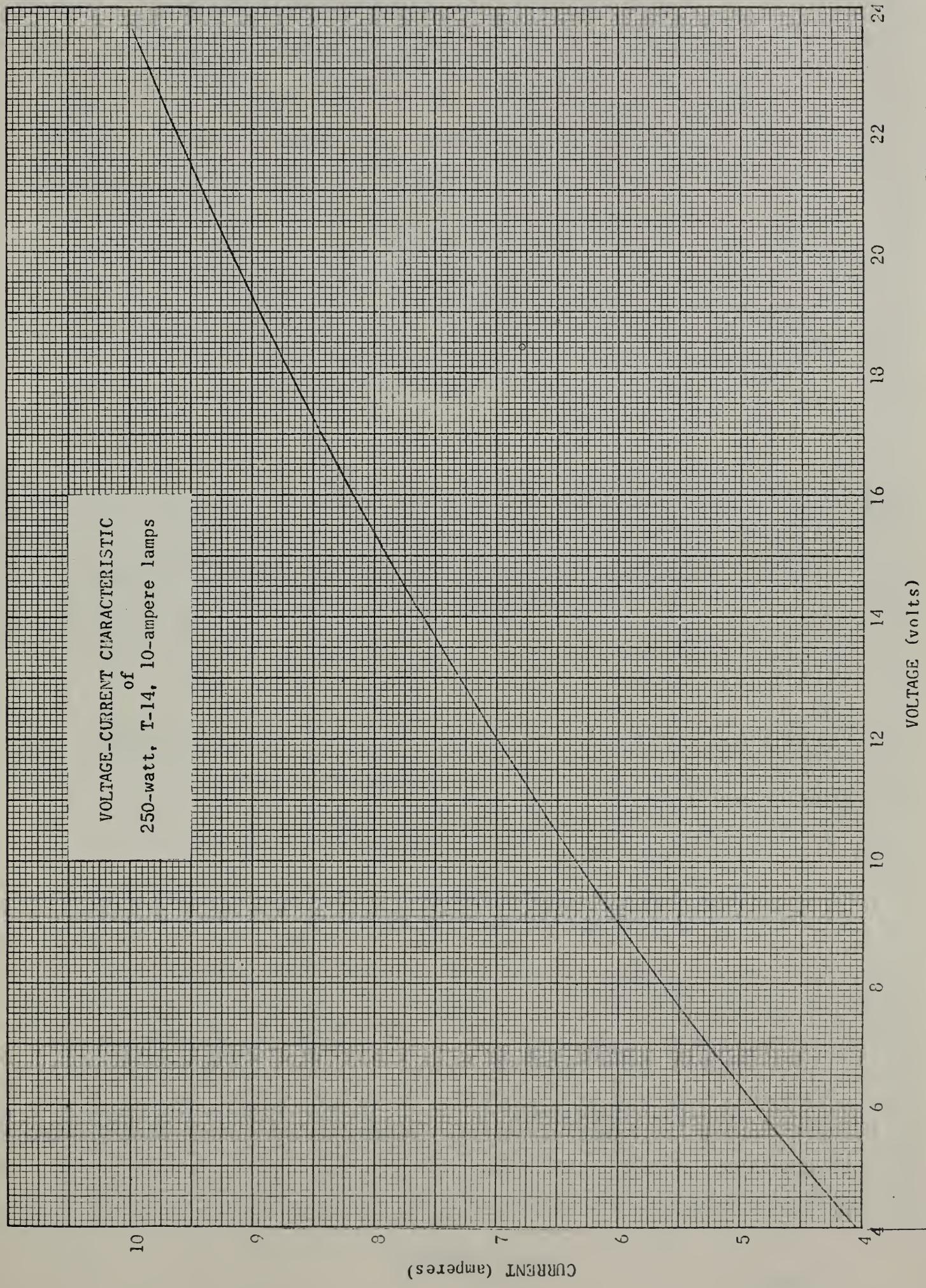
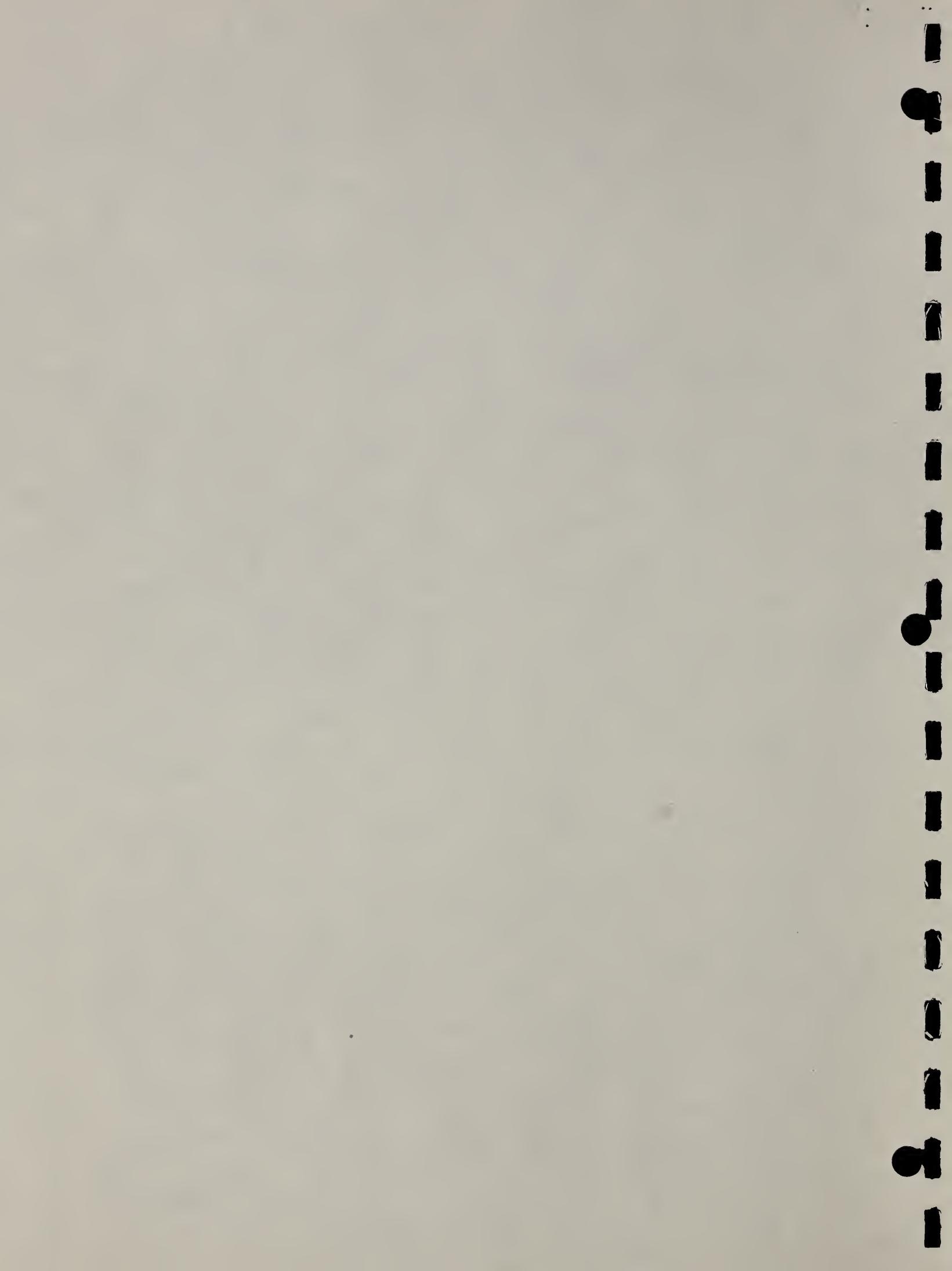


Figure 6c



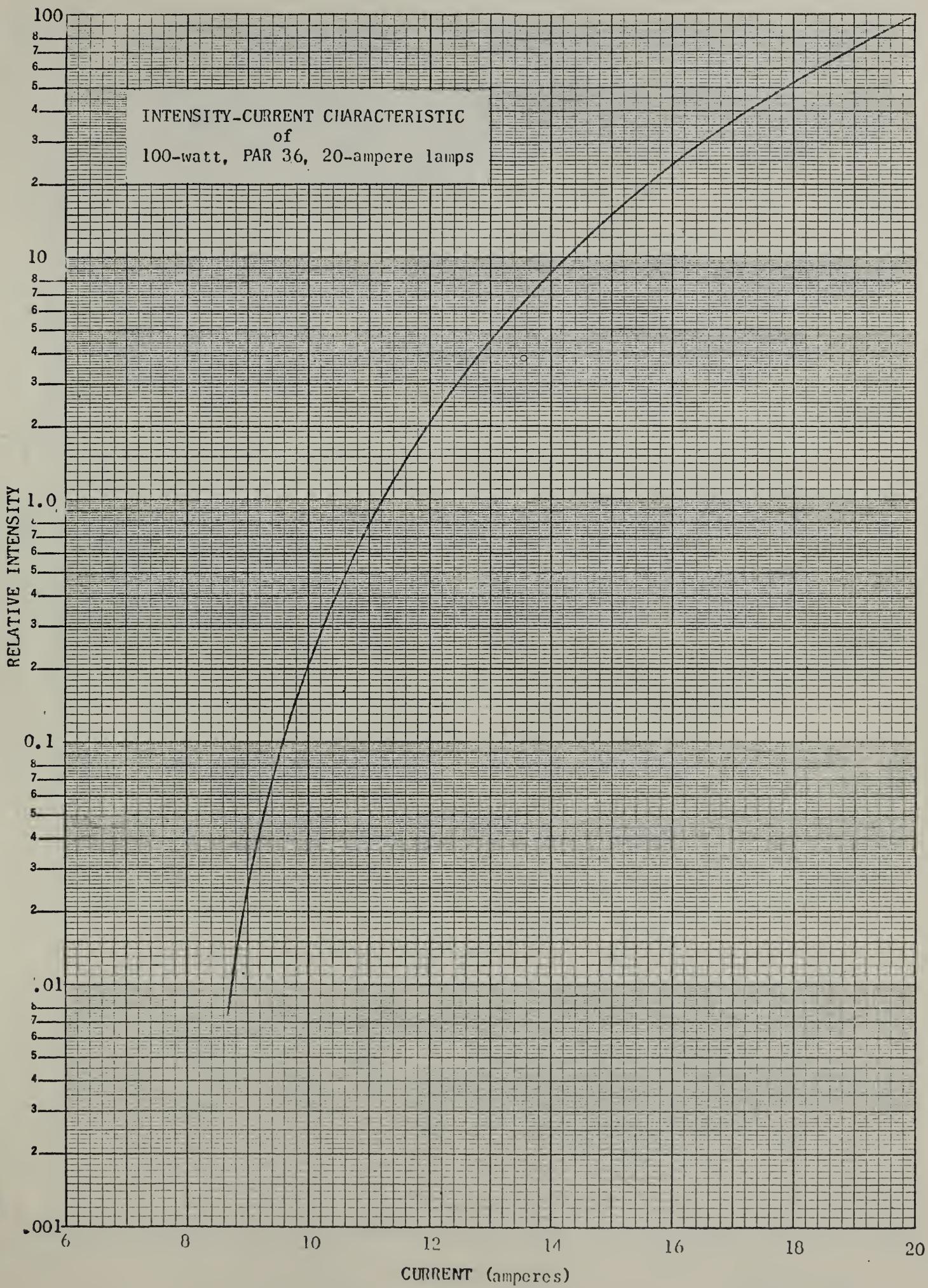
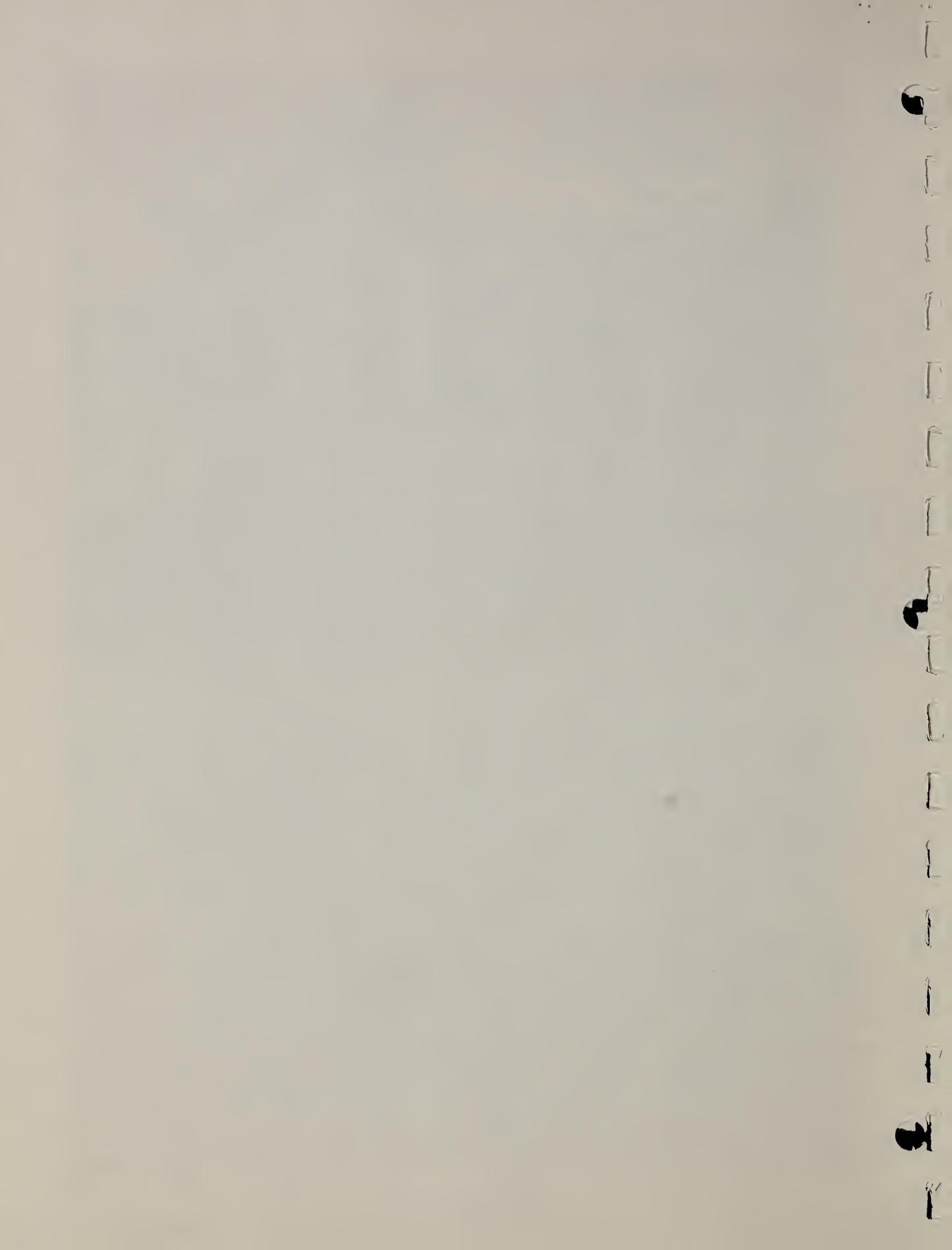


Figure 7a



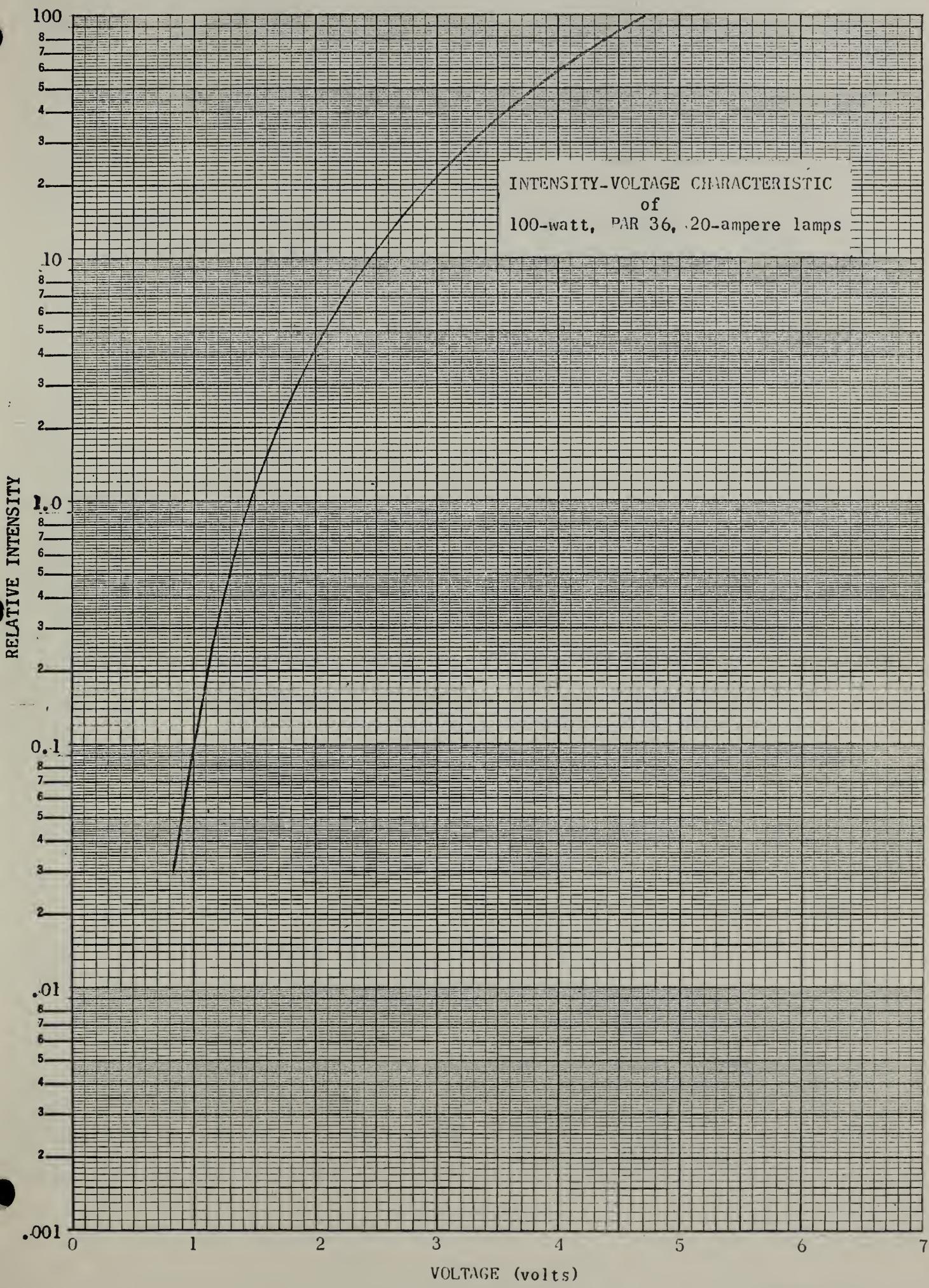
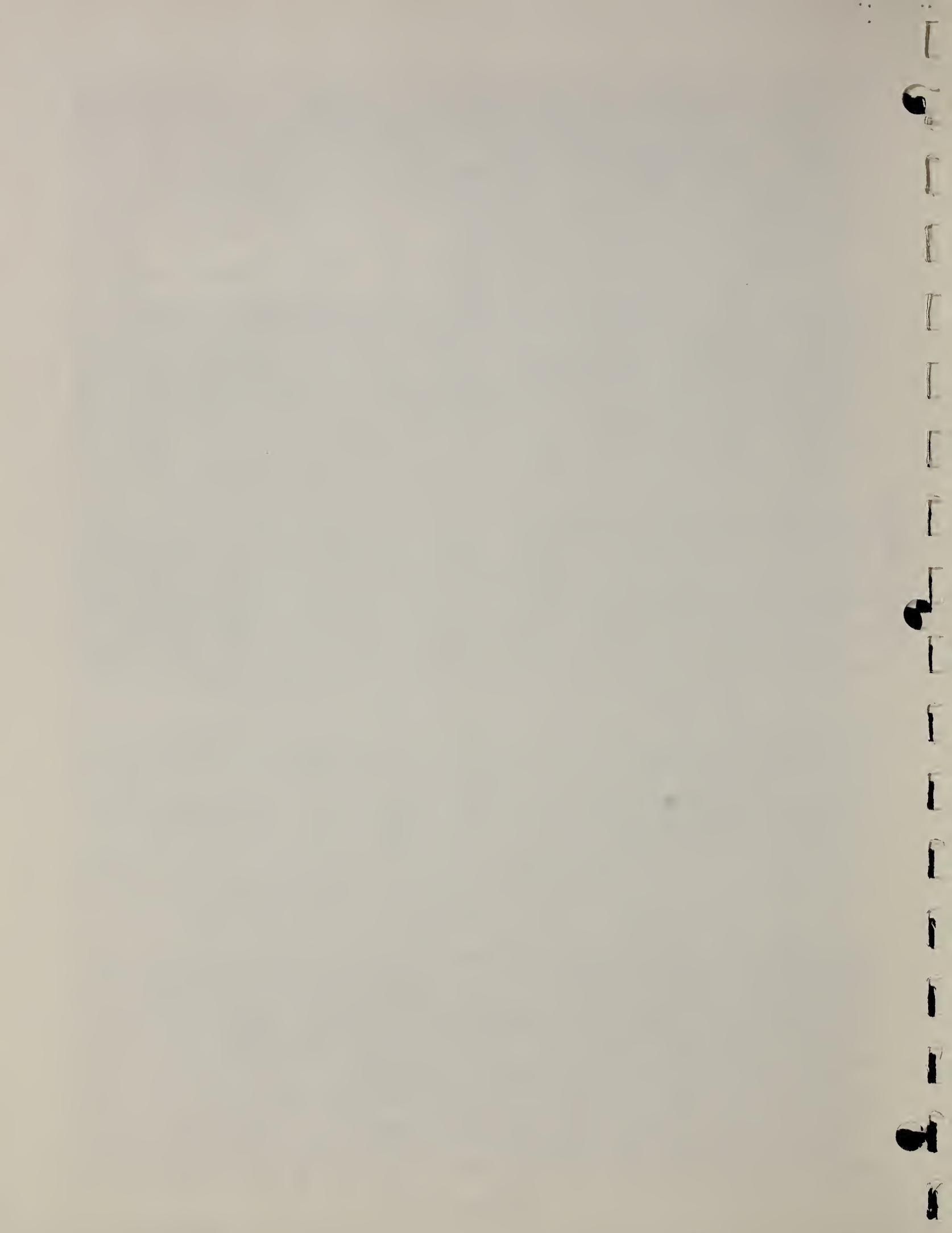


Figure 7b



VOLTAGE-CURRENT CHARACTERISTIC
of
100-watt, PAR 36, 20-ampere lamps

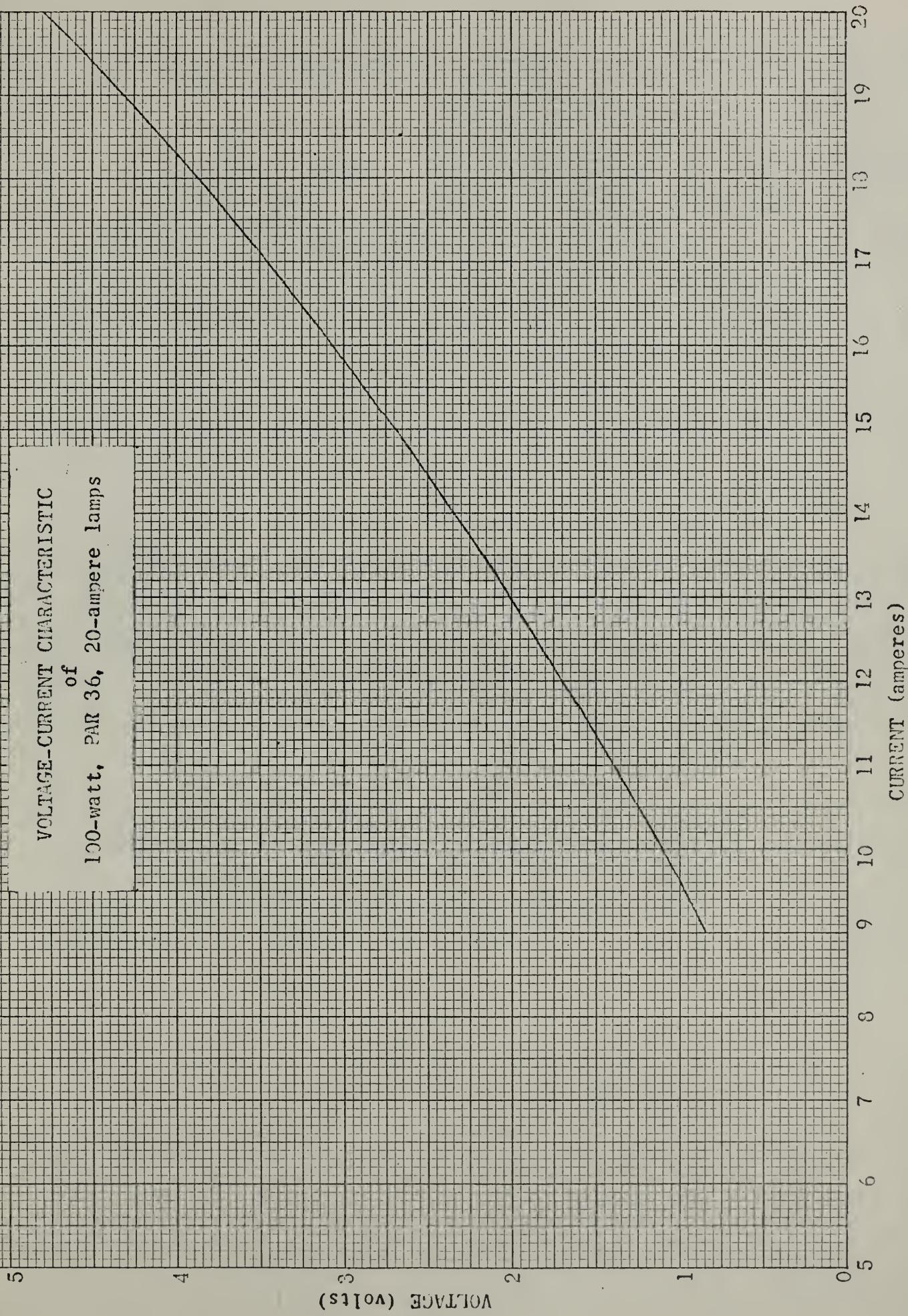


Figure 7c

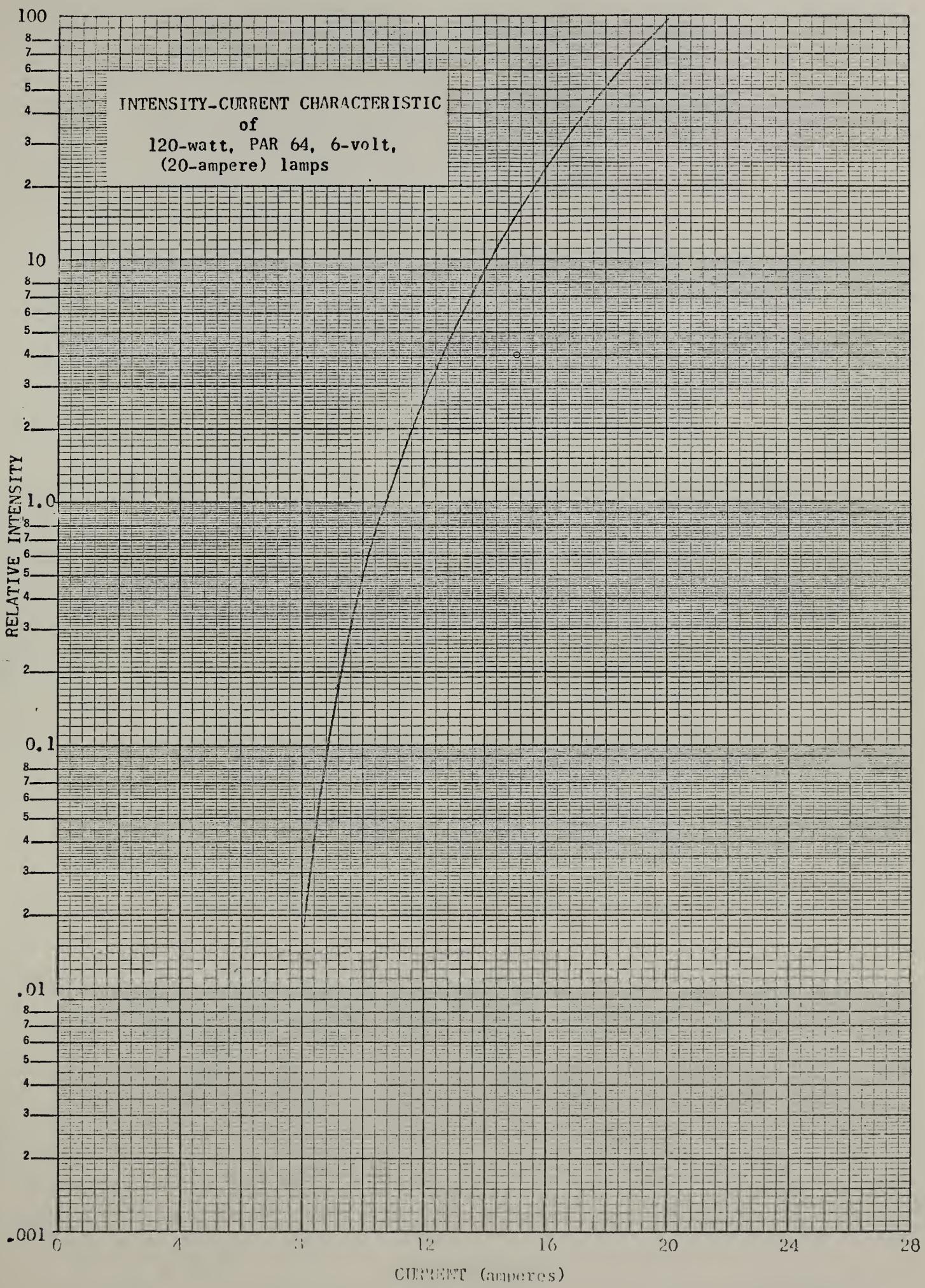
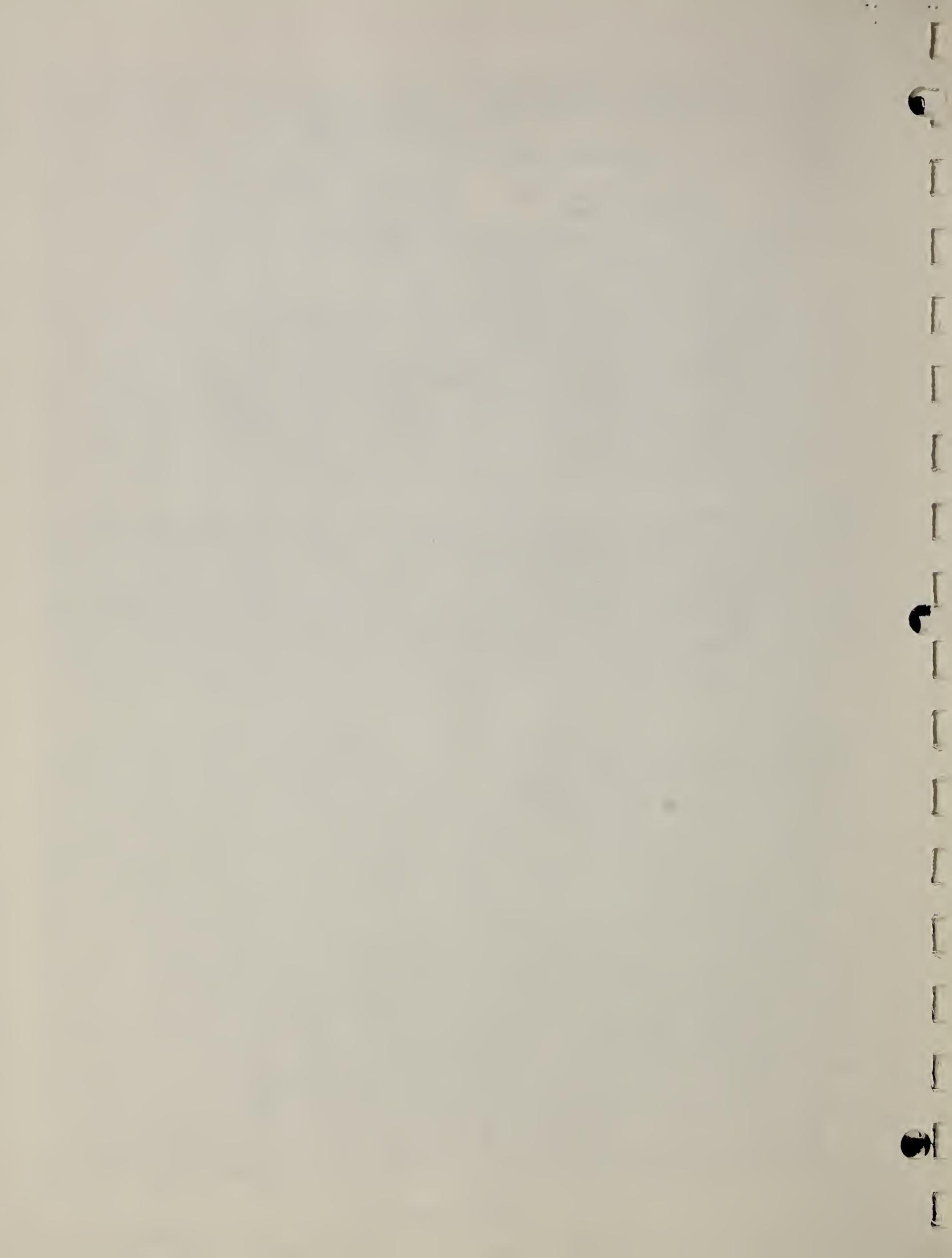


Figure 8a



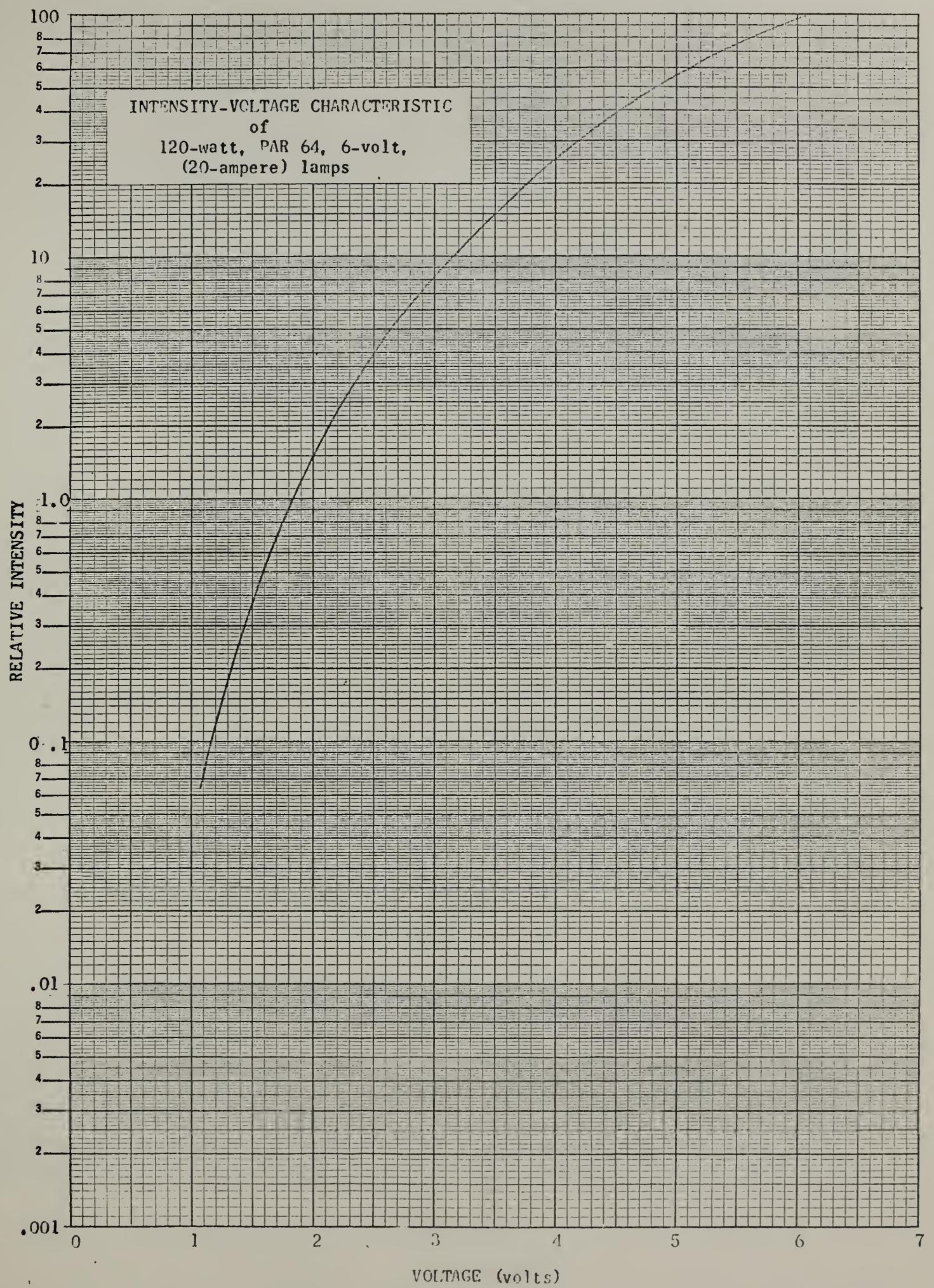
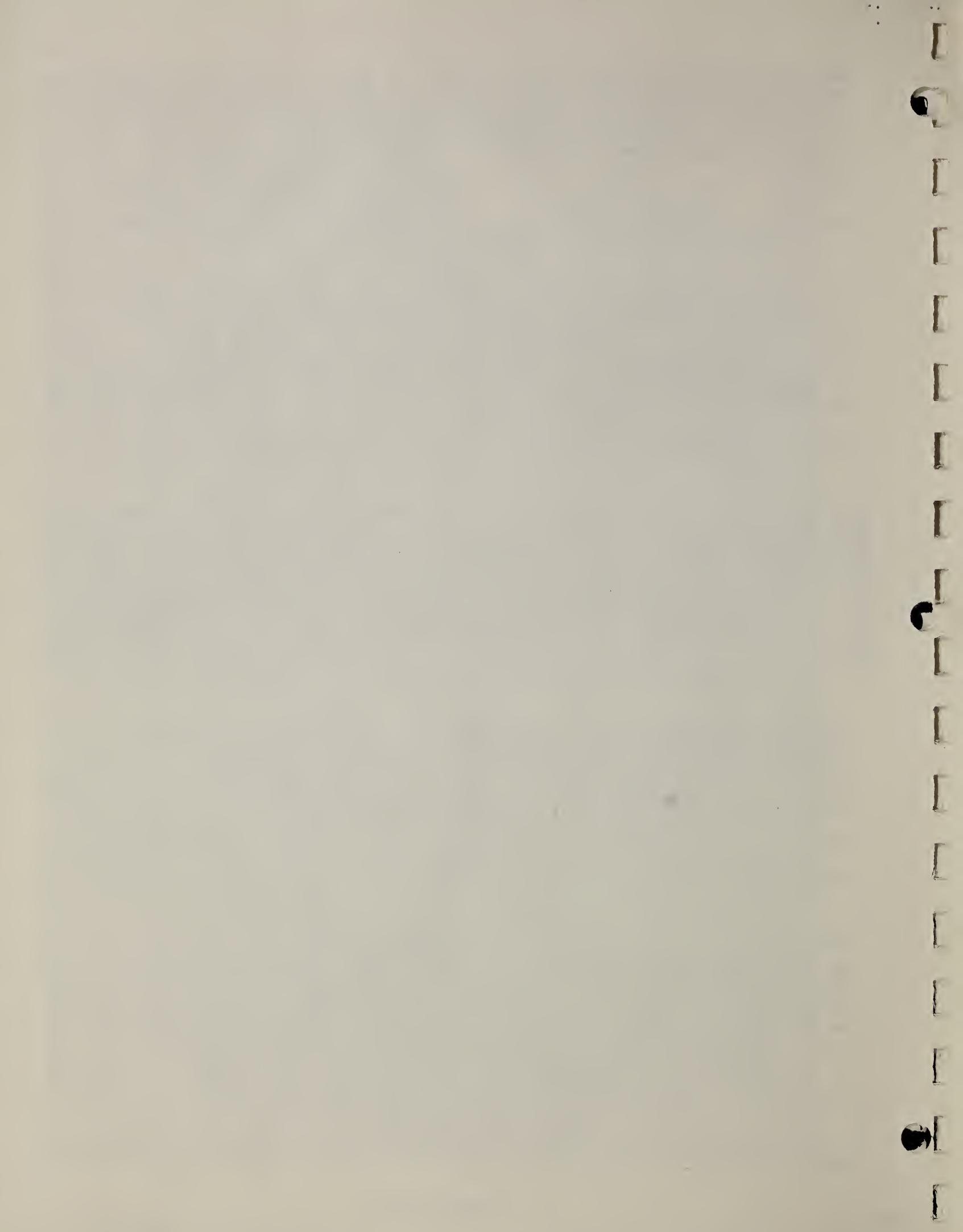


Figure 8b



VOLTAGE-CURRENT CHARACTERISTIC
of
120-watt, PAR 64, 6-volt,
(20-ampere) lamps

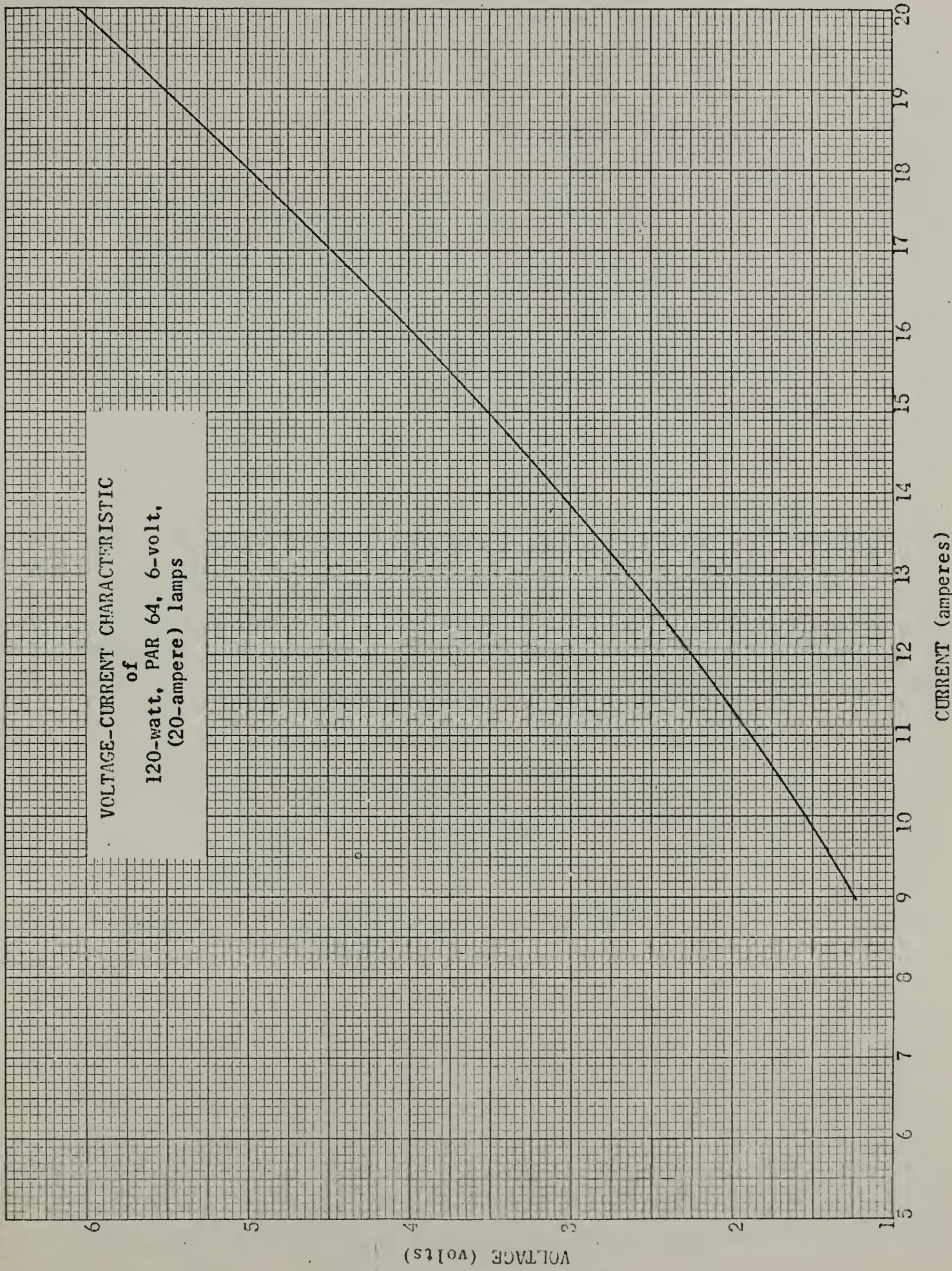


Figure 8c

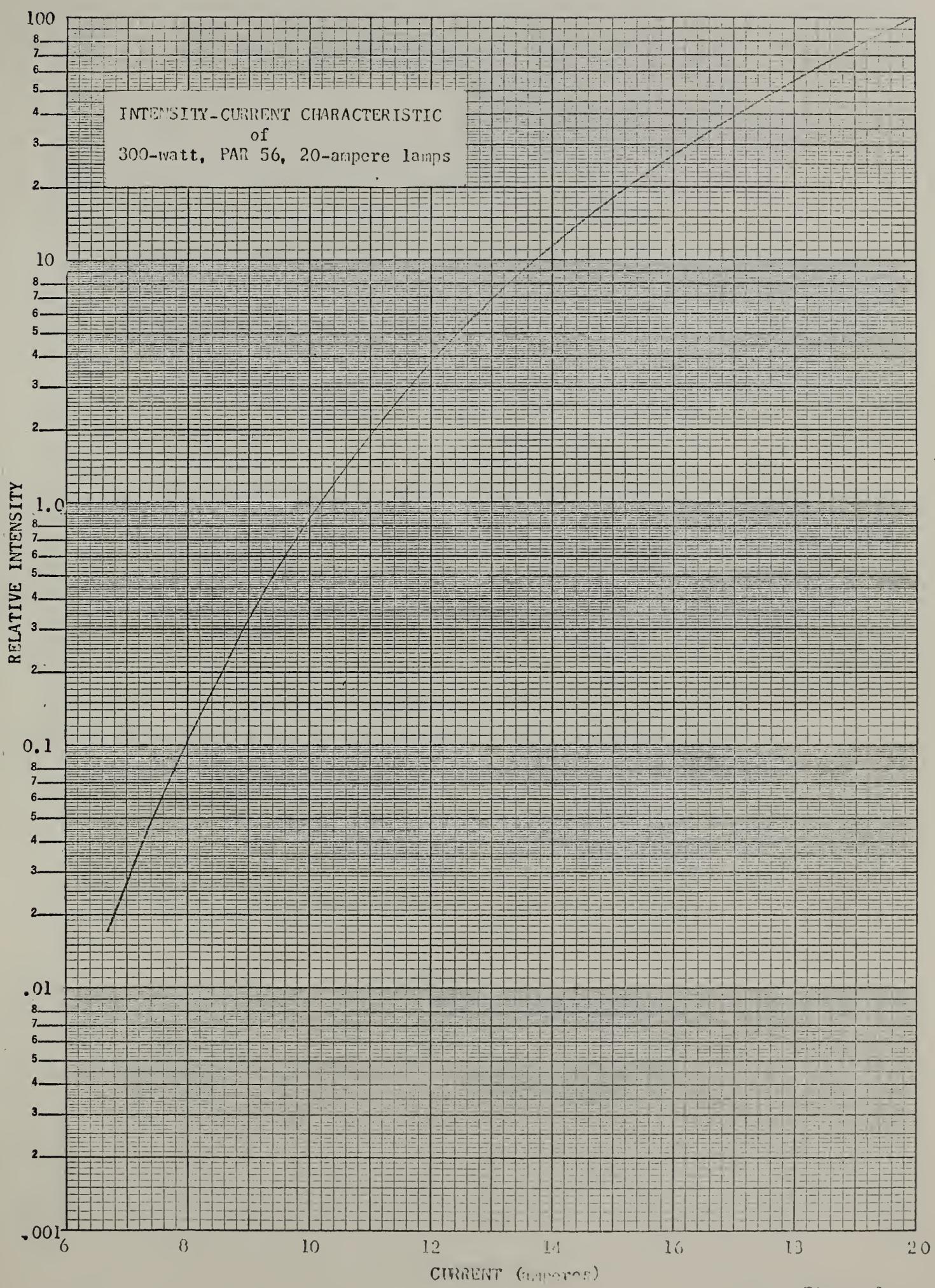
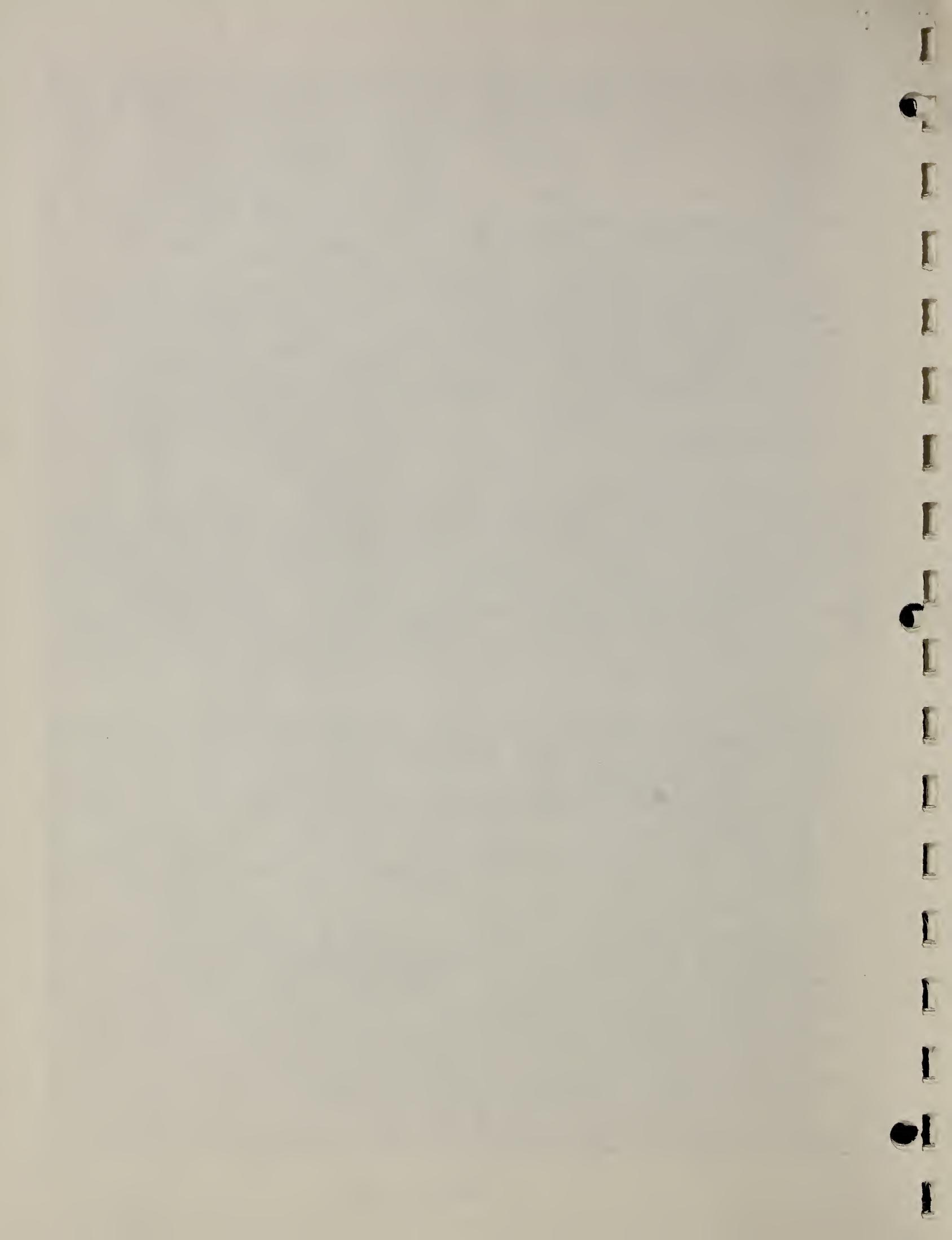


Figure 9a



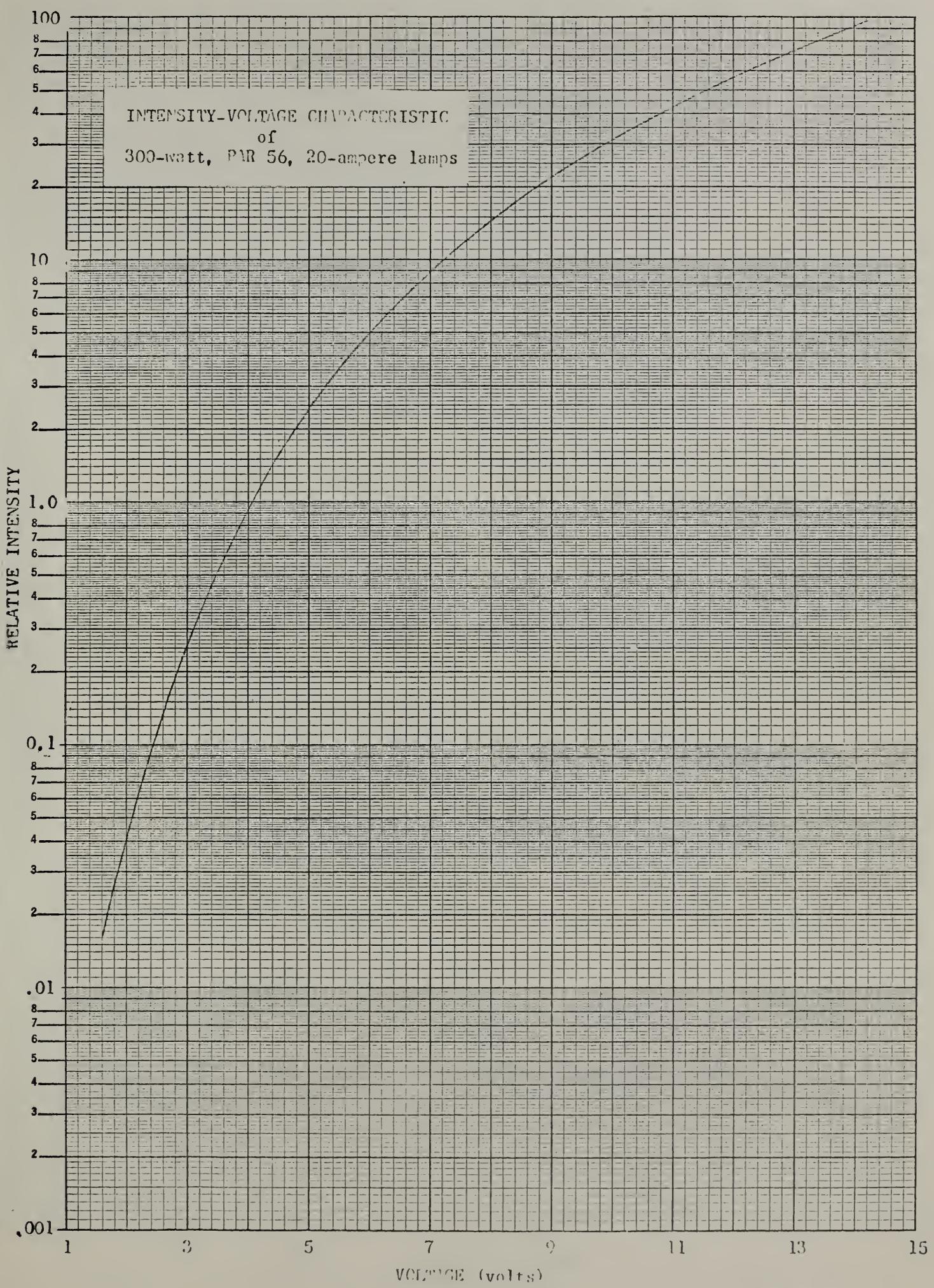
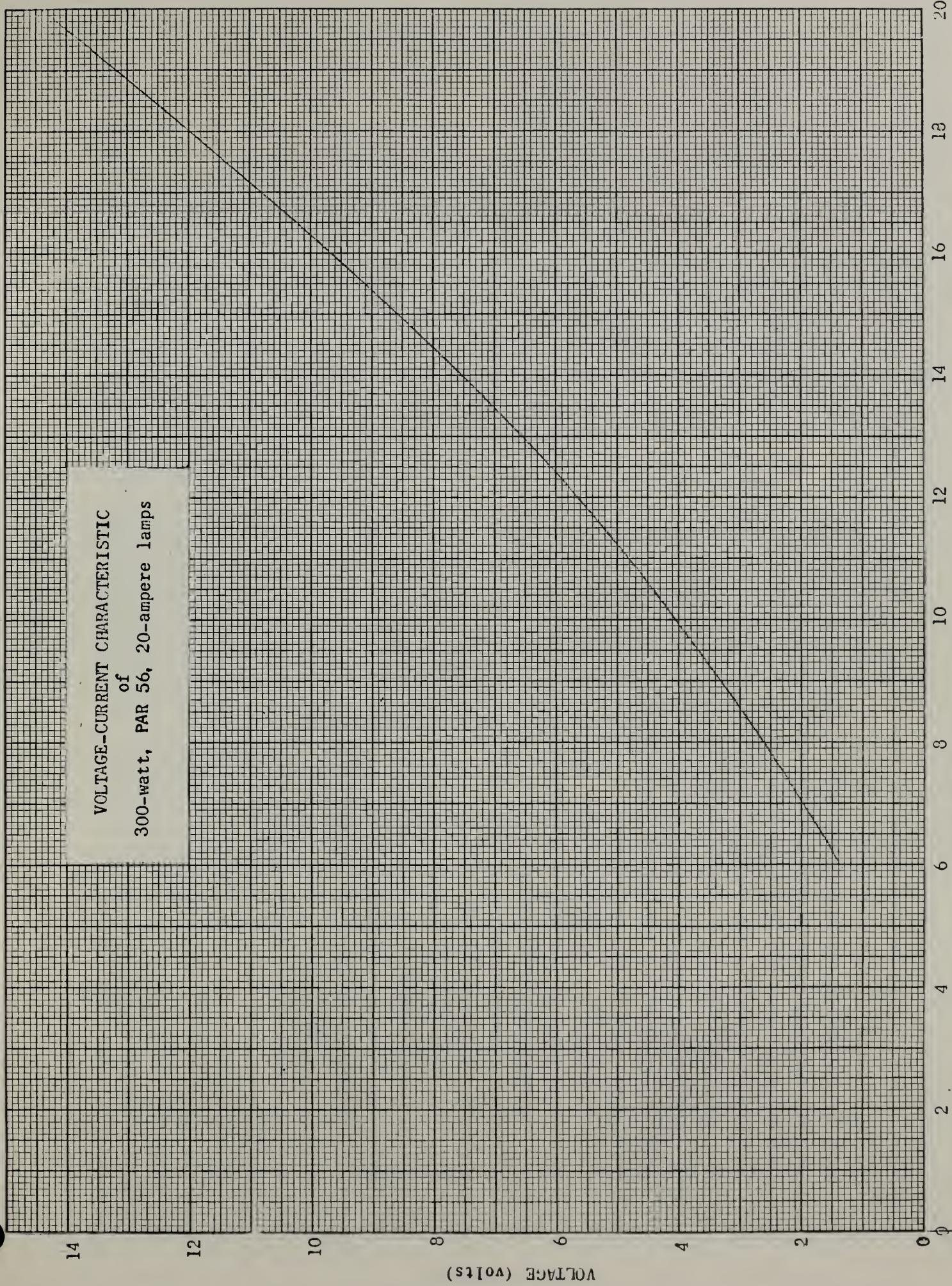
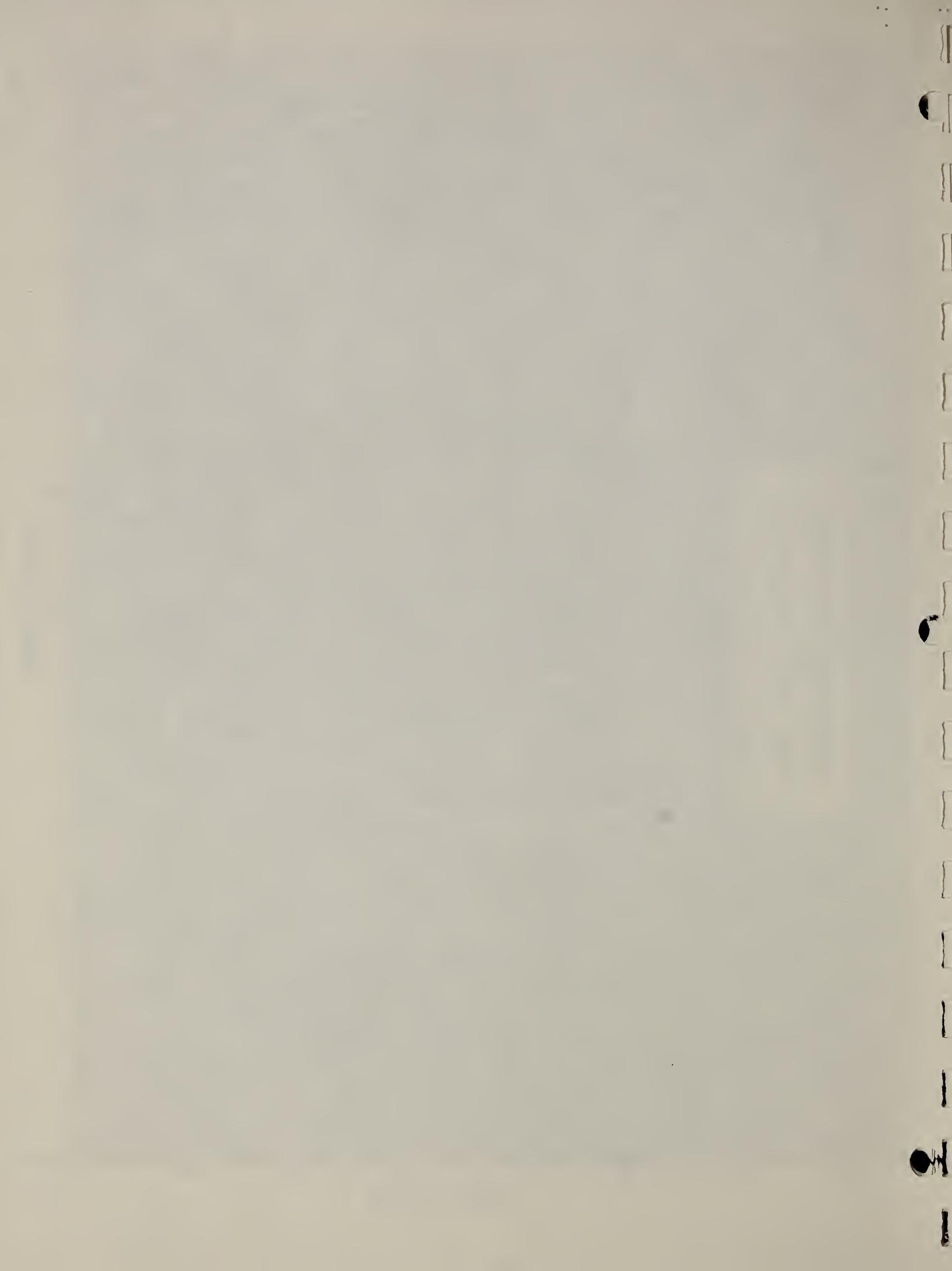


Figure 9b

Figure 9c





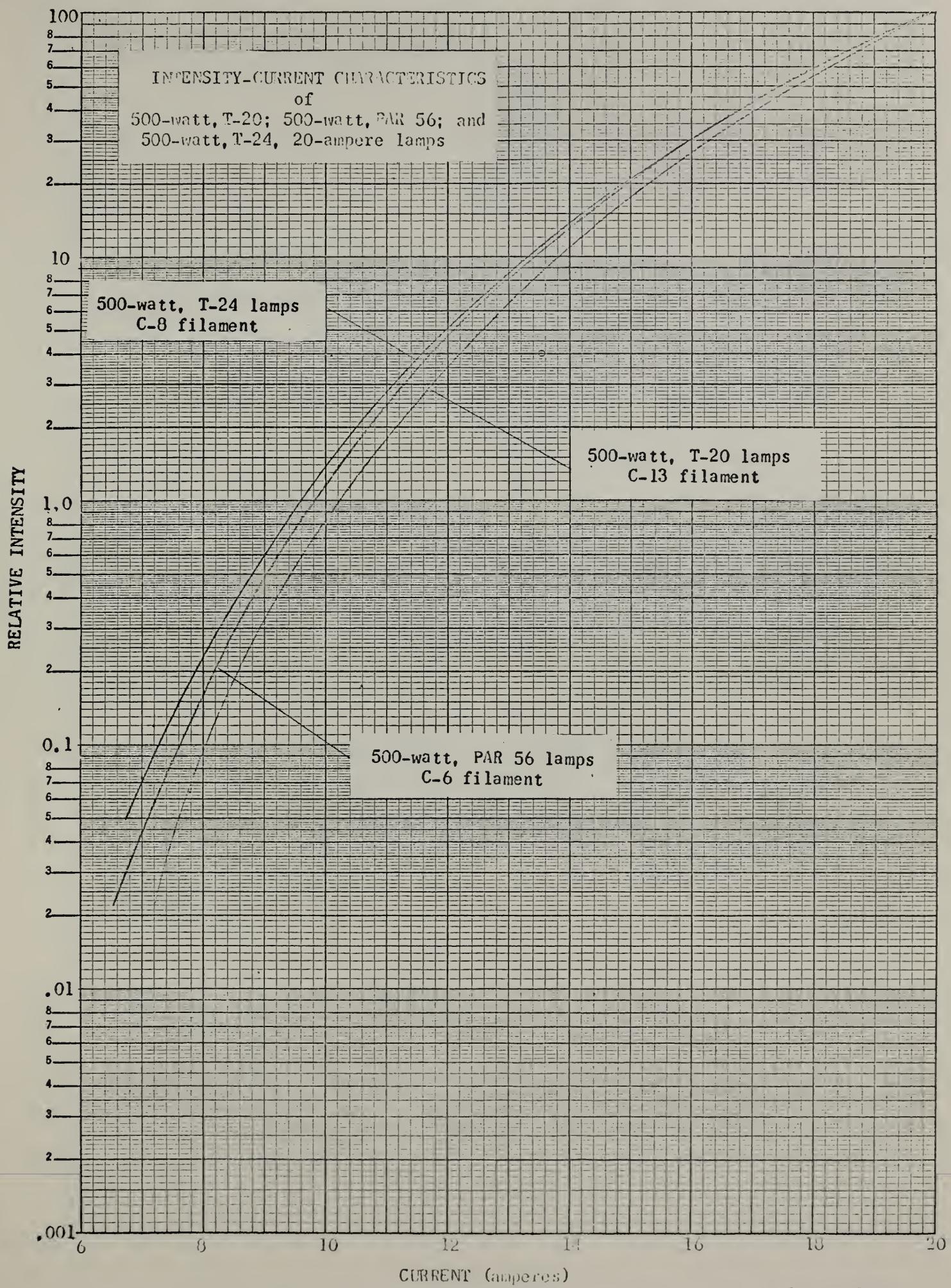


Figure 10a

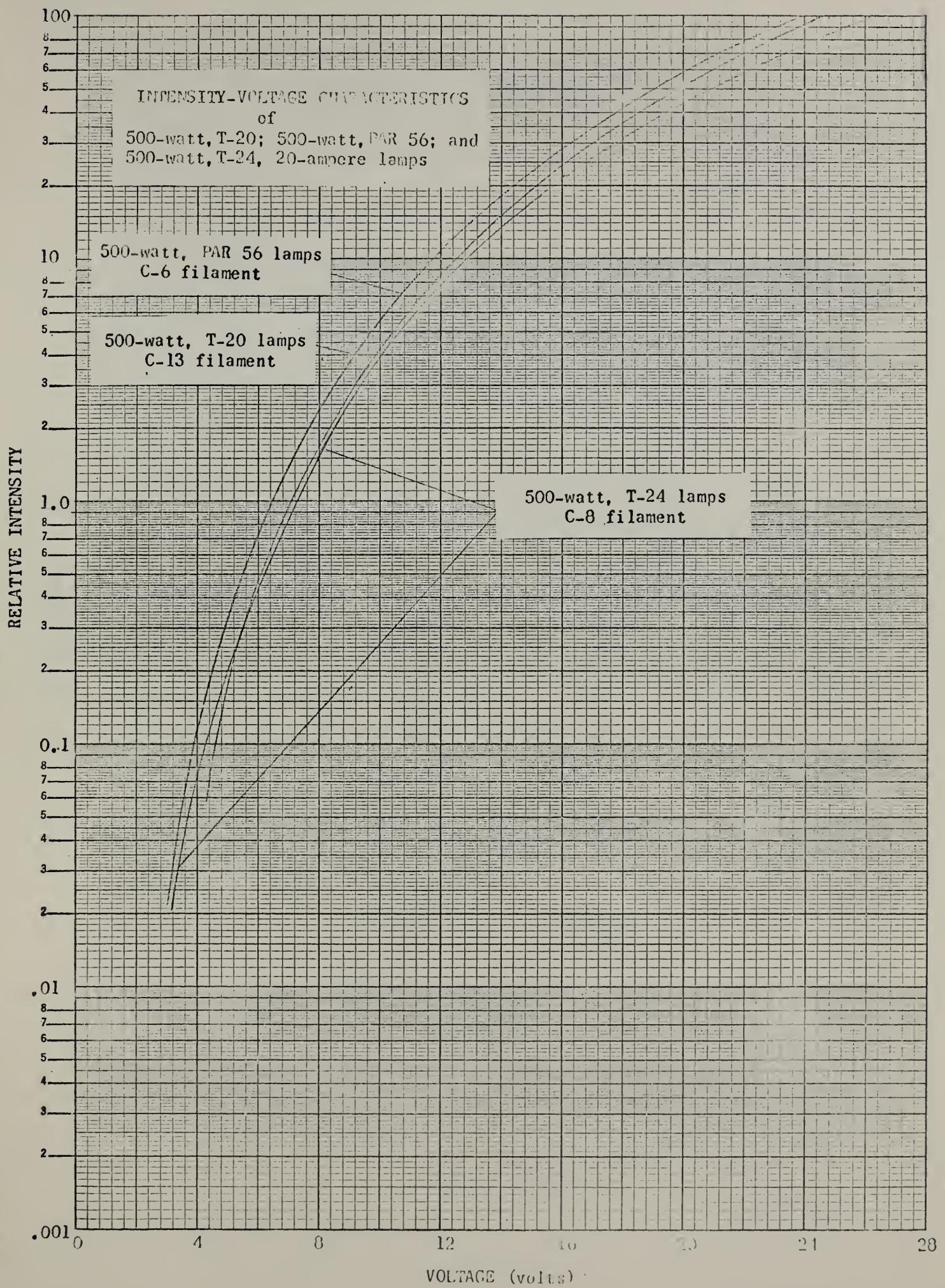
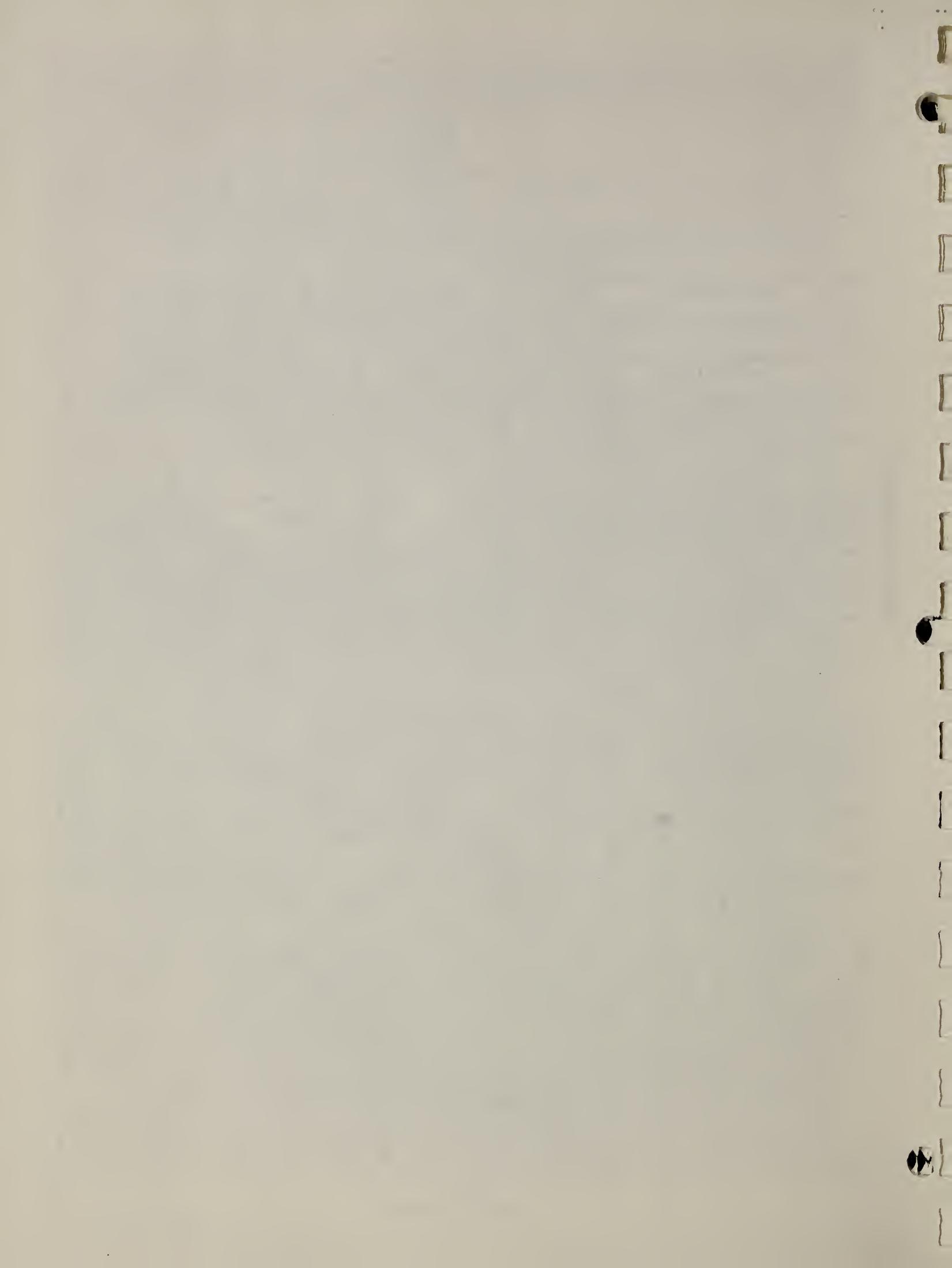


Figure 10b



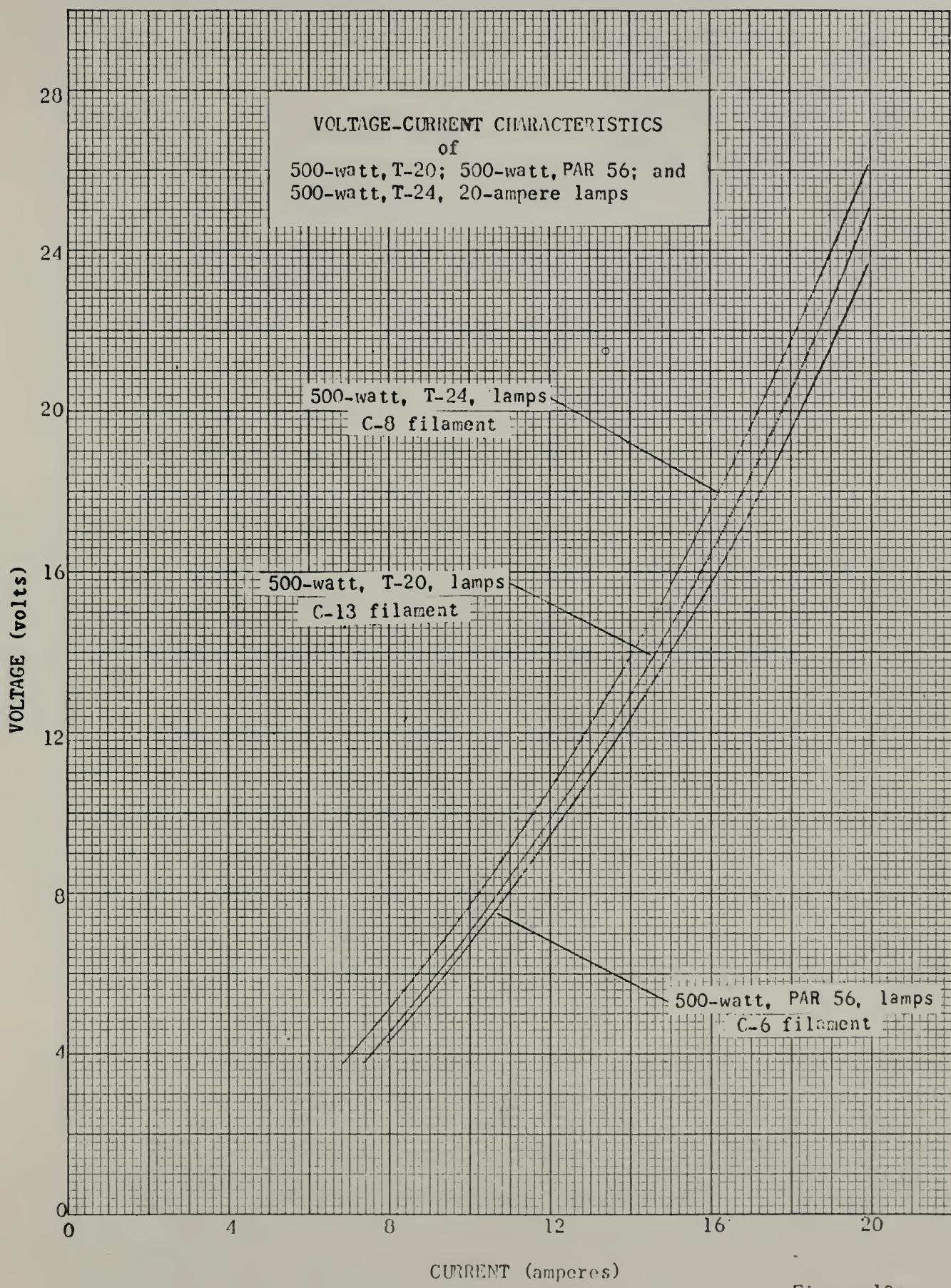


Figure 10c

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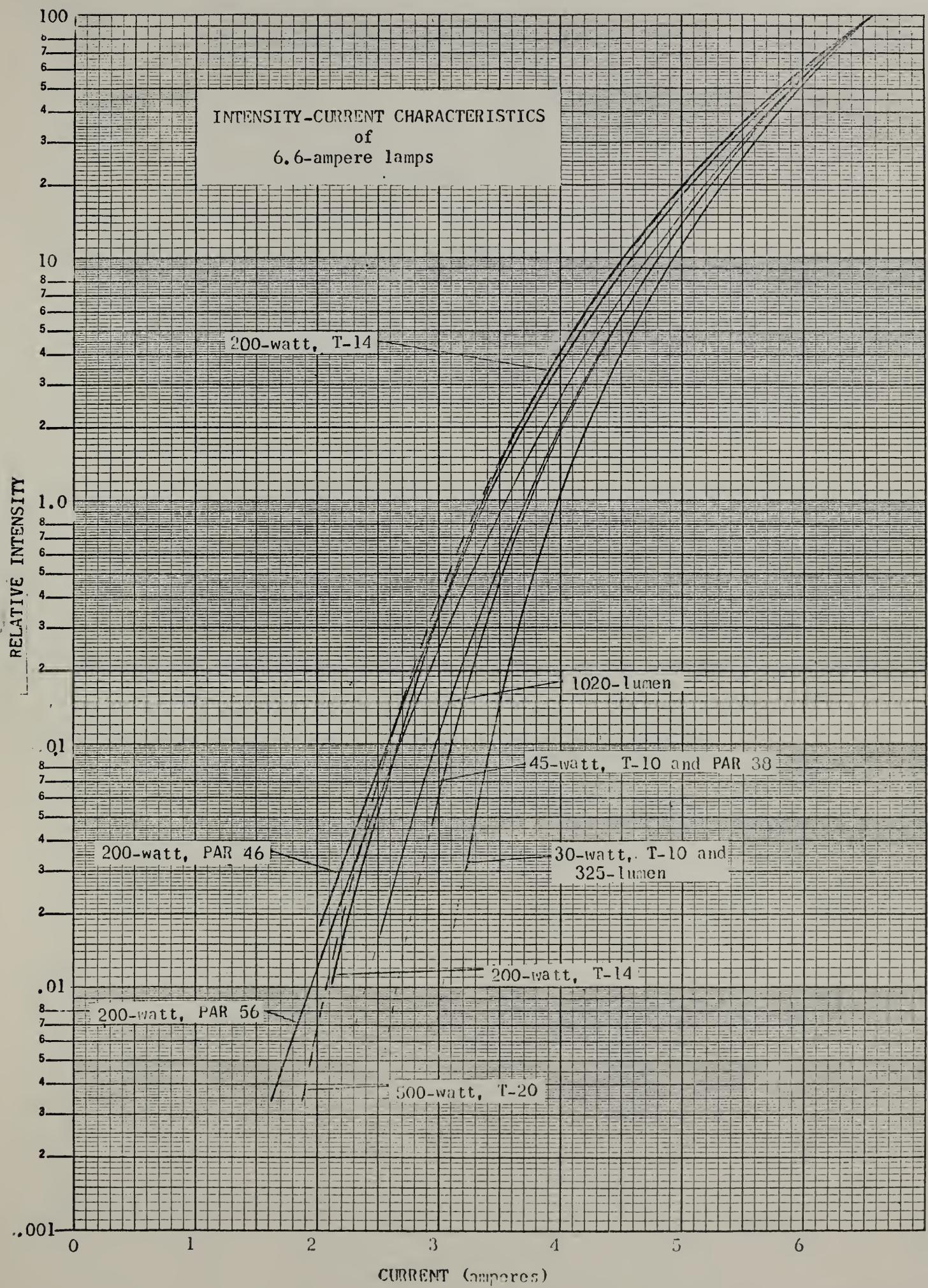
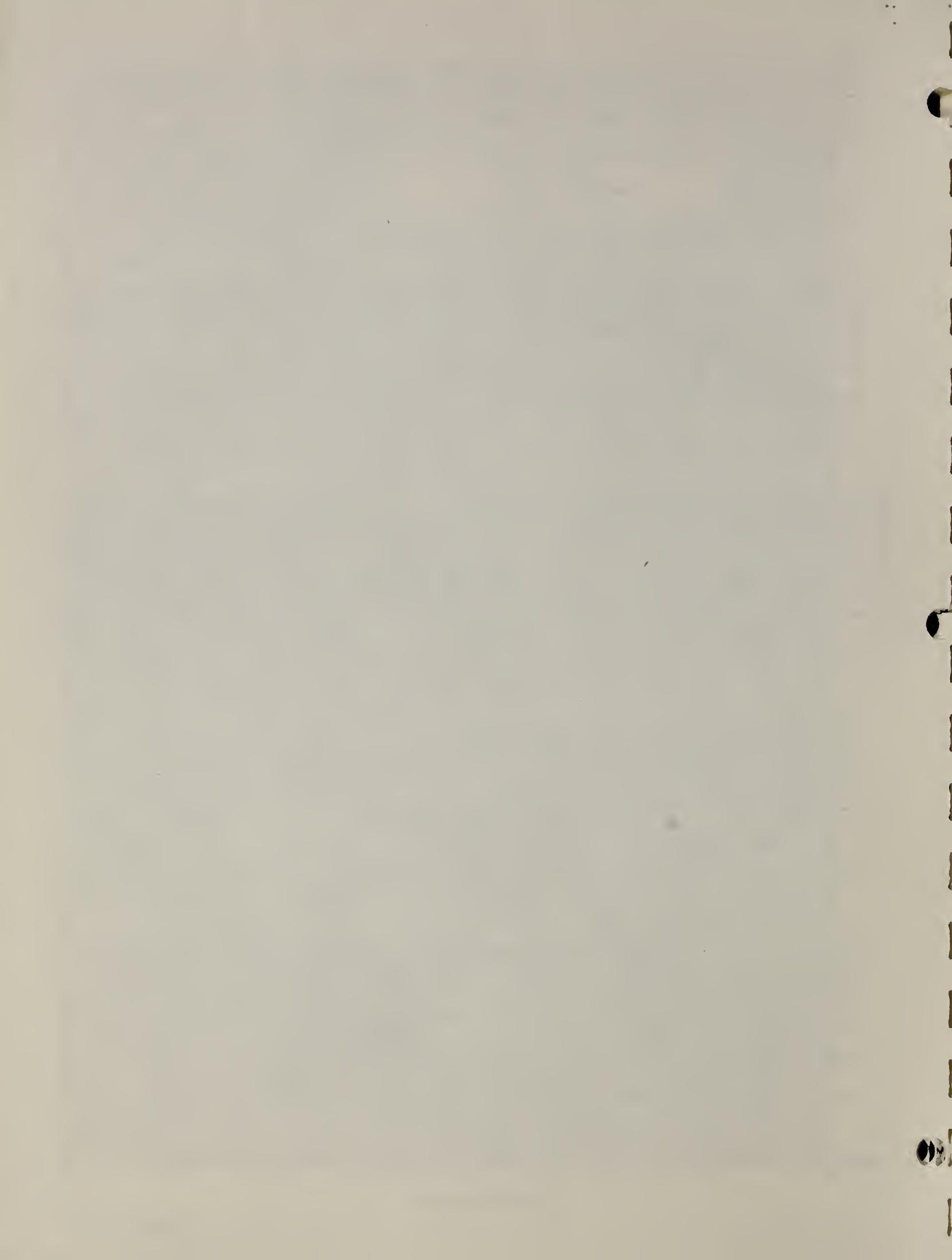


Figure 11



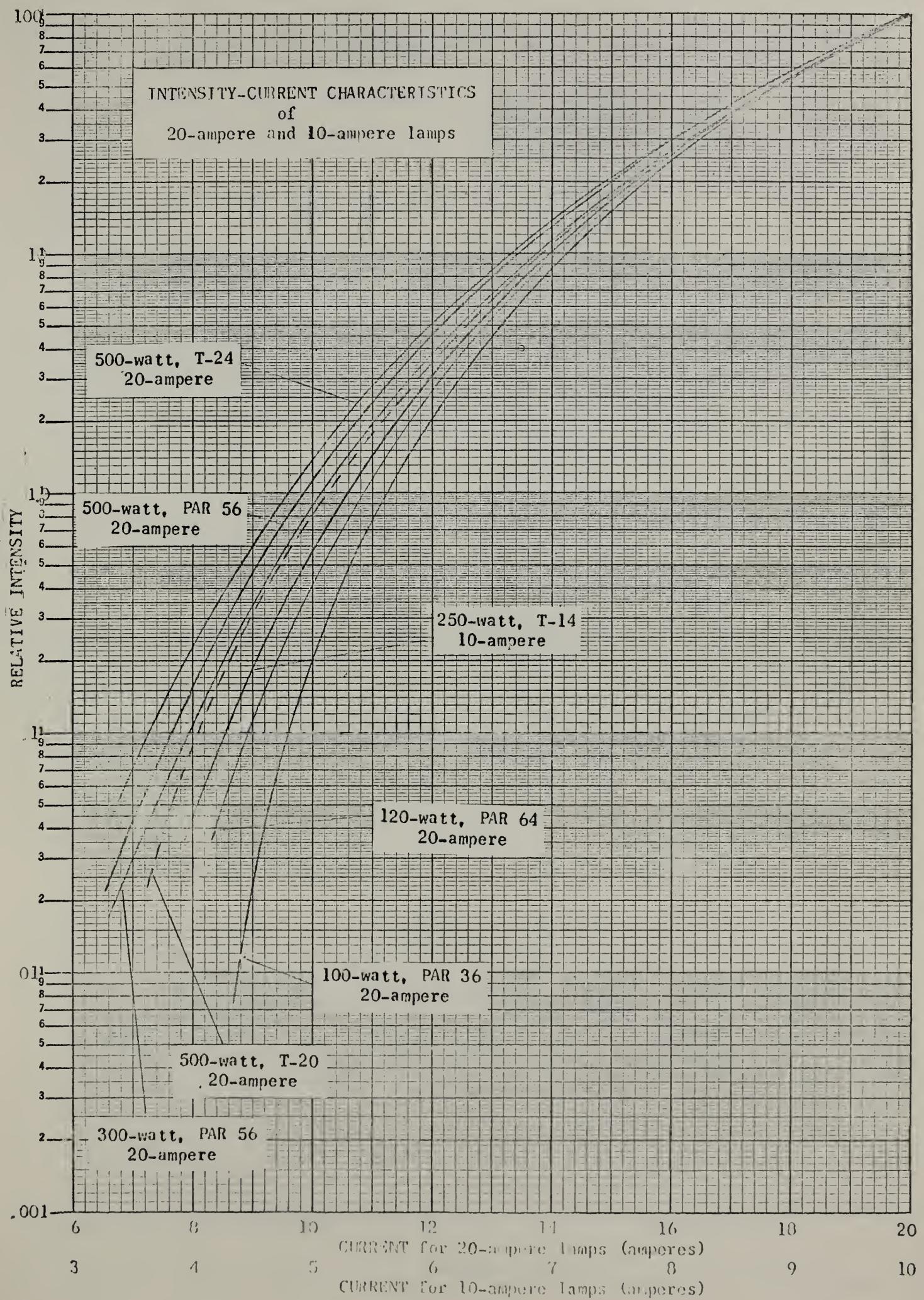
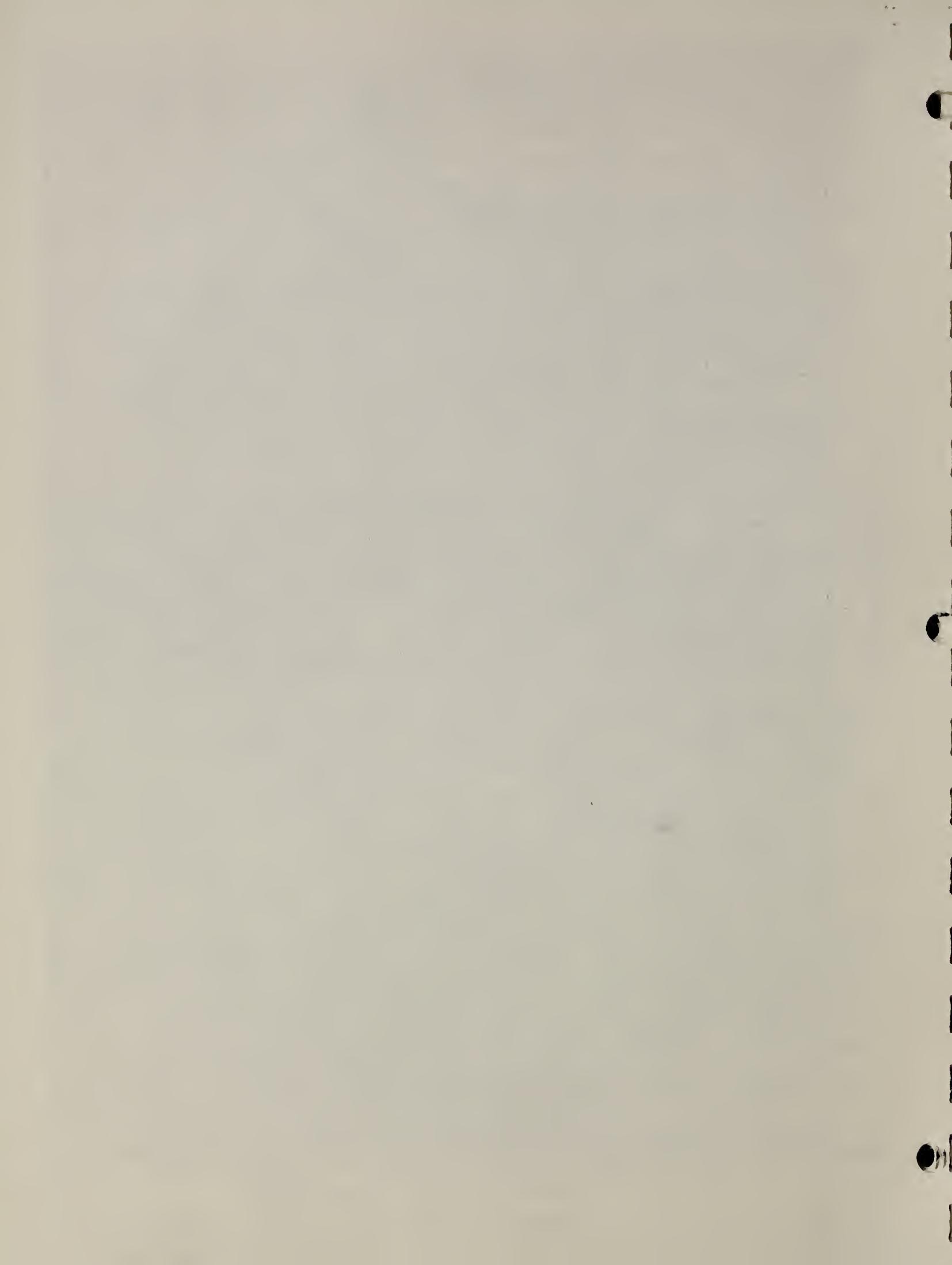


Figure 12



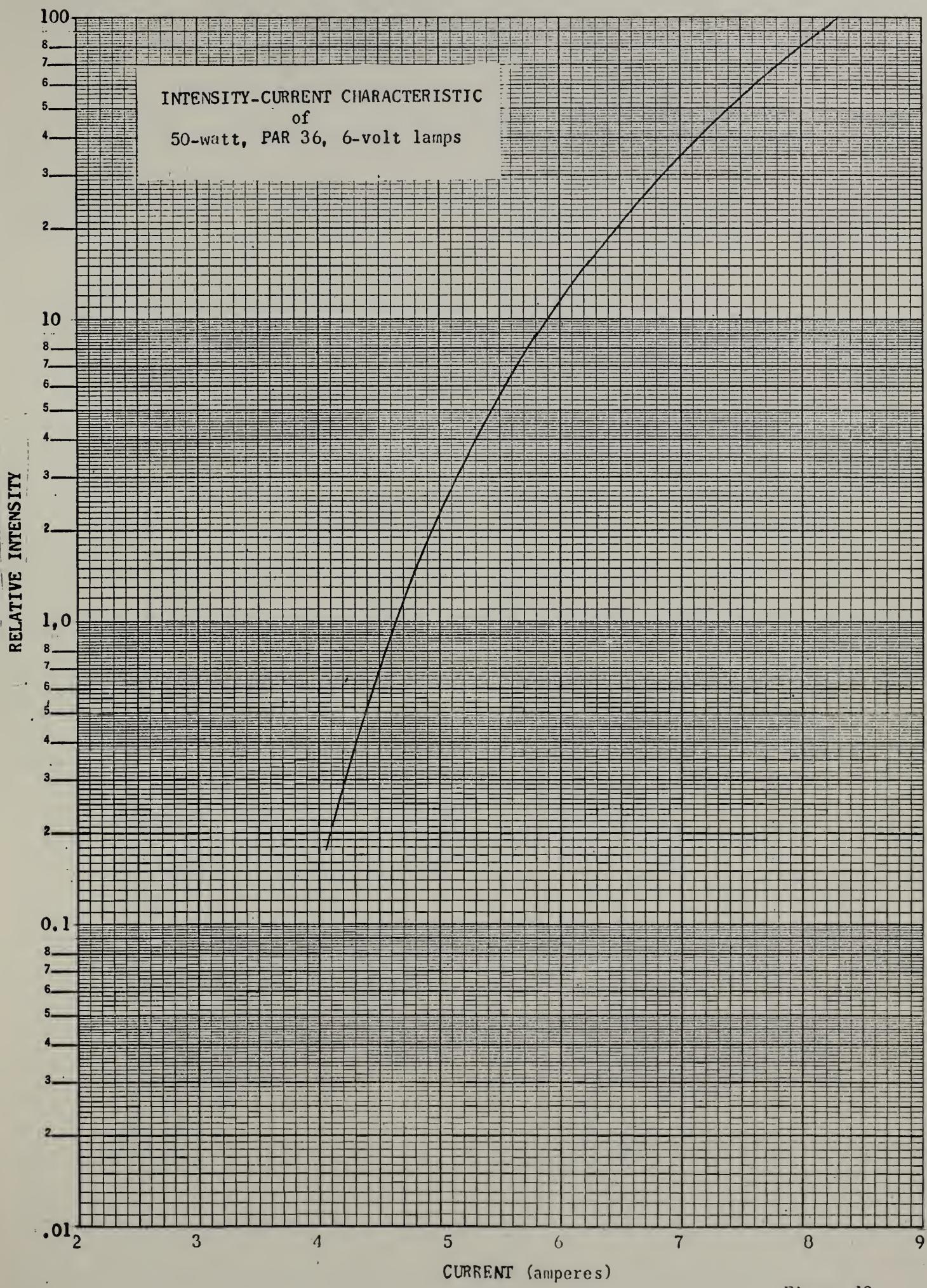
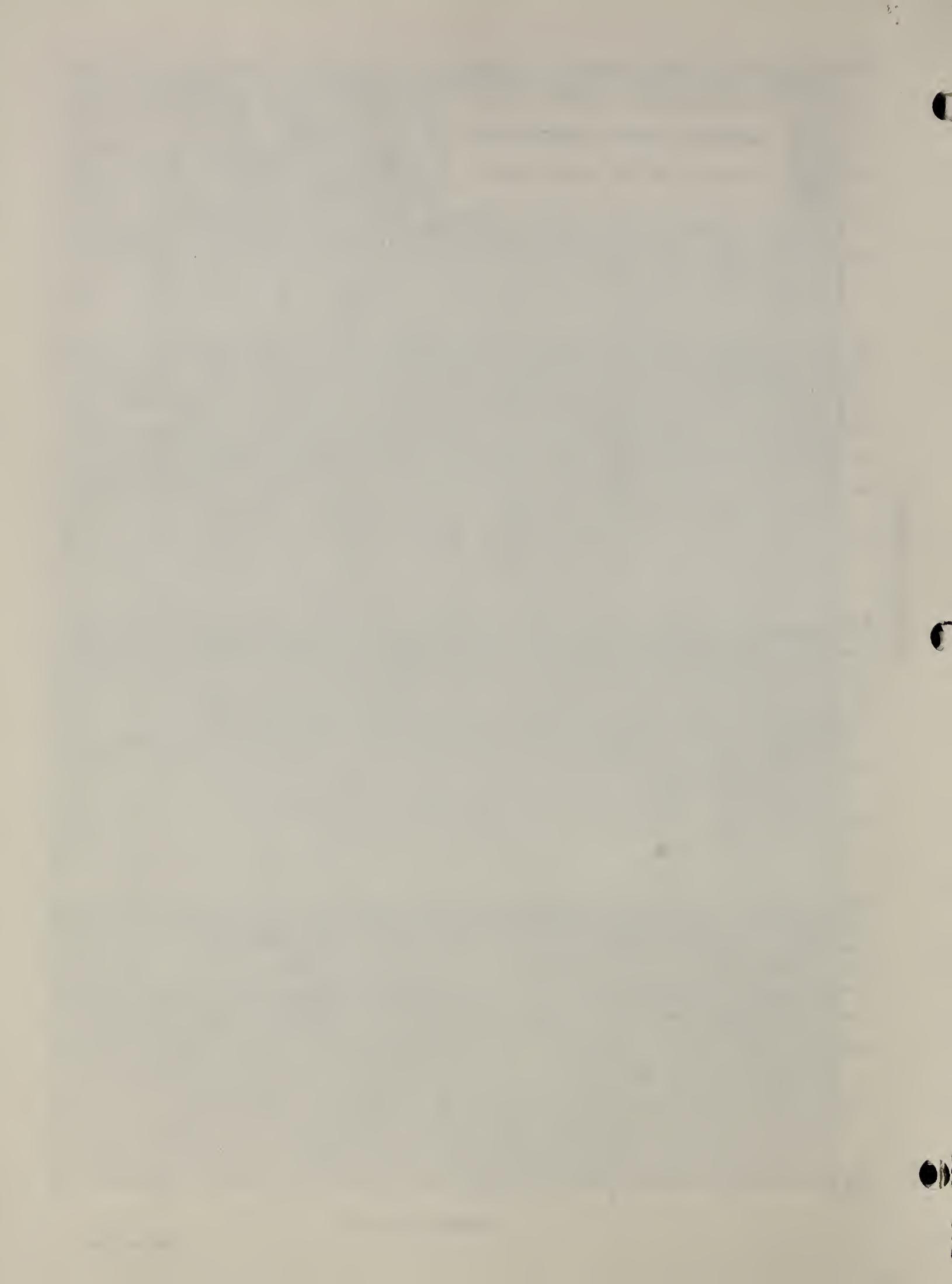


Figure 13a



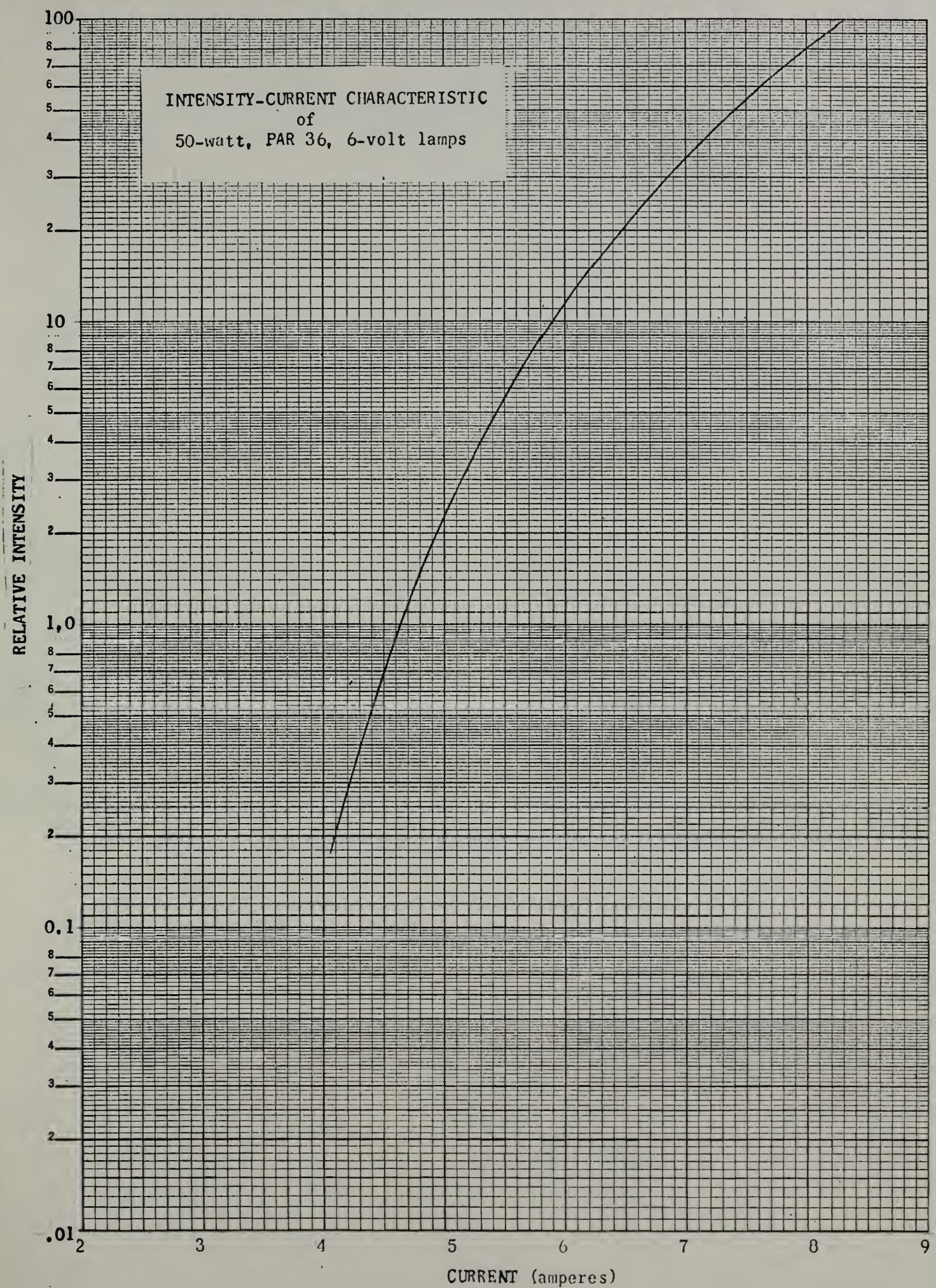


Figure 13a

1

Q

11

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Q

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Q1

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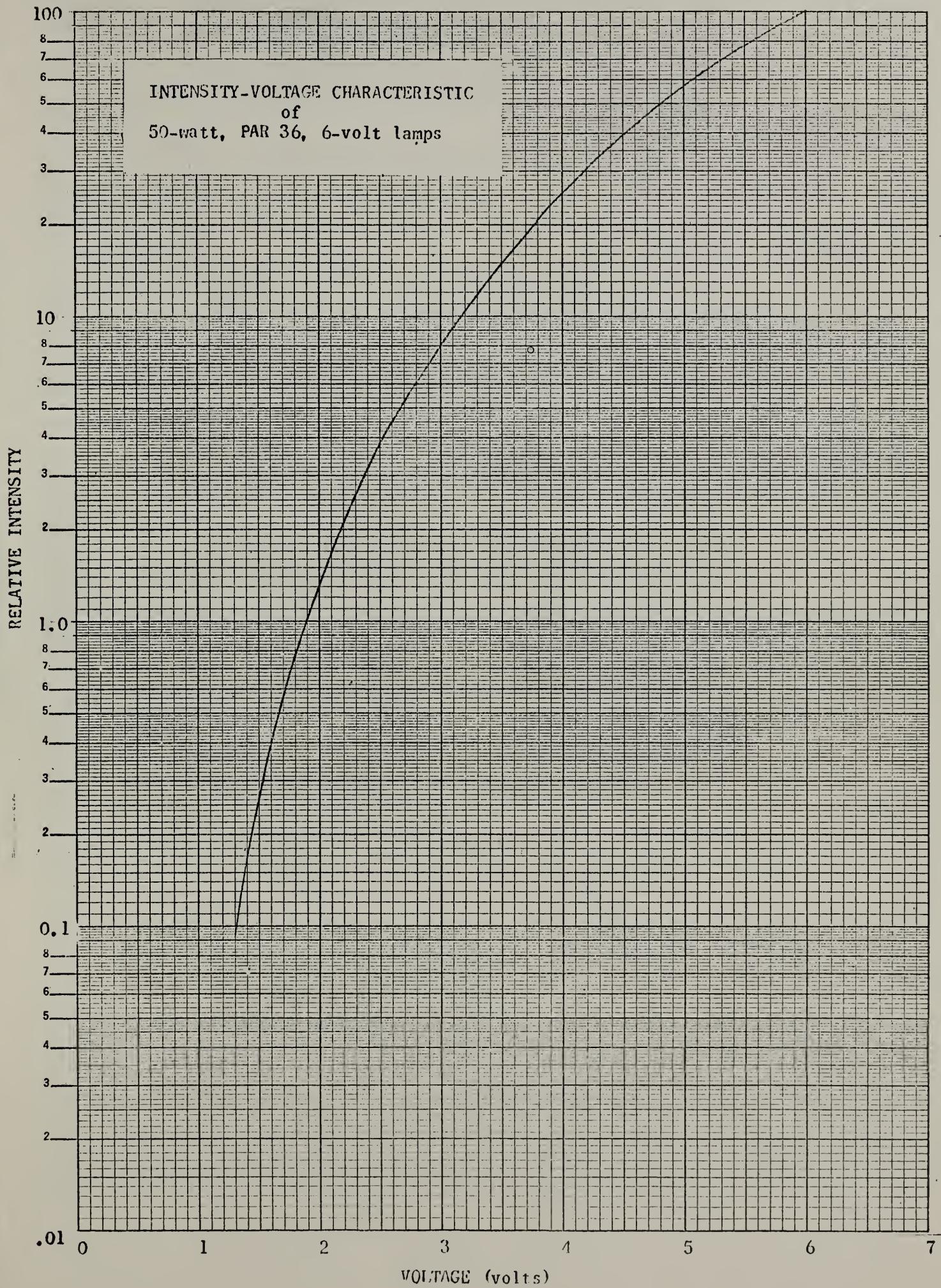


Figure 13b



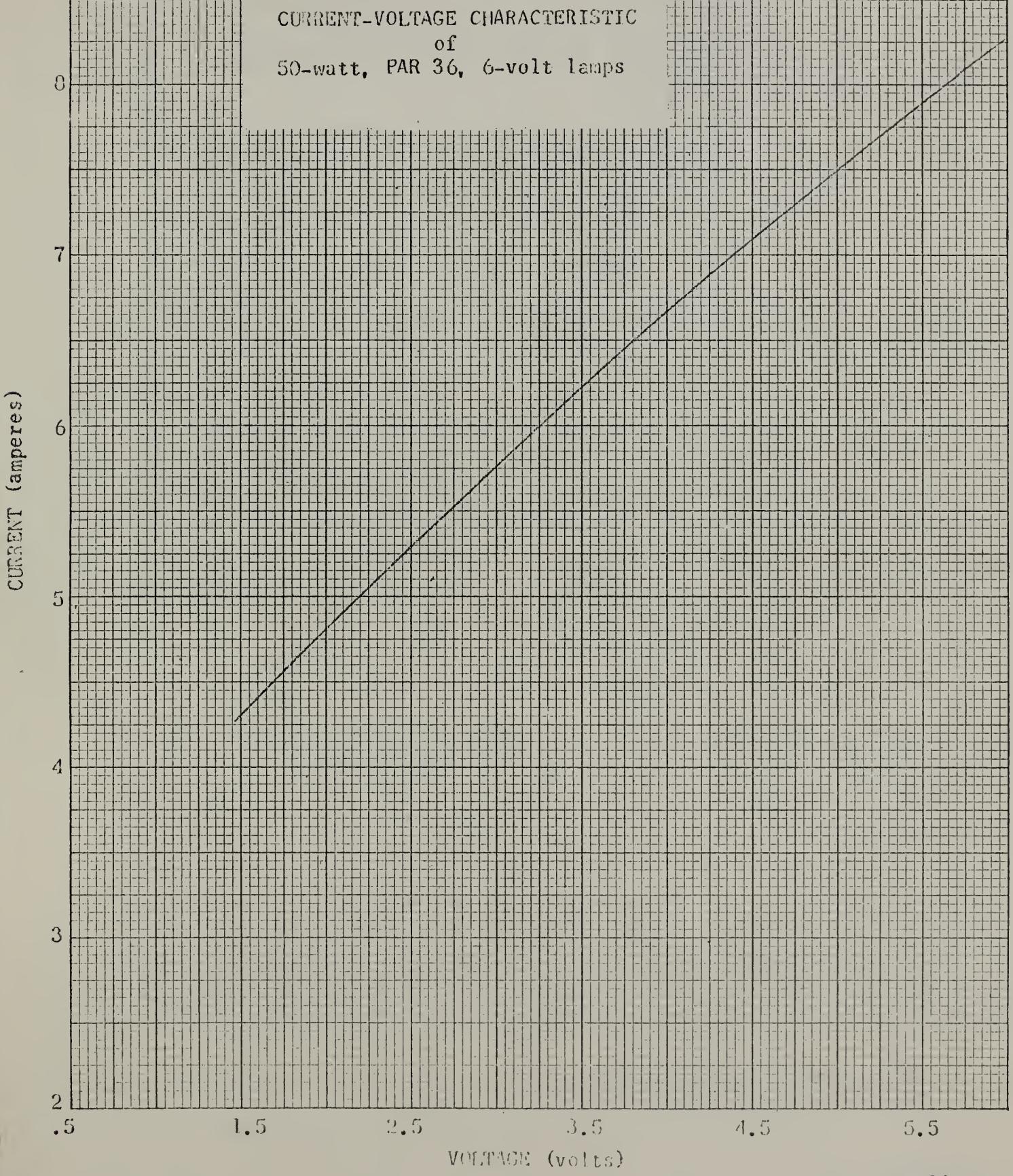
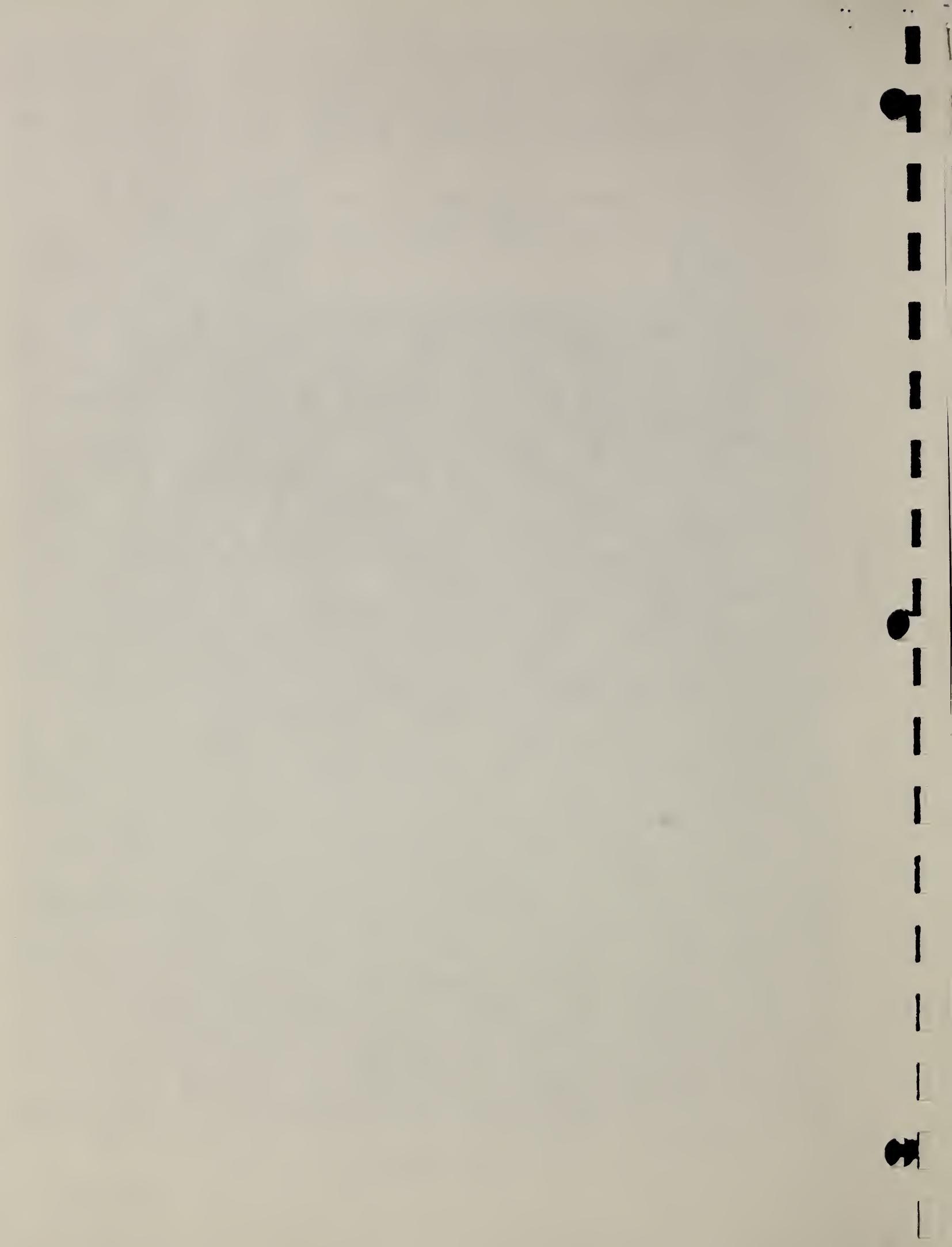


Figure 13c



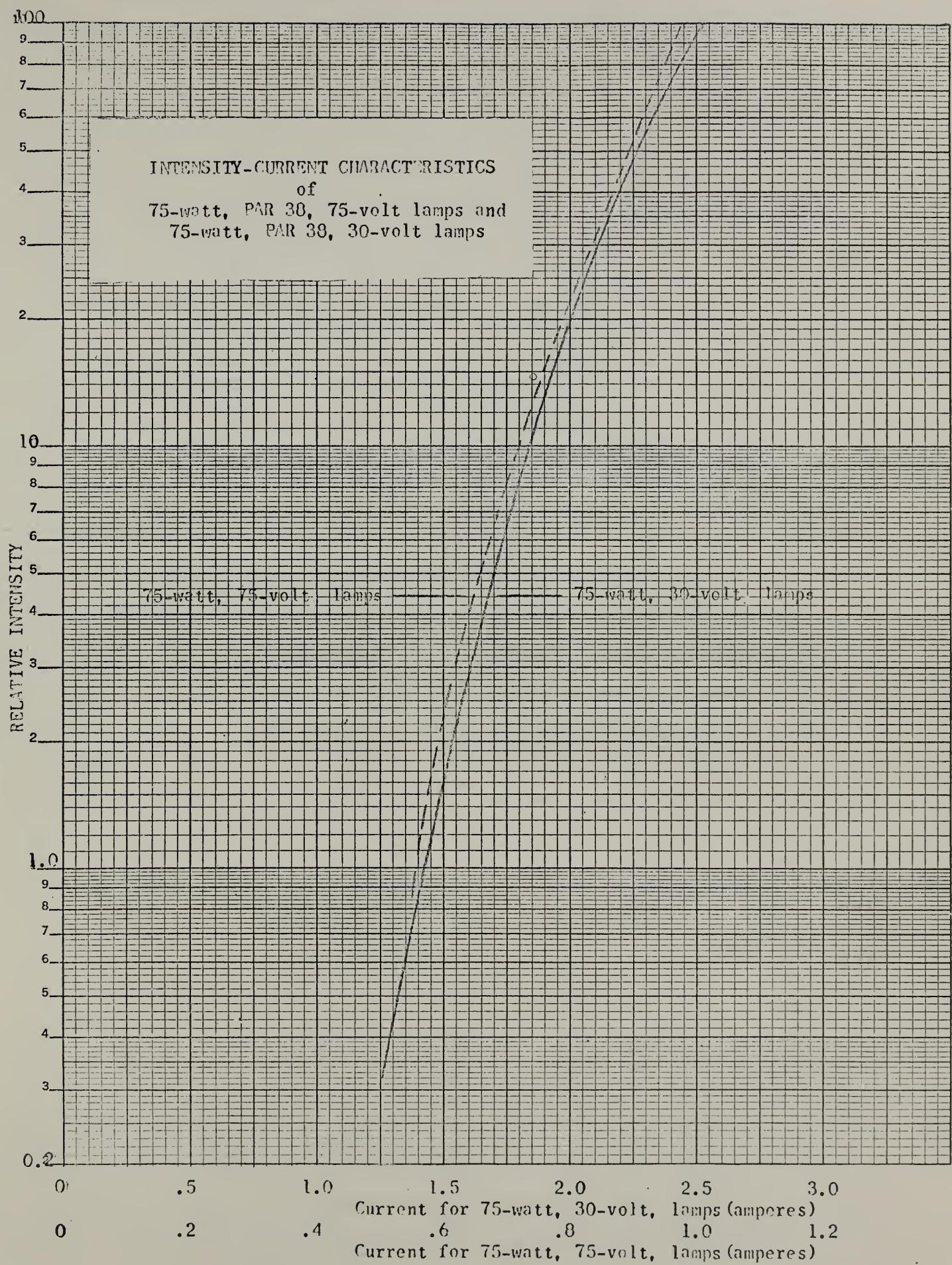
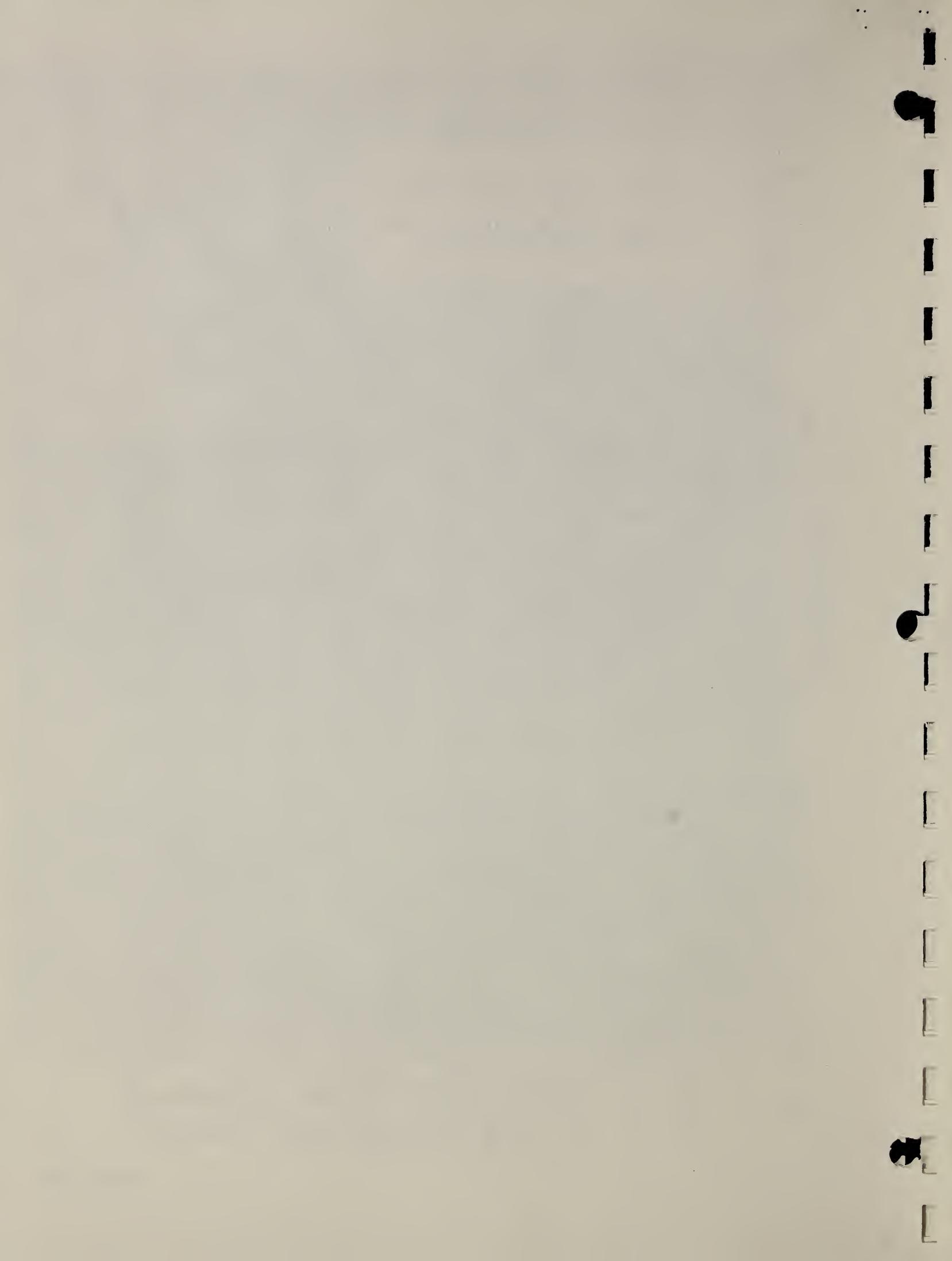


Figure 14a



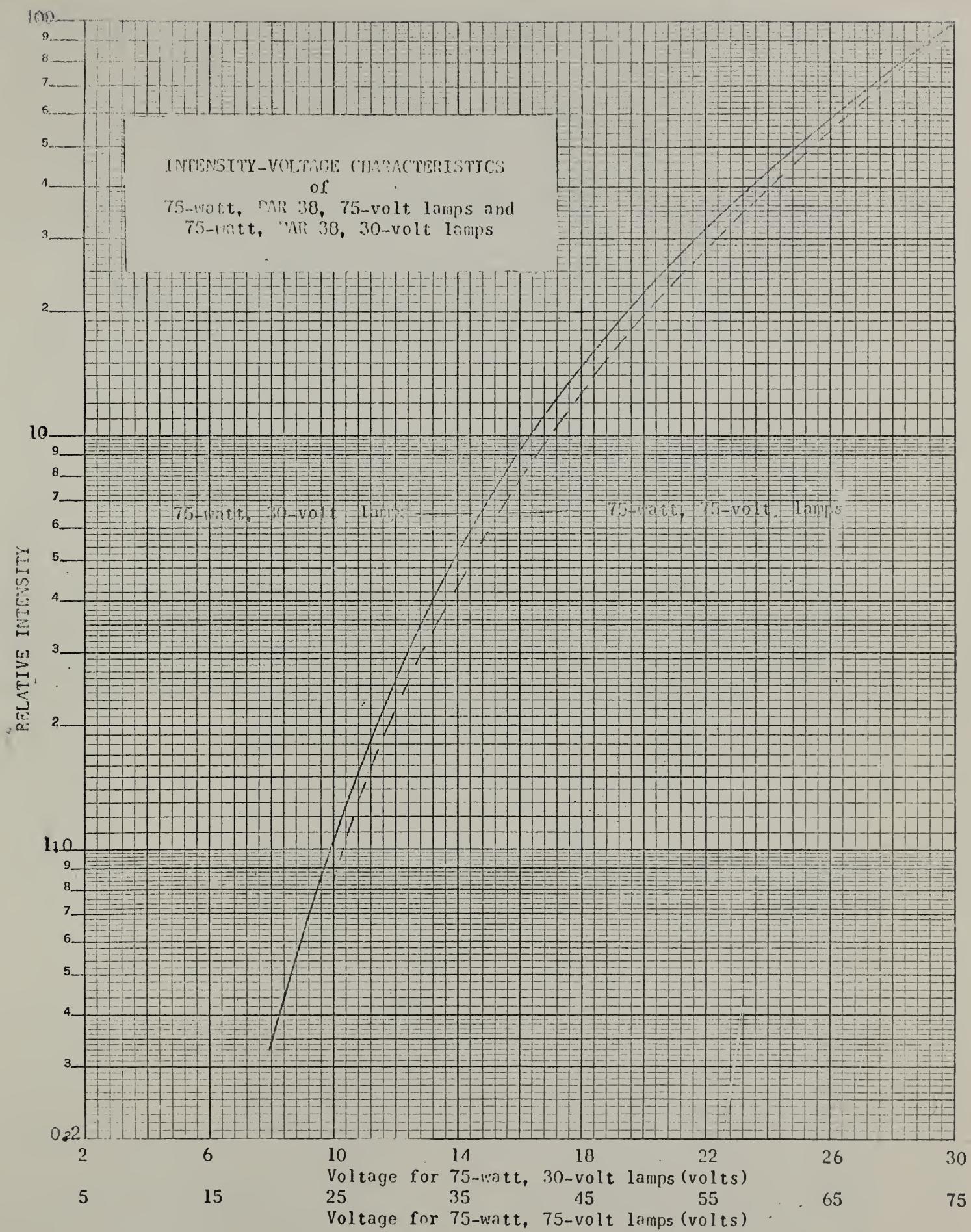


Figure 14b

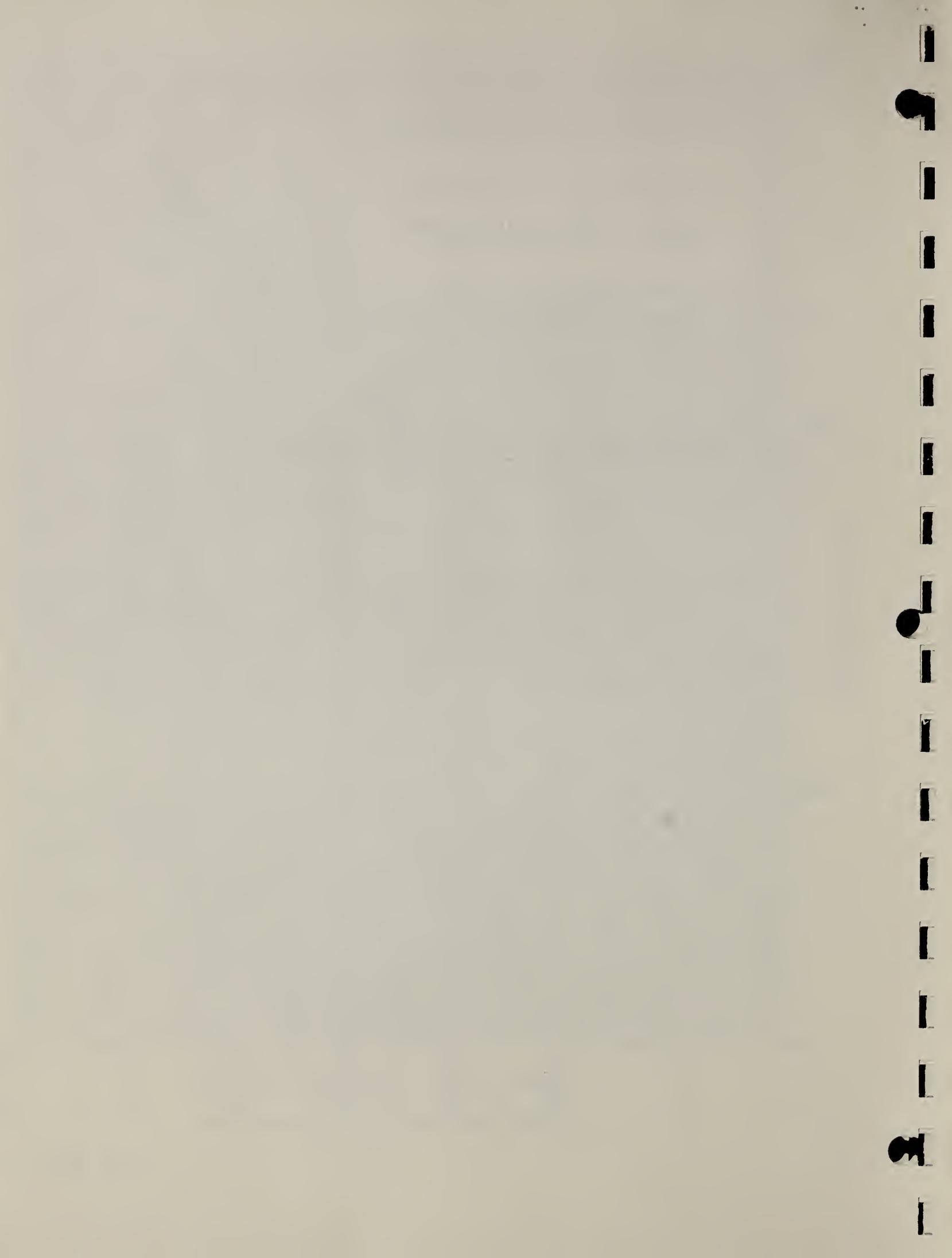
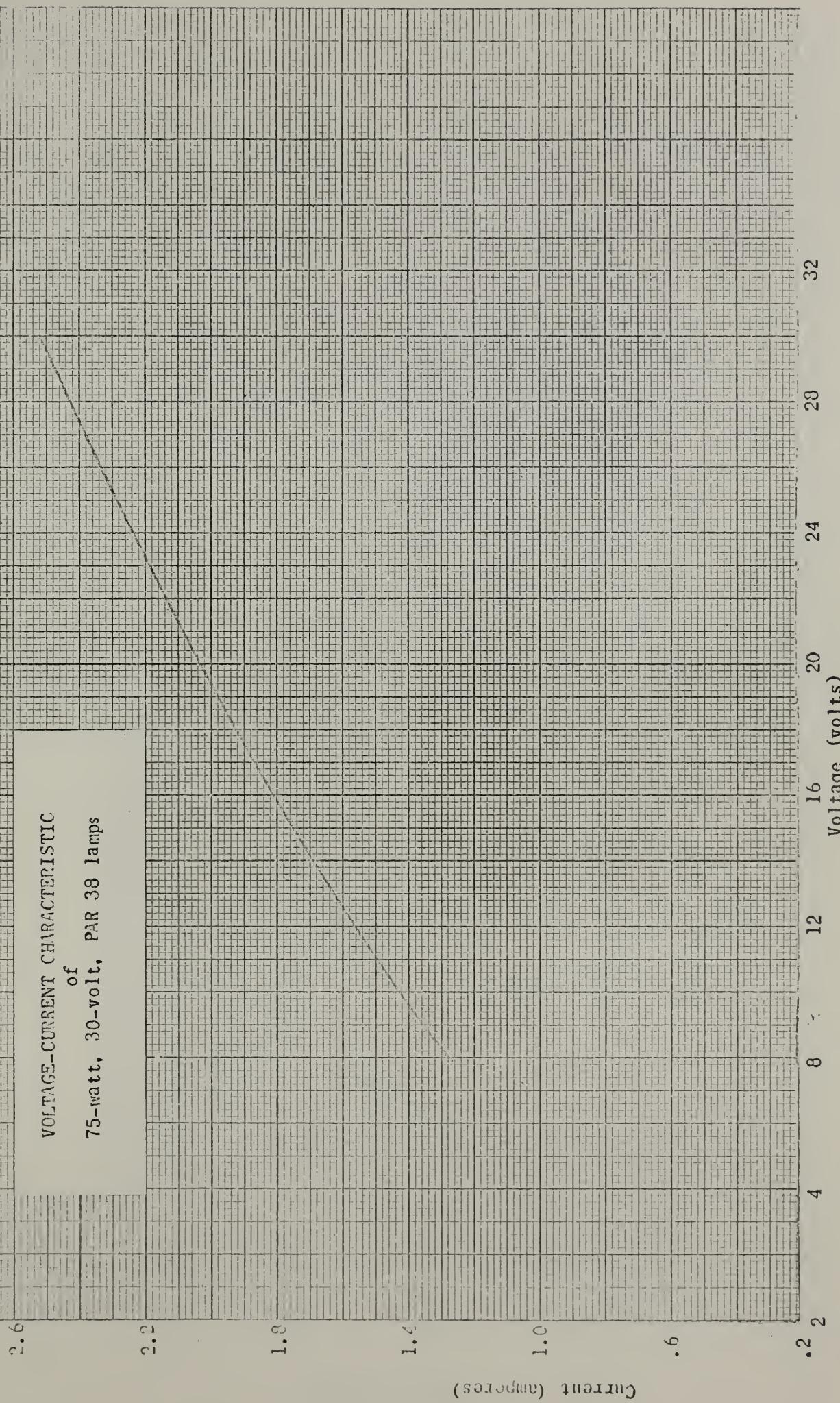
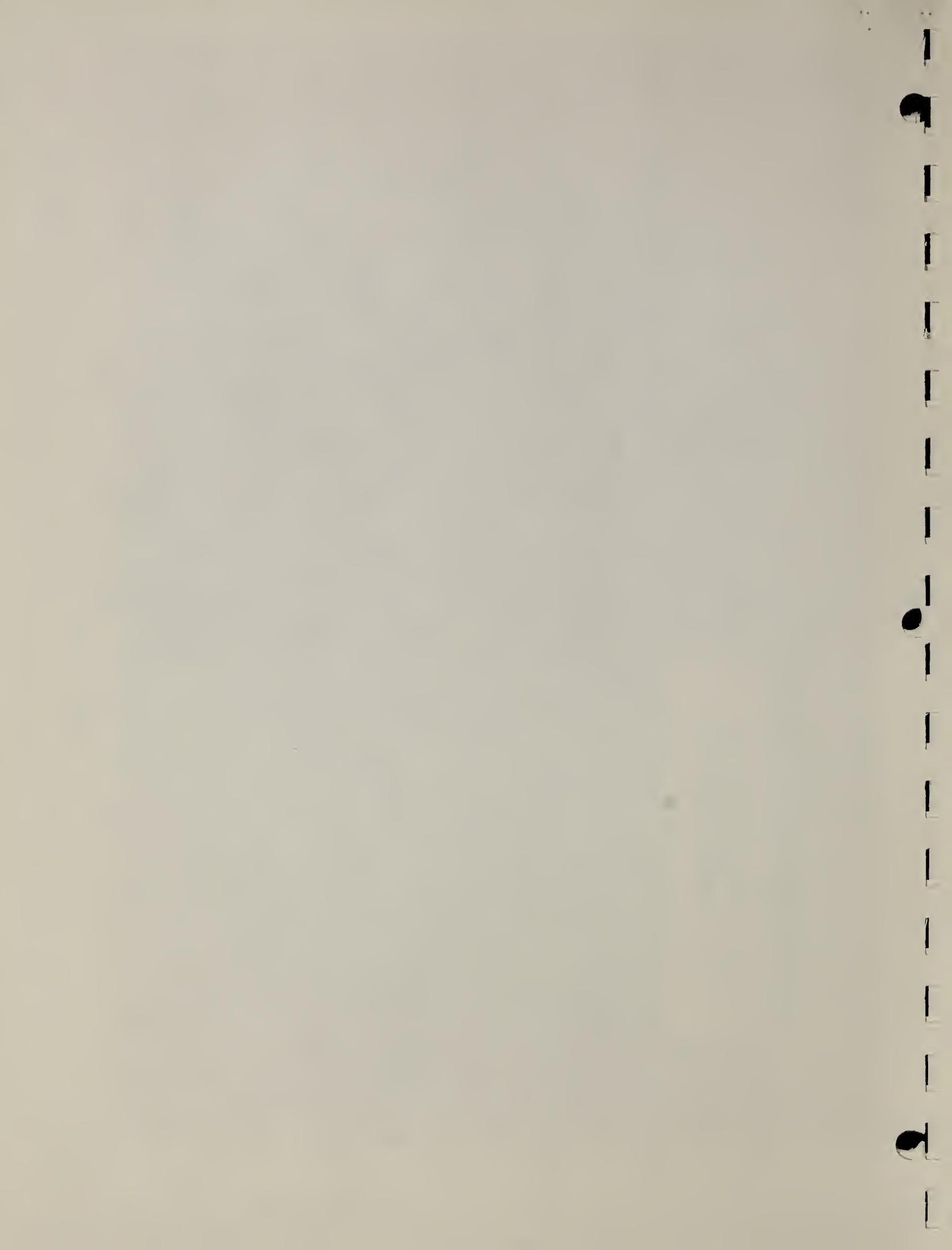


Figure 14c





VOLTAGE-CURRENT CHARACTERISTIC
of
75-watt, 75-volt, PAR 38 lamps

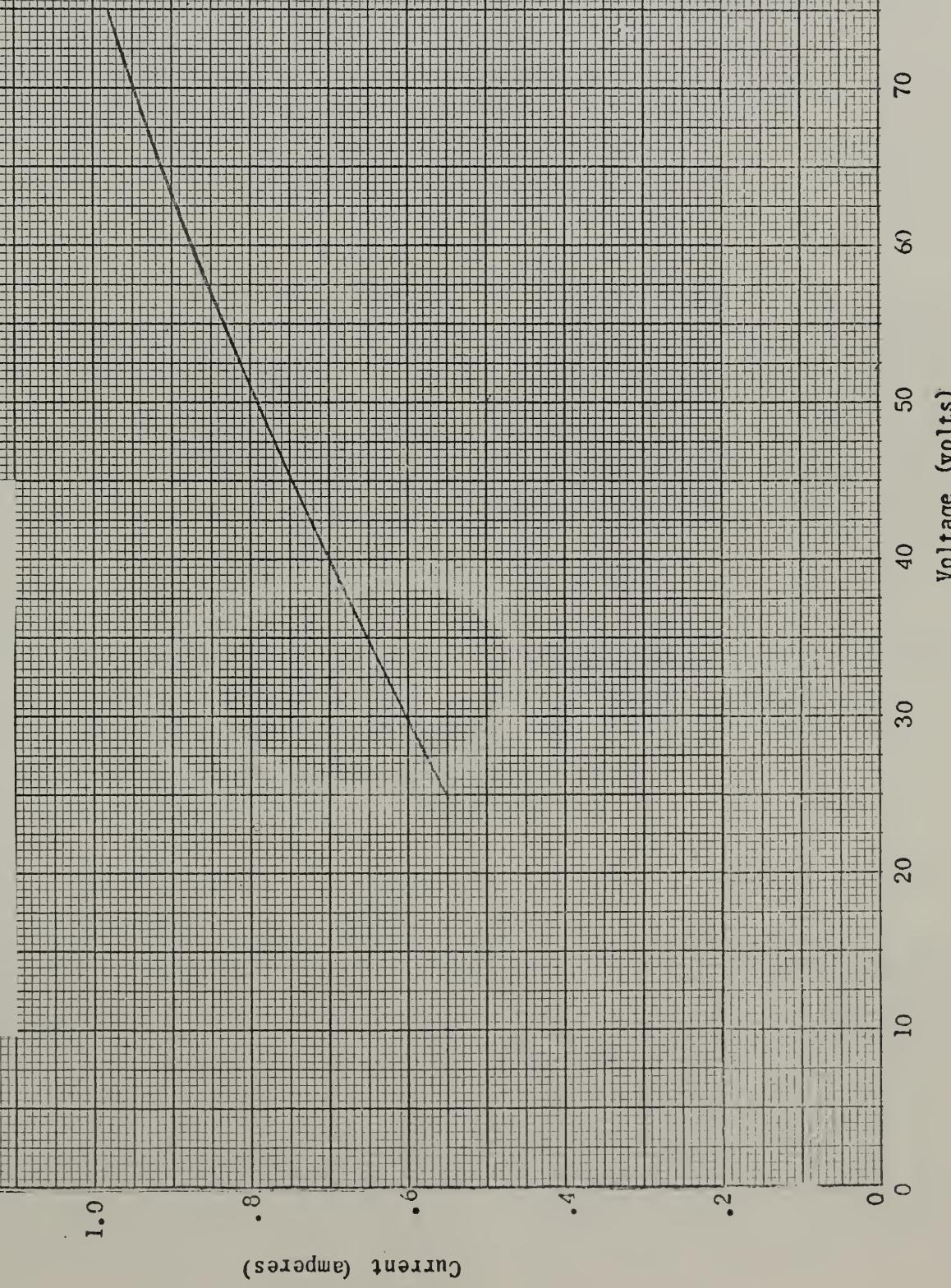


Figure 14d

K+E
SEMI-LOGARITHMIC
359-91
REUFFEL & ESSER CO.
MADE IN U.S.A.
5 CYCLES X 70 DIVISIONS

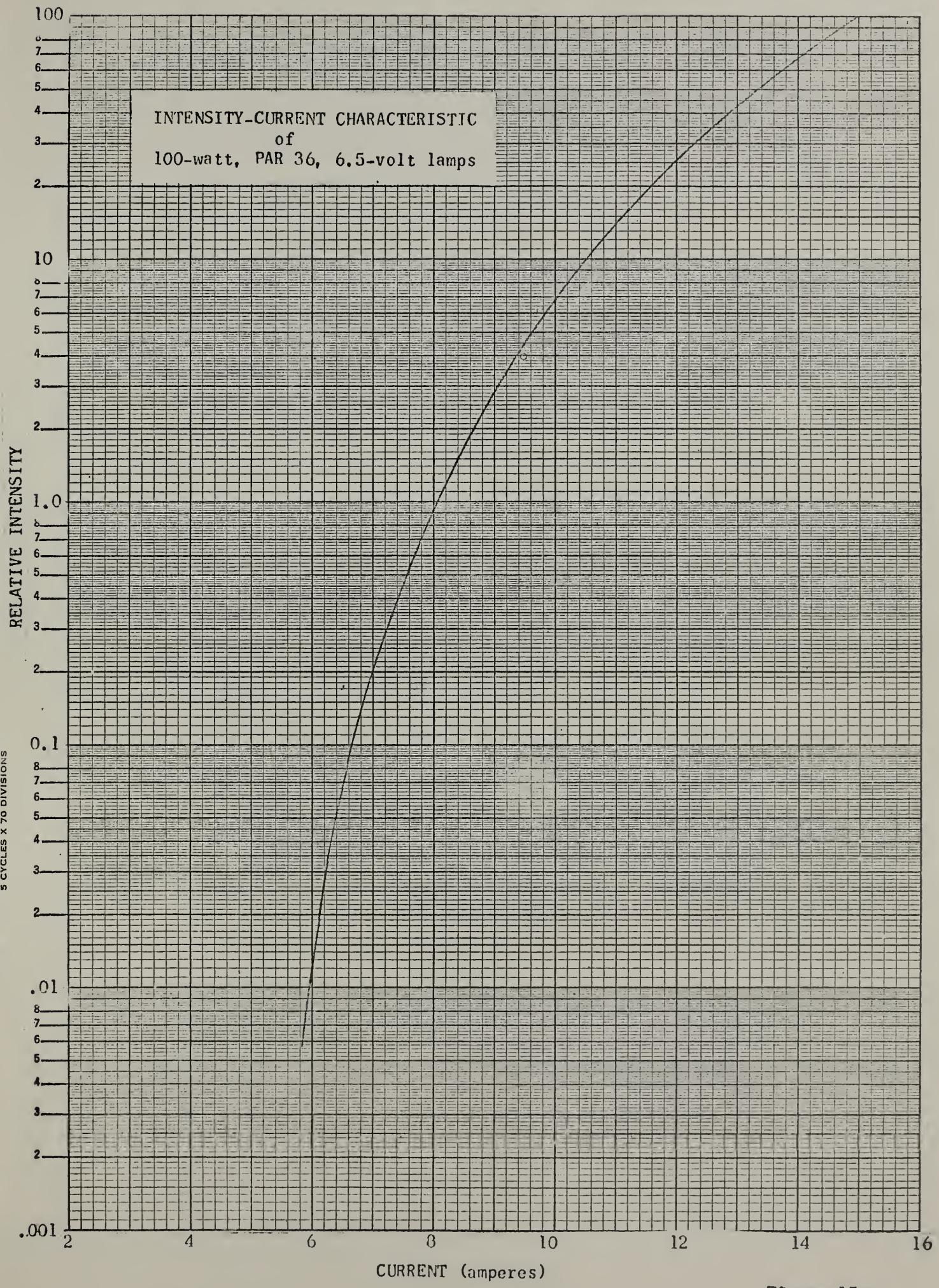
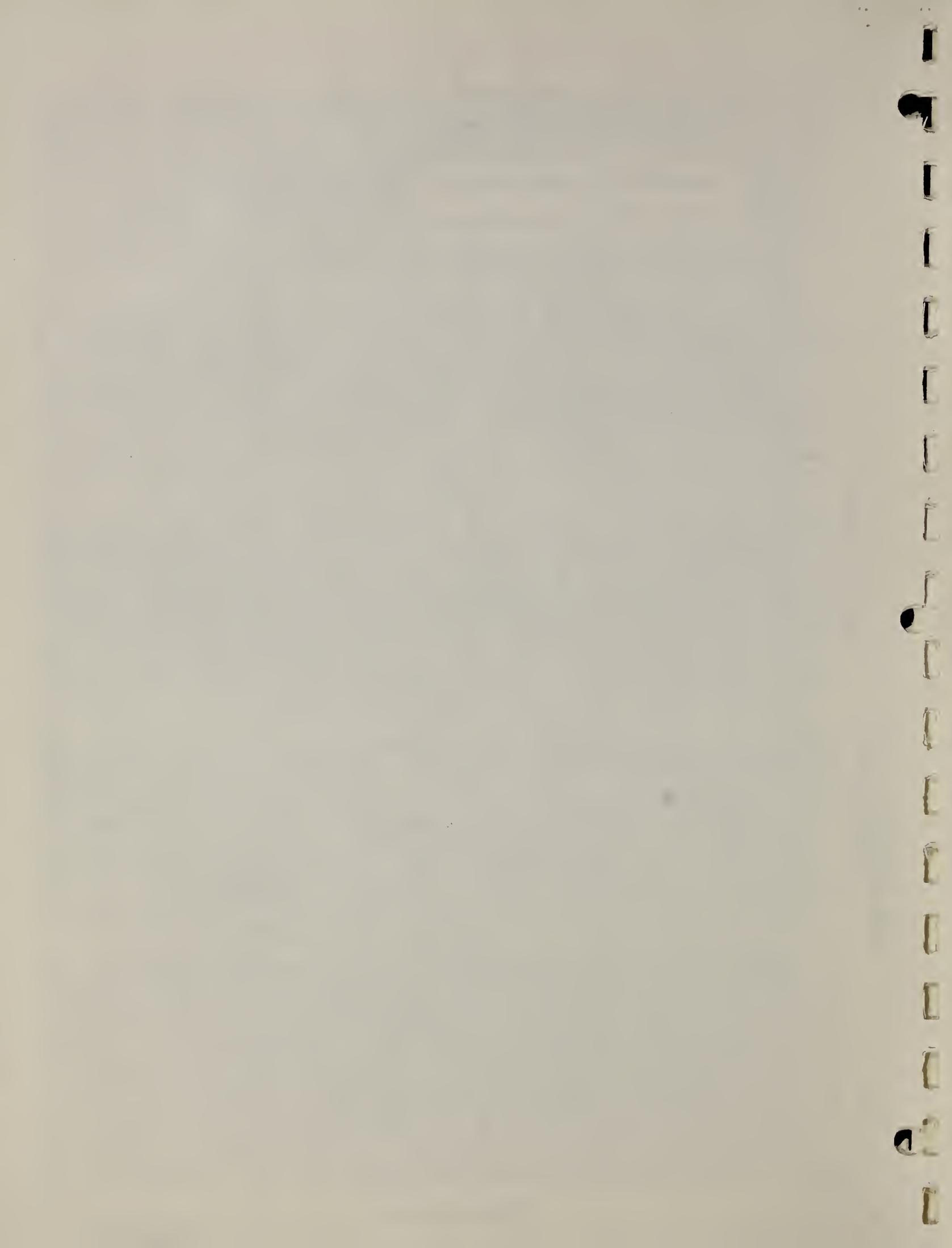


Figure 15a



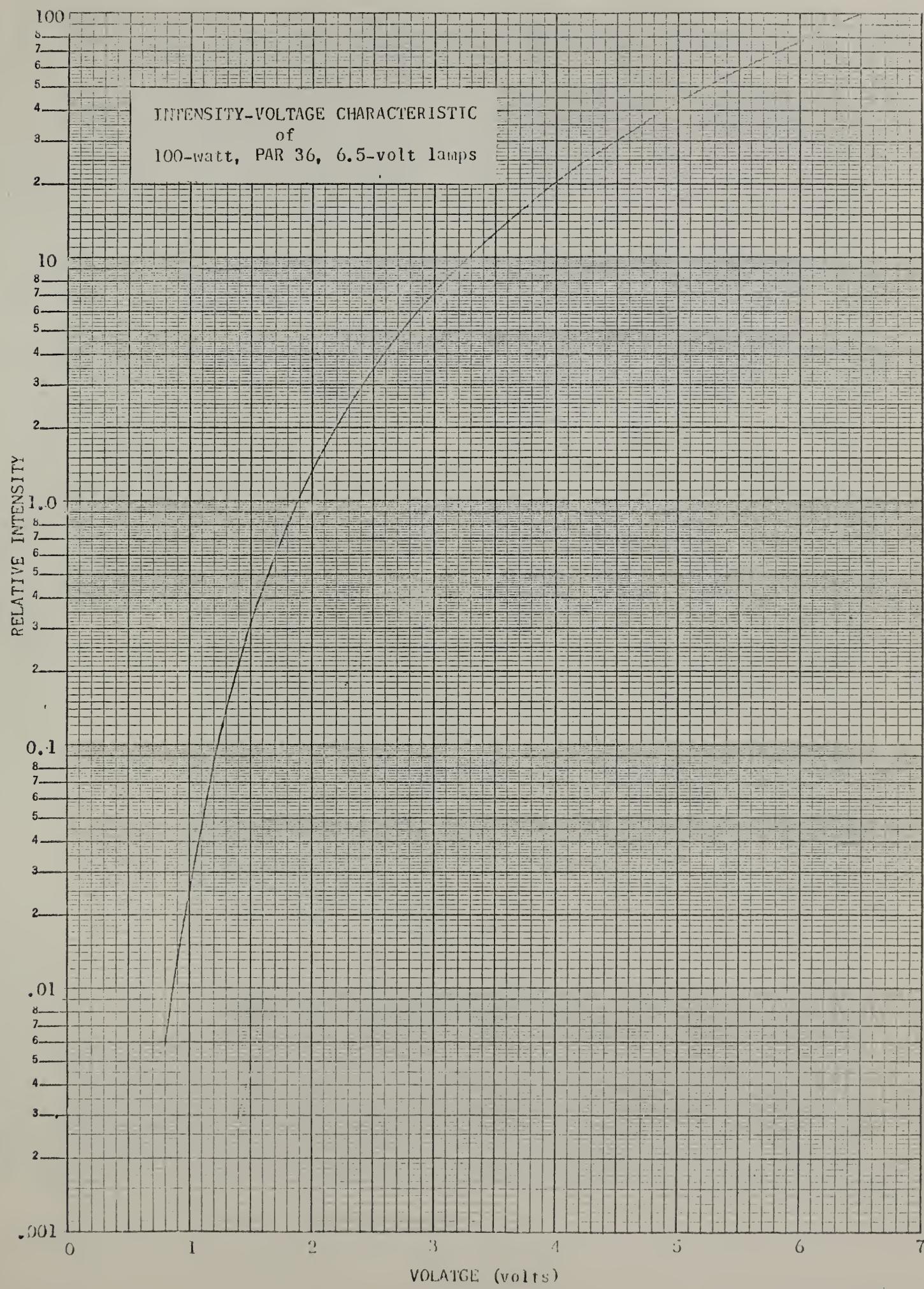
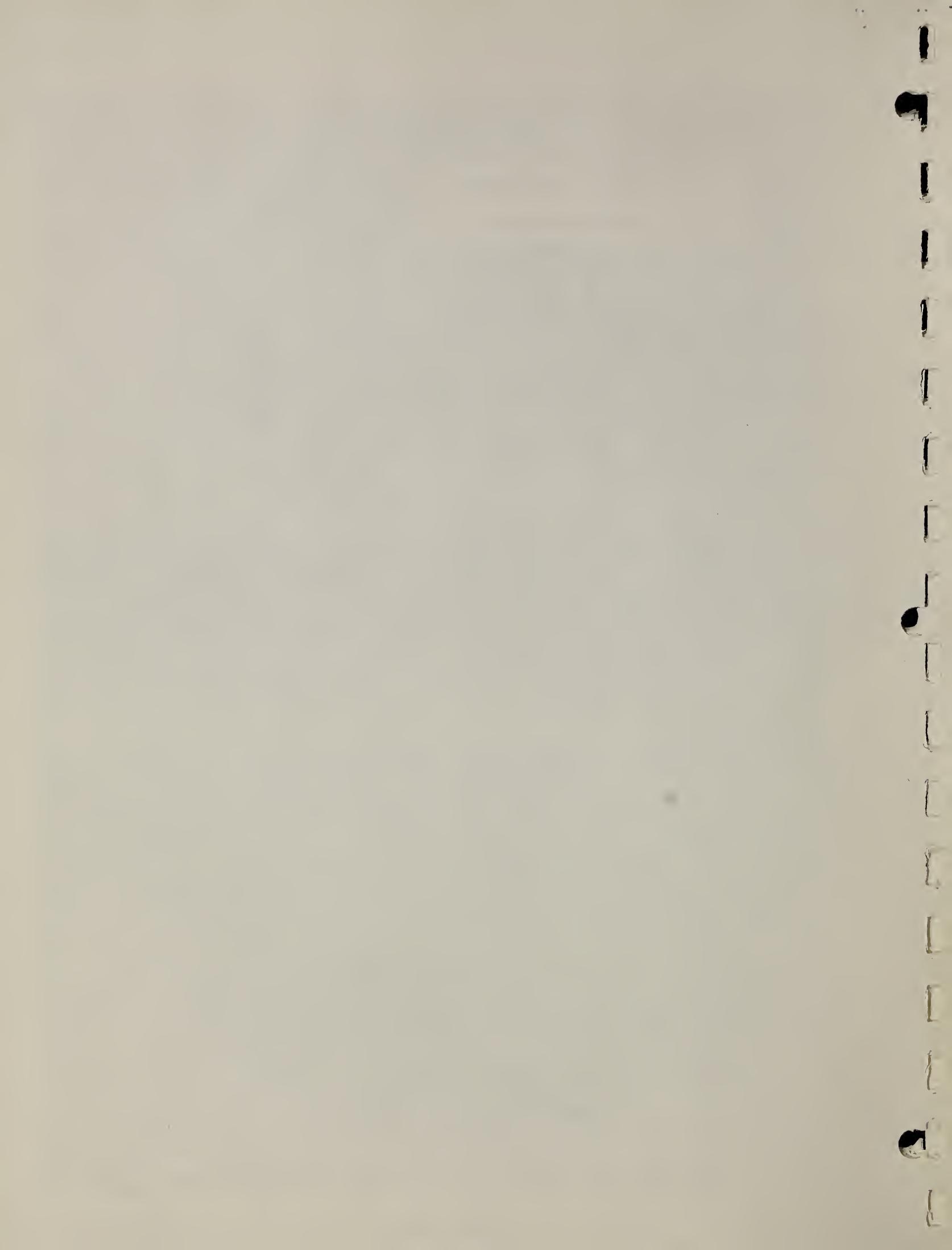


Figure 15b



CURRENT-VOLTAGE CHARACTERISTIC
of
100-watt, PAR 36, 6.5-volt lamps

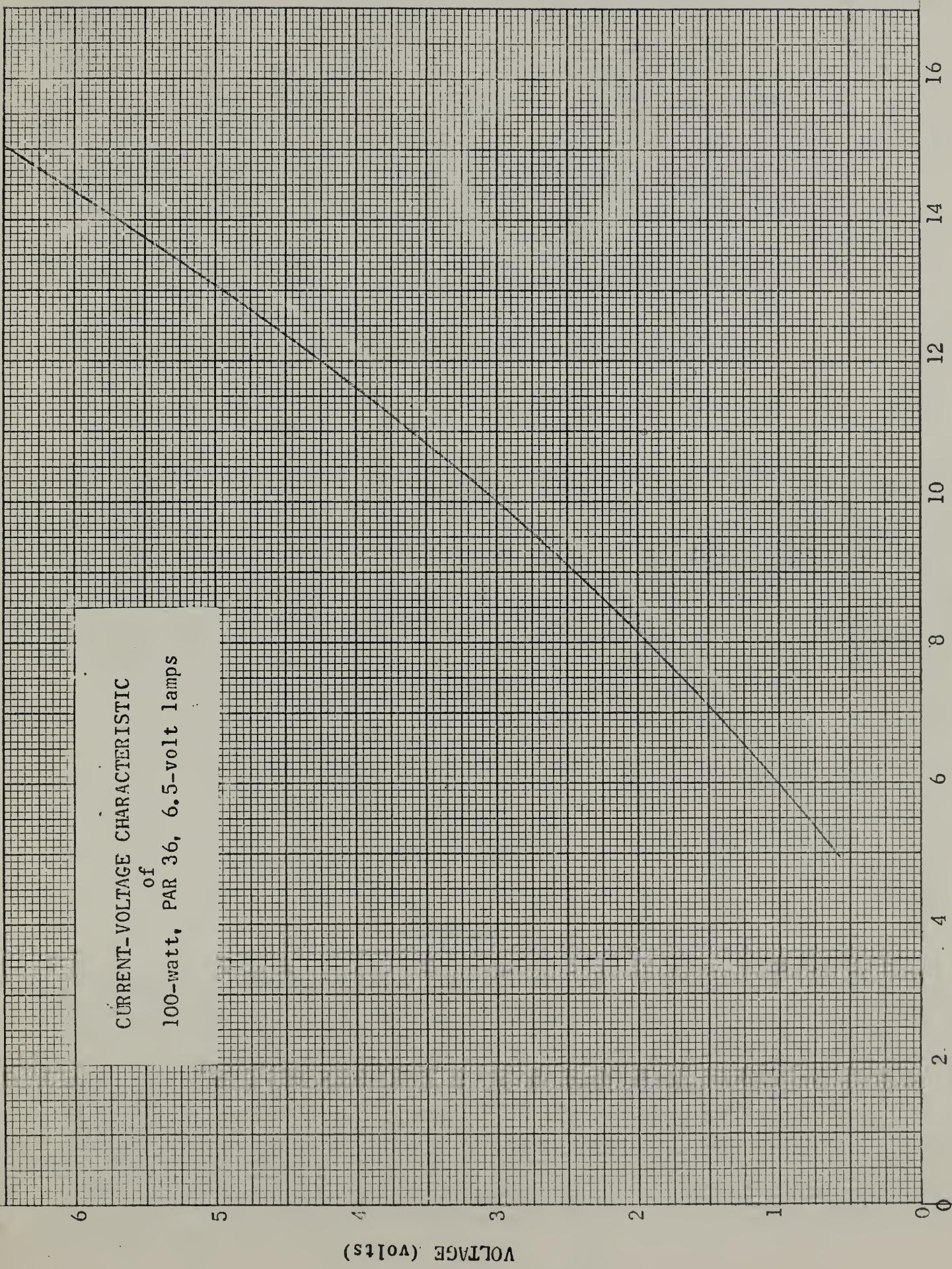
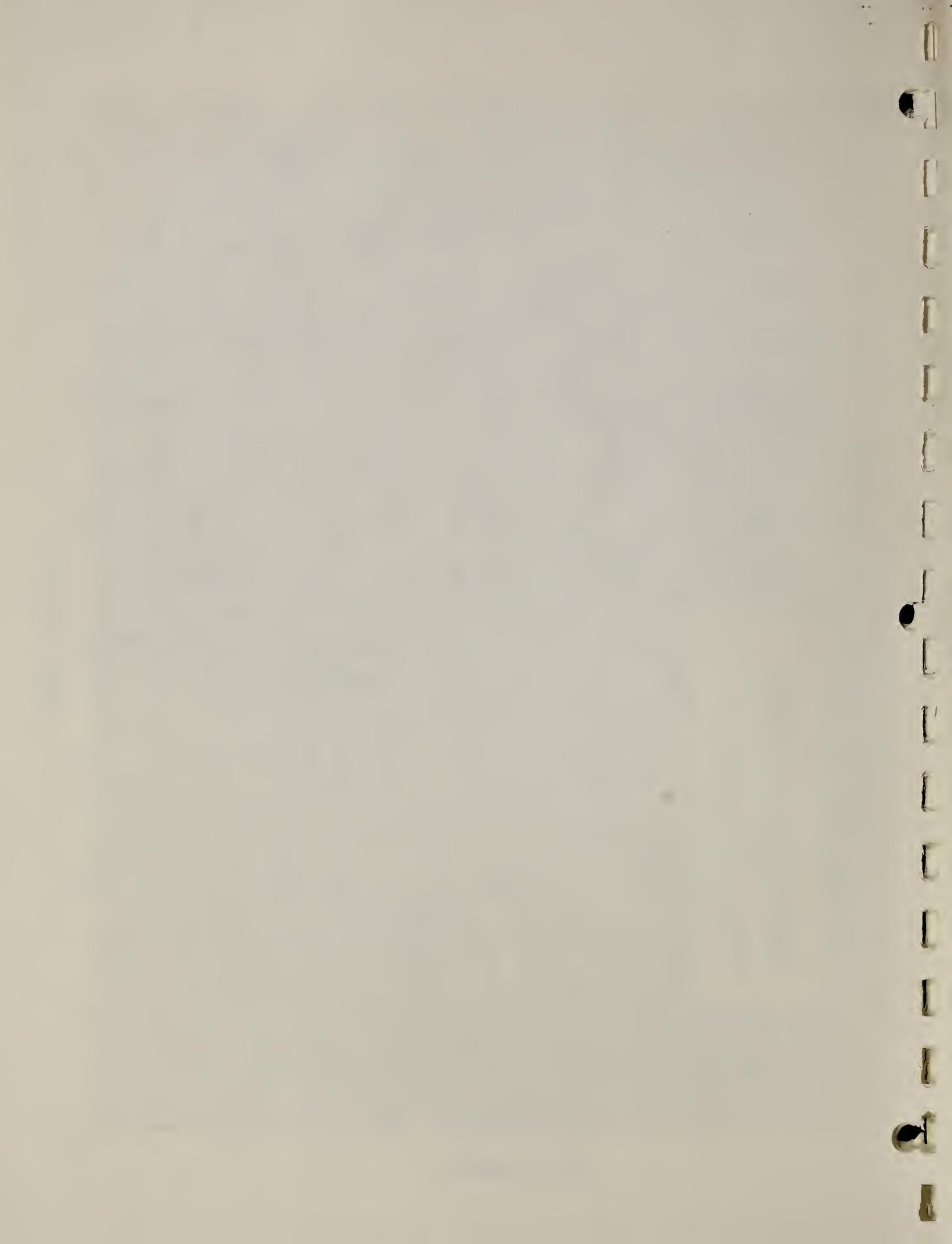


Figure 15c



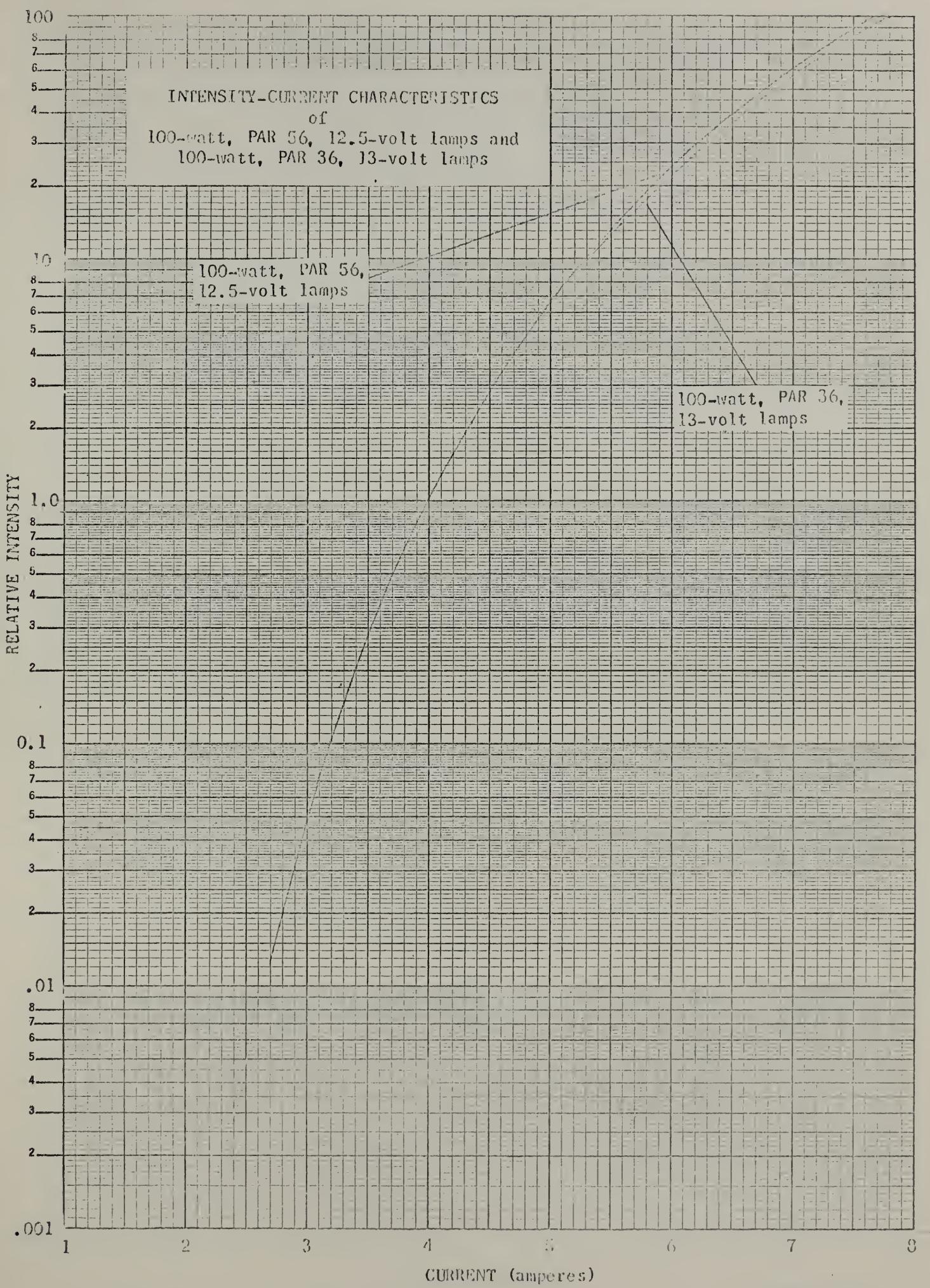


Figure 16a



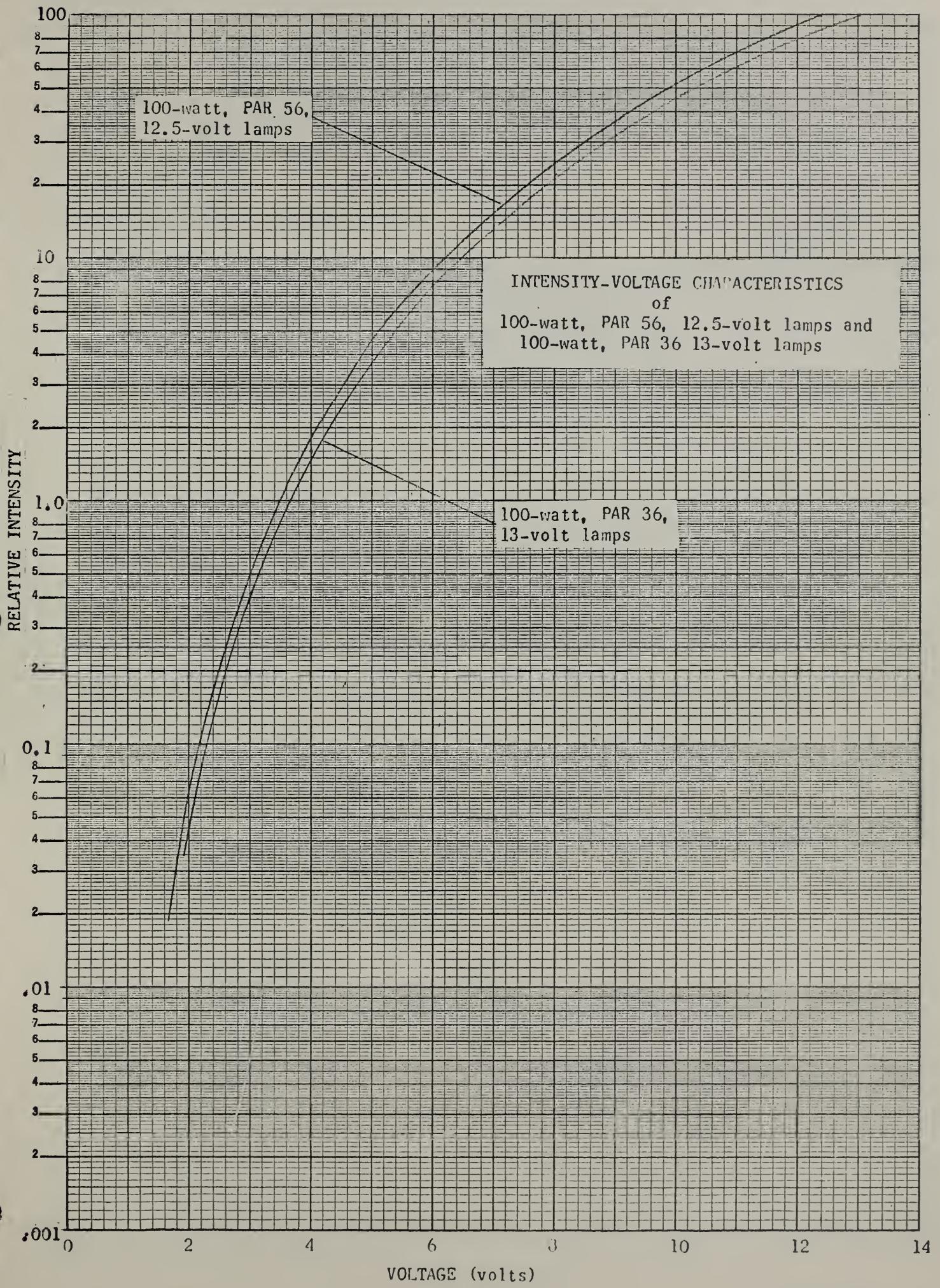


Figure 16b

Q E

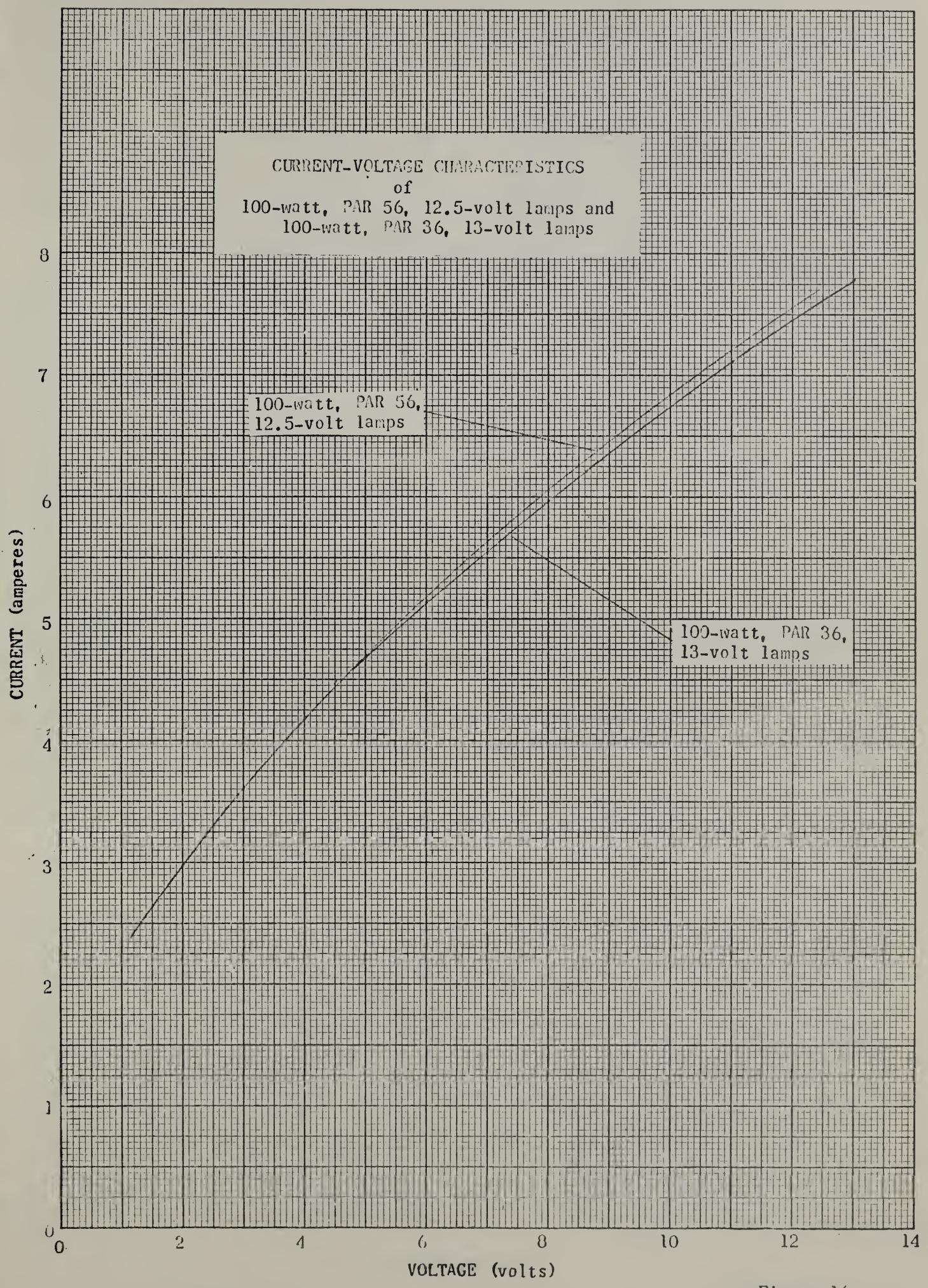
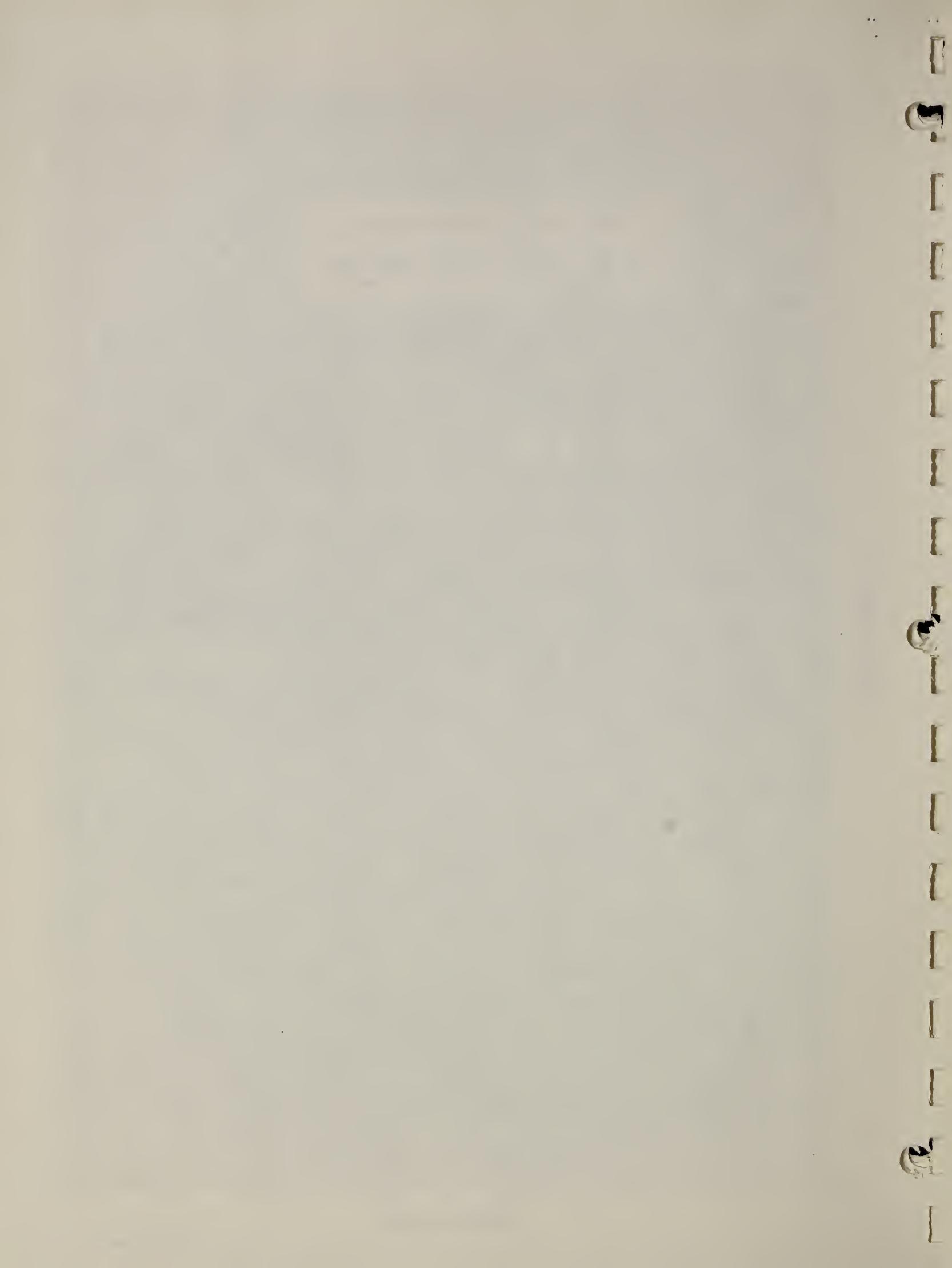


Figure 16c



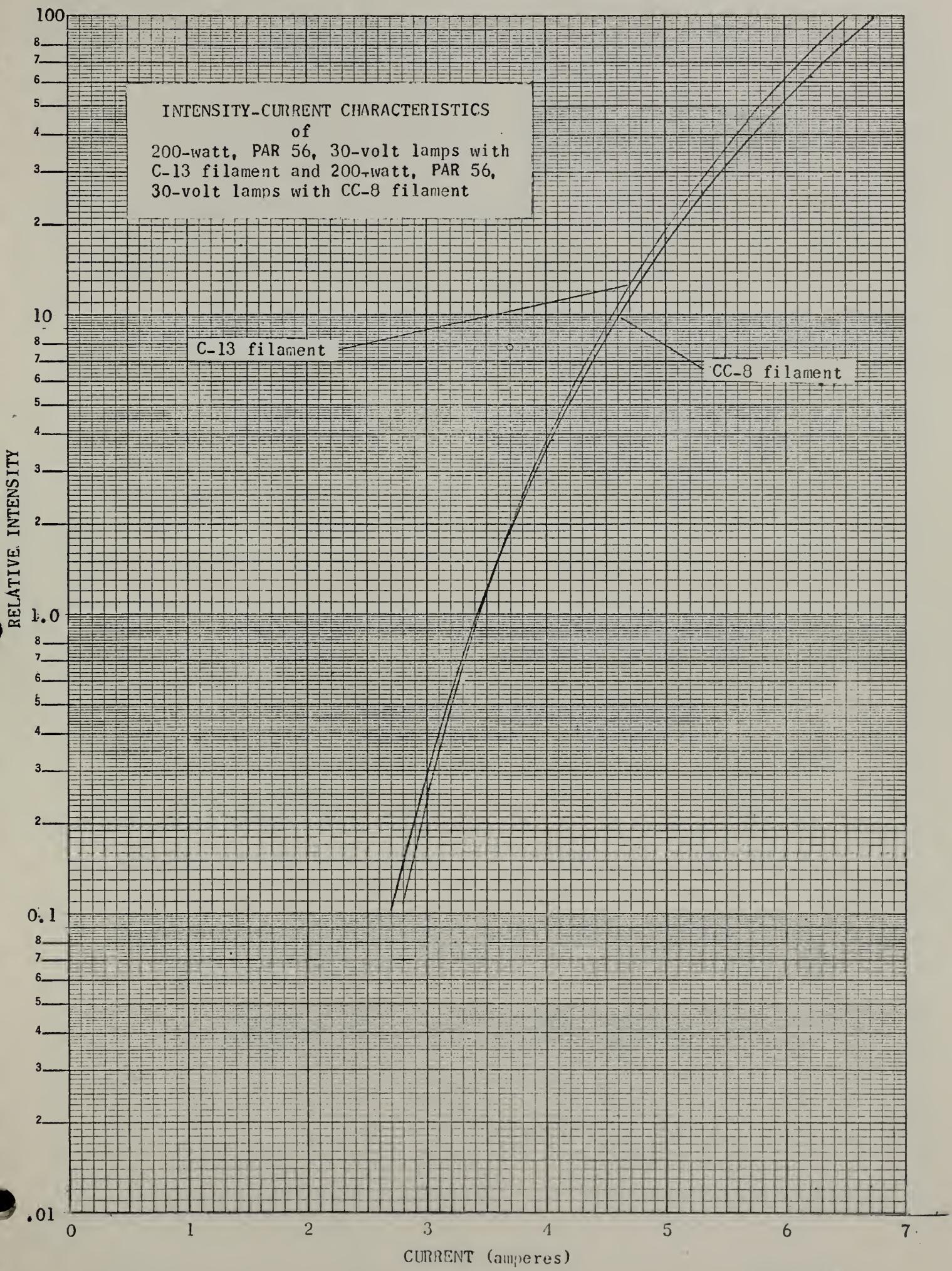
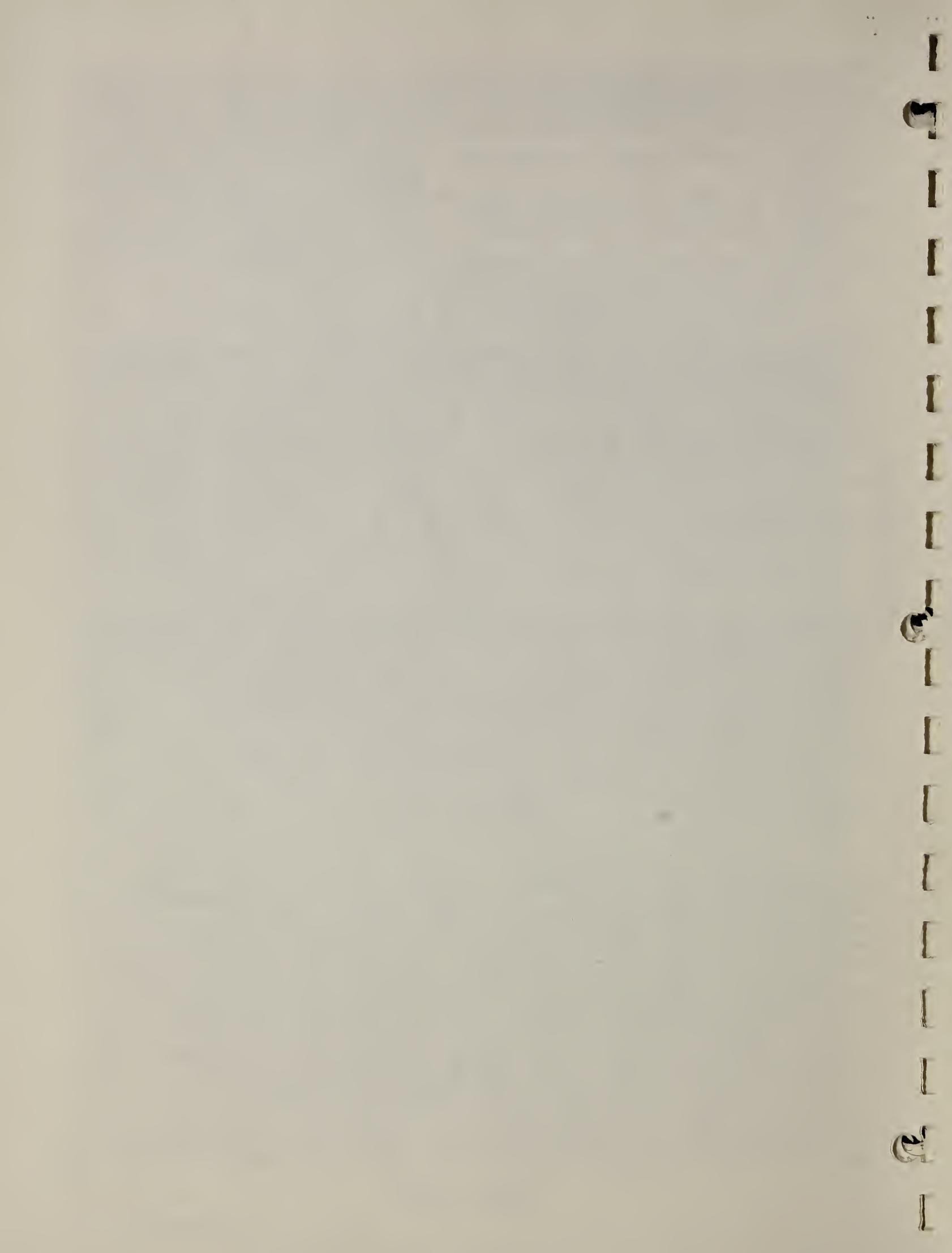


Figure 17a



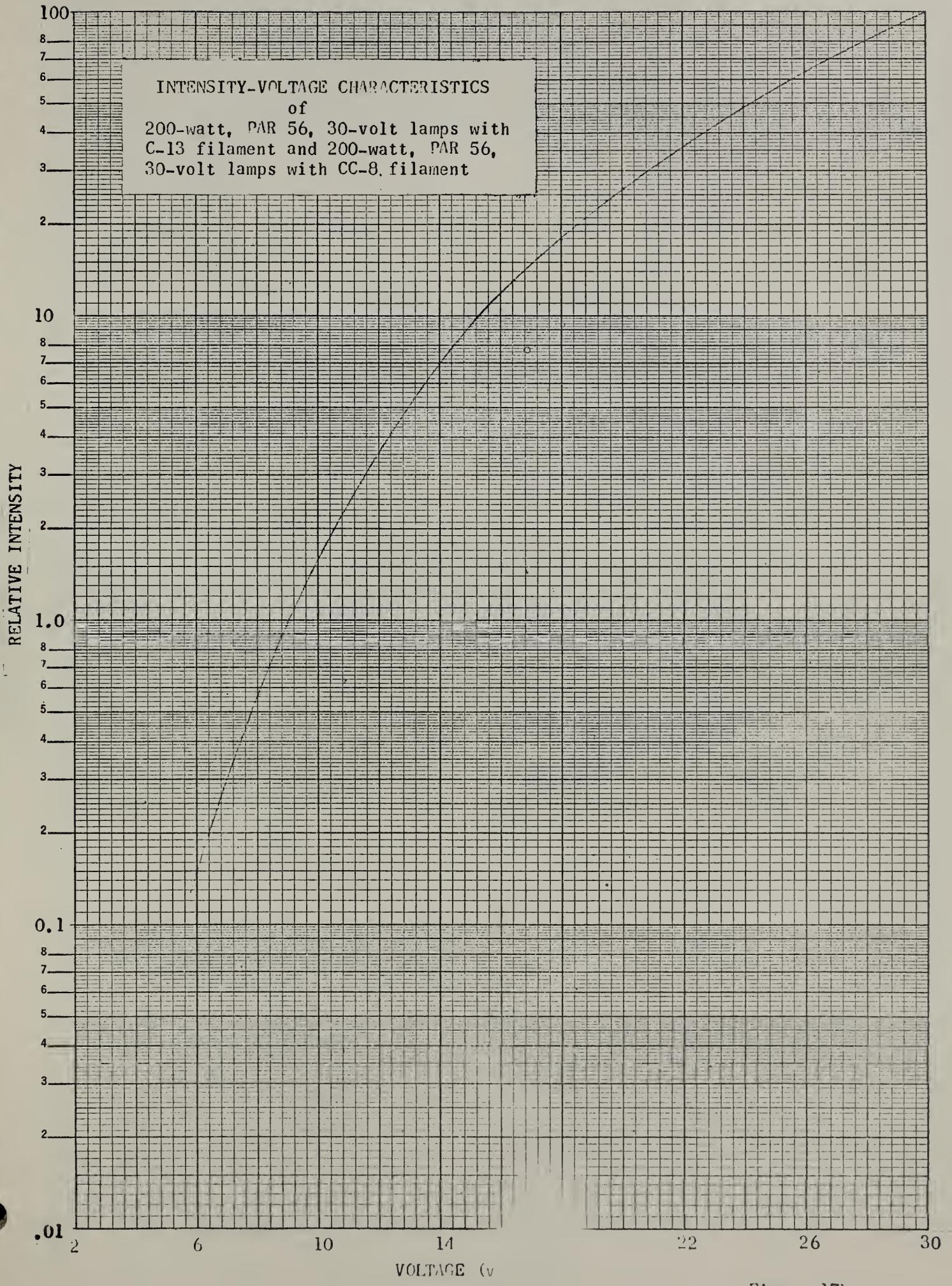
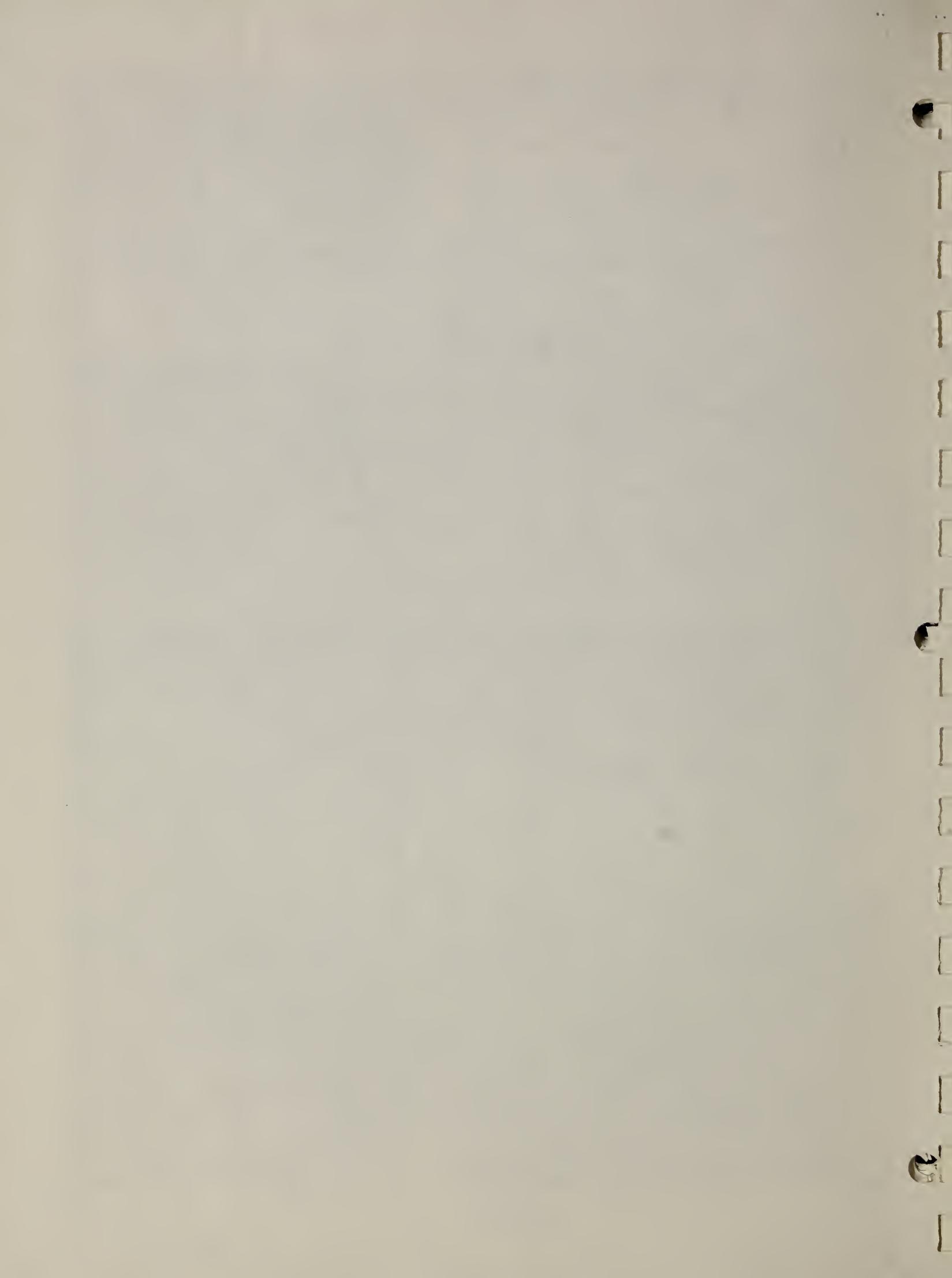


Figure 17b



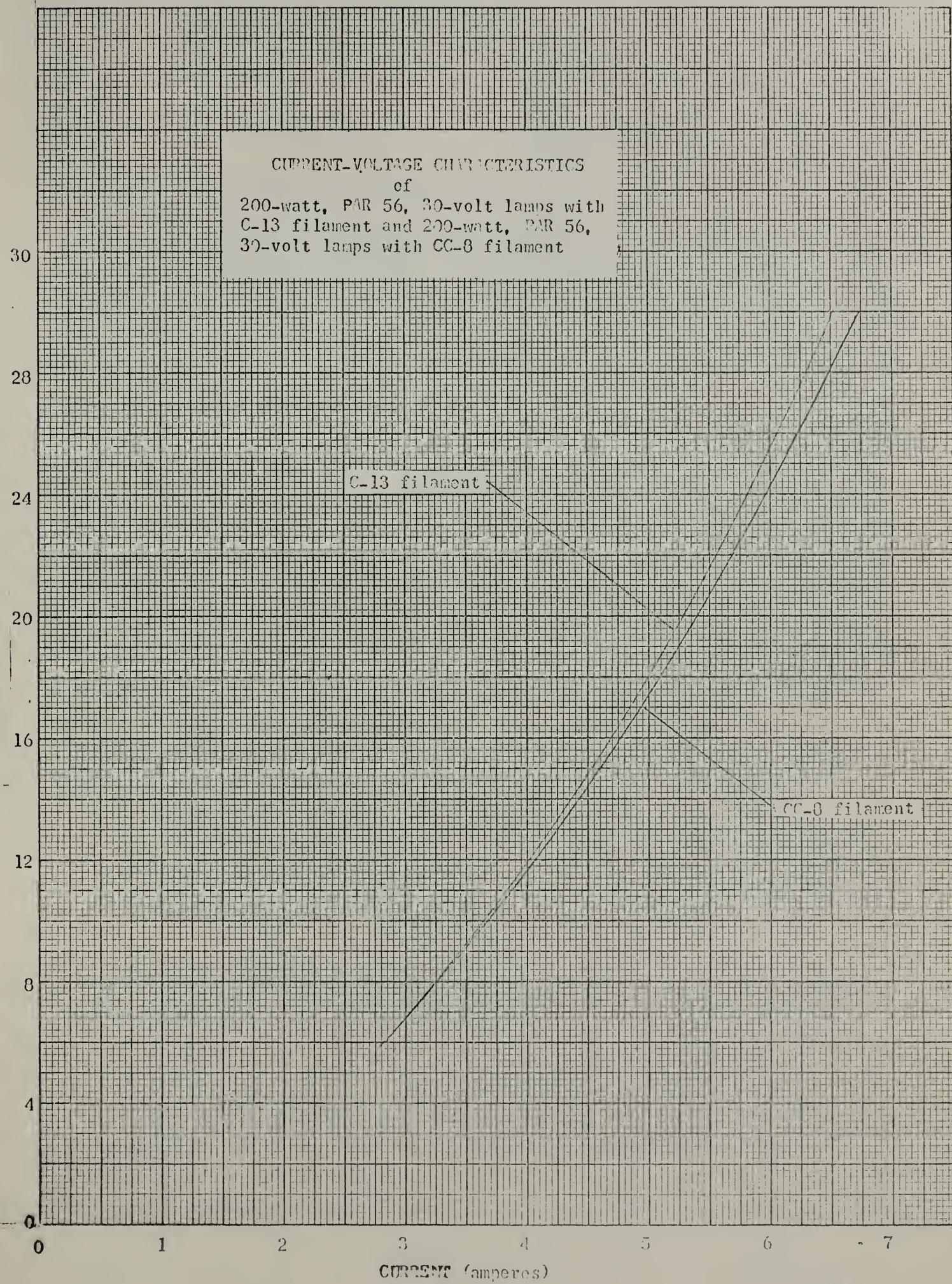
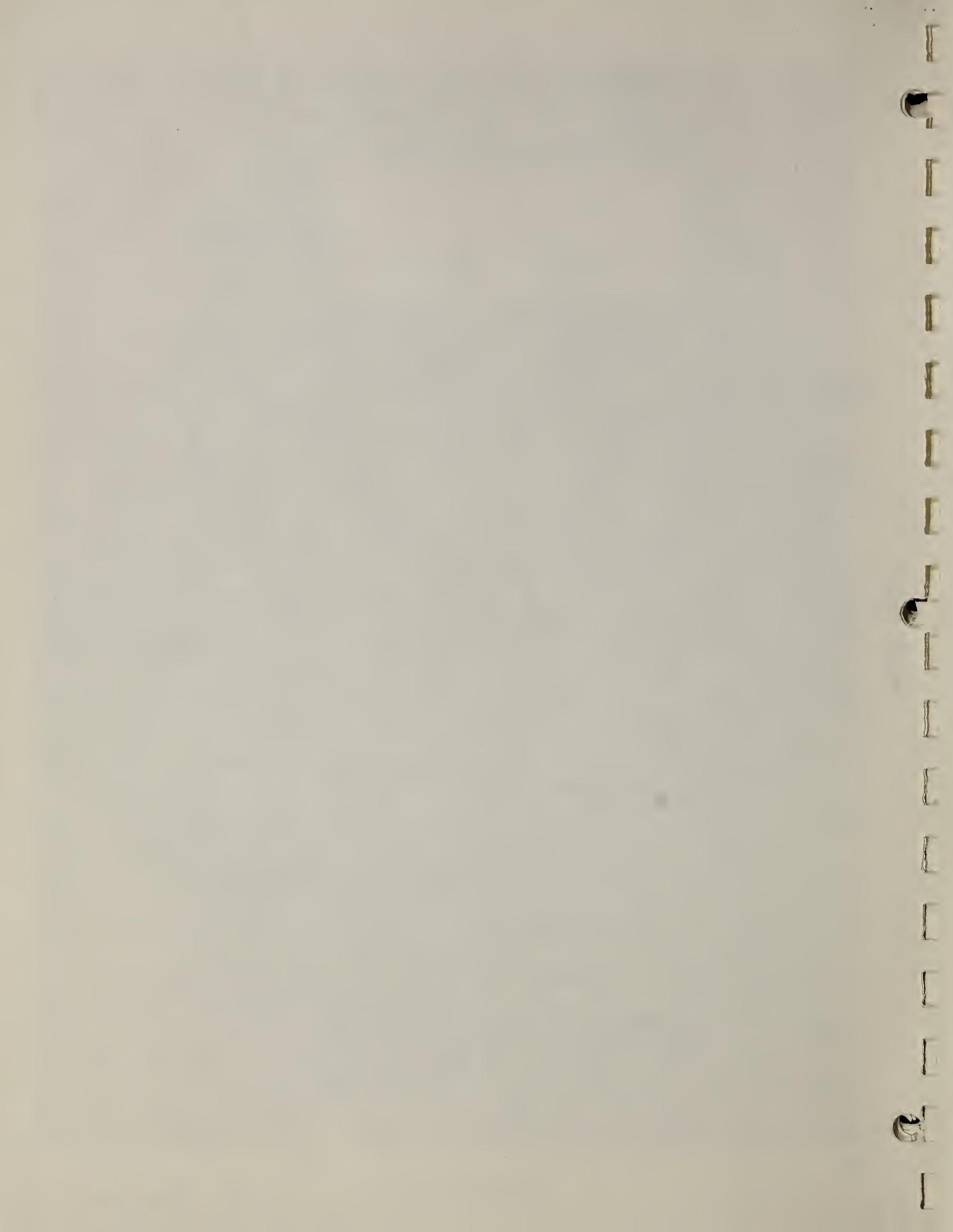


Figure 17c



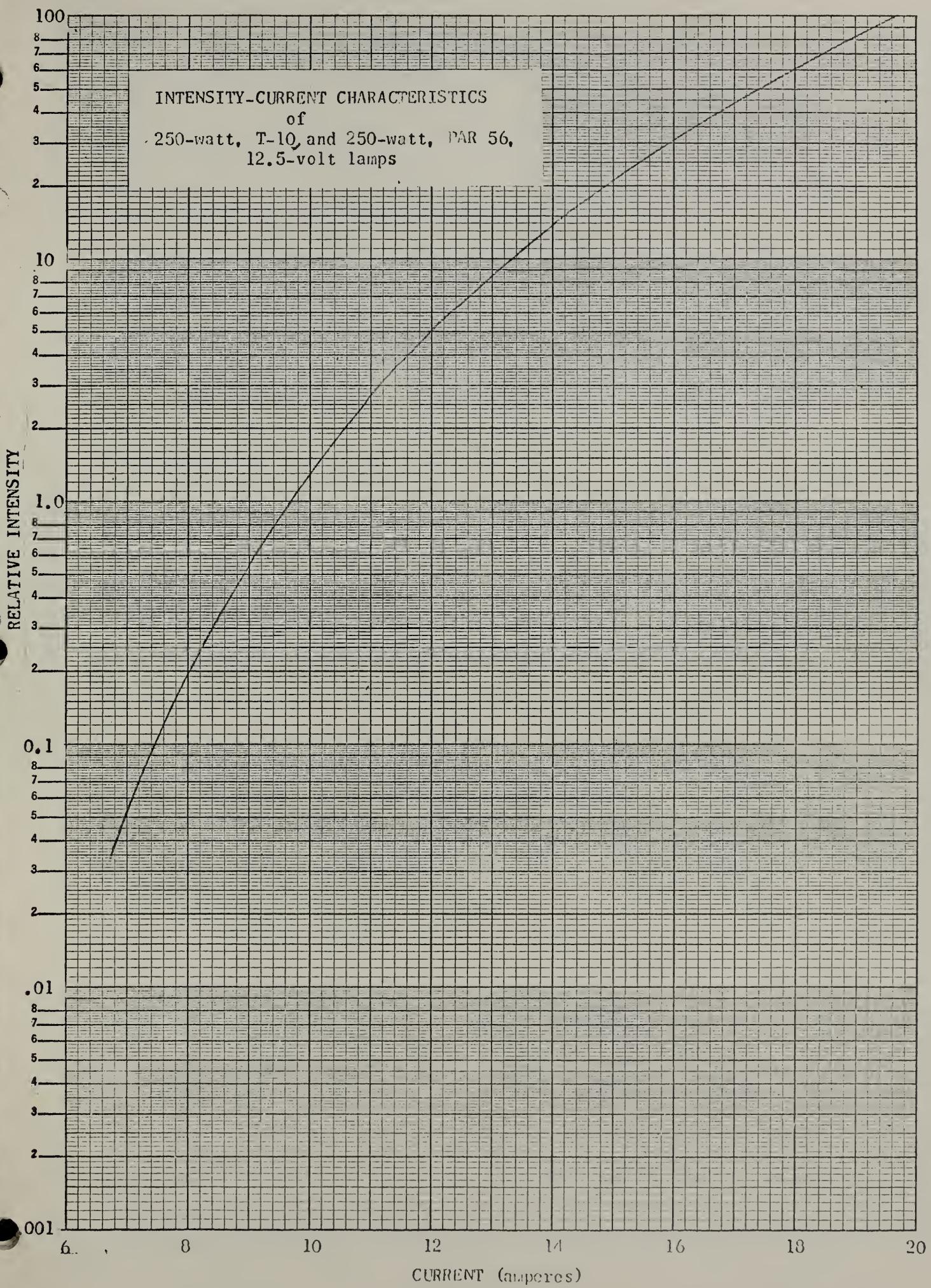
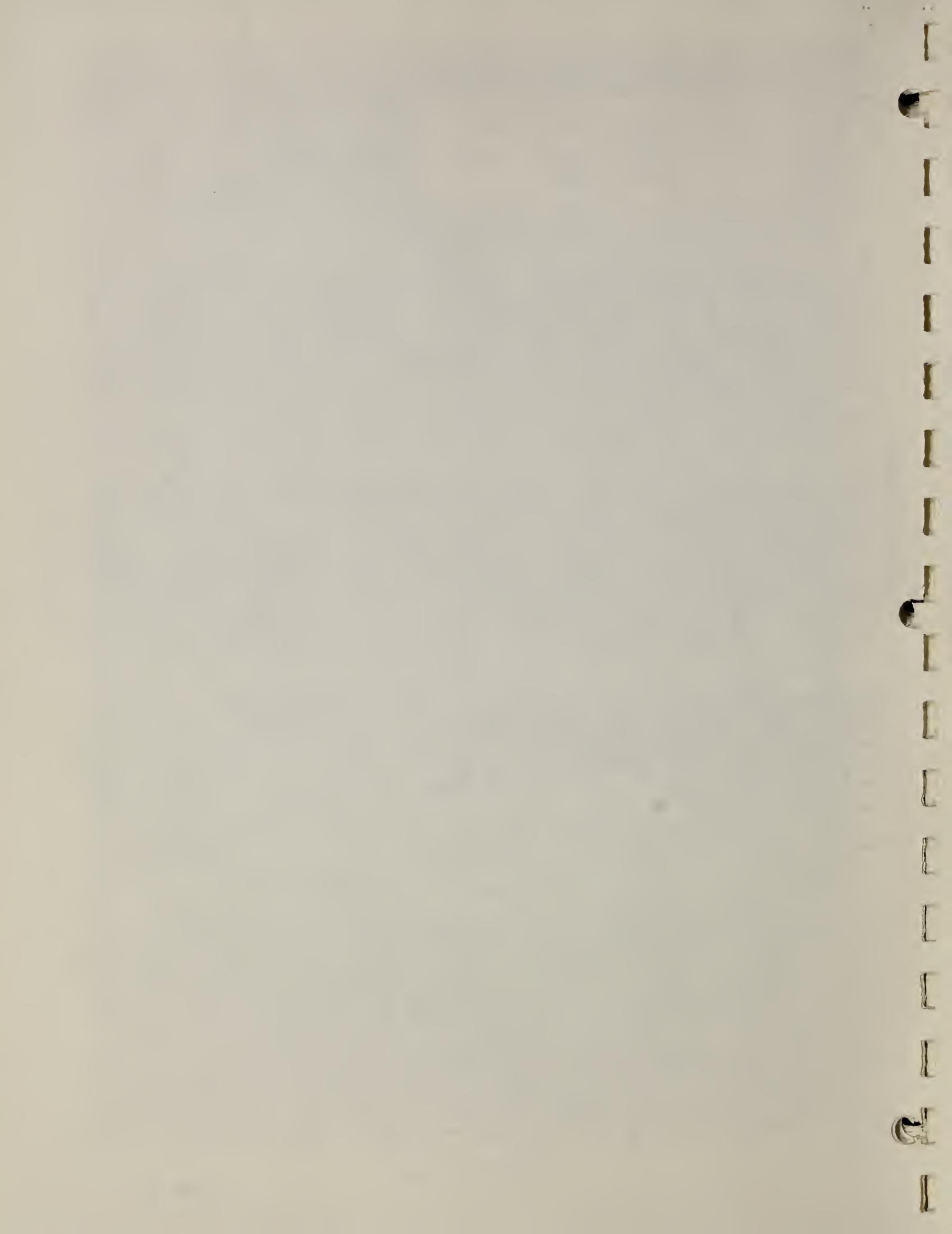


Figure 18a



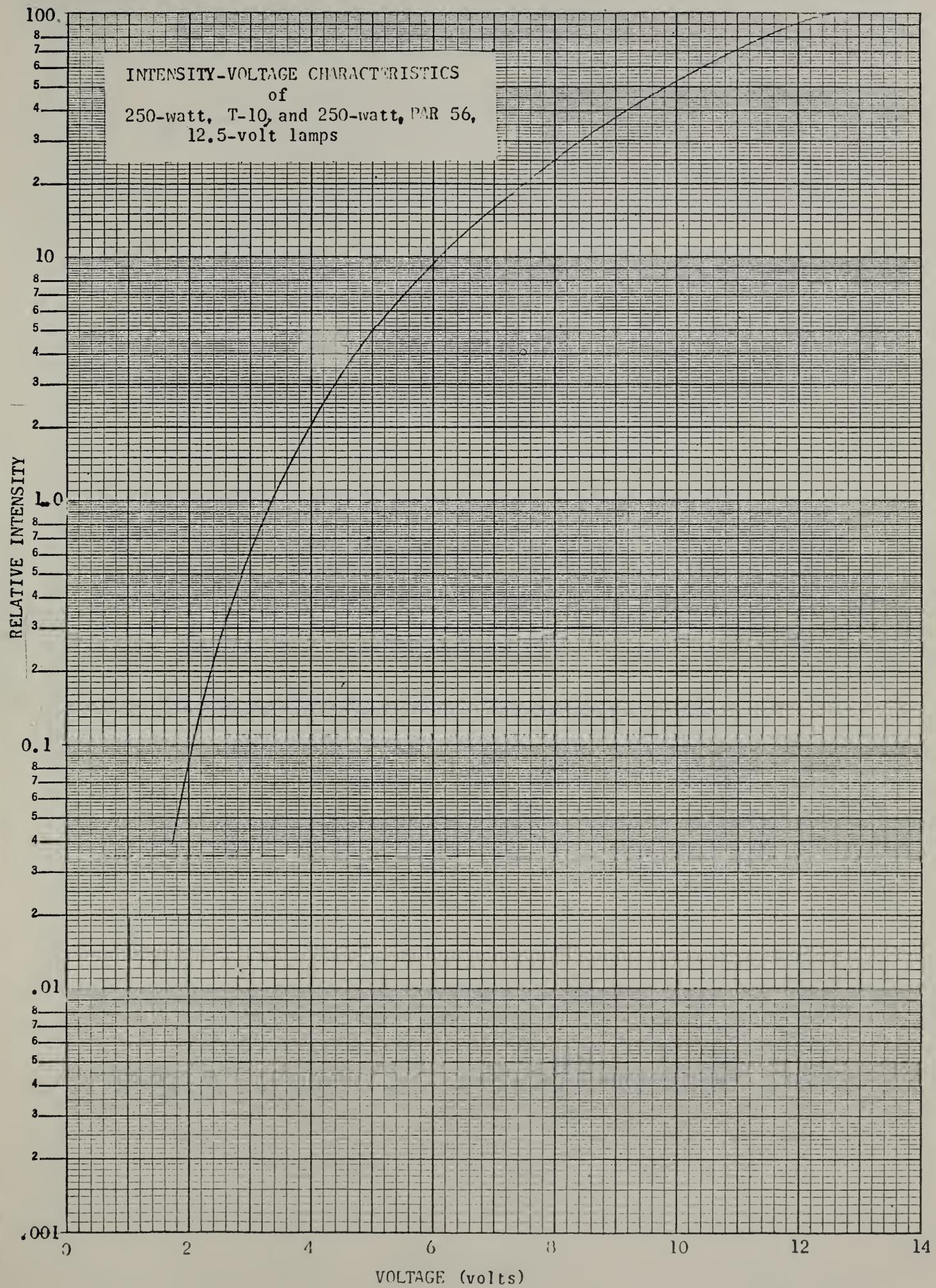
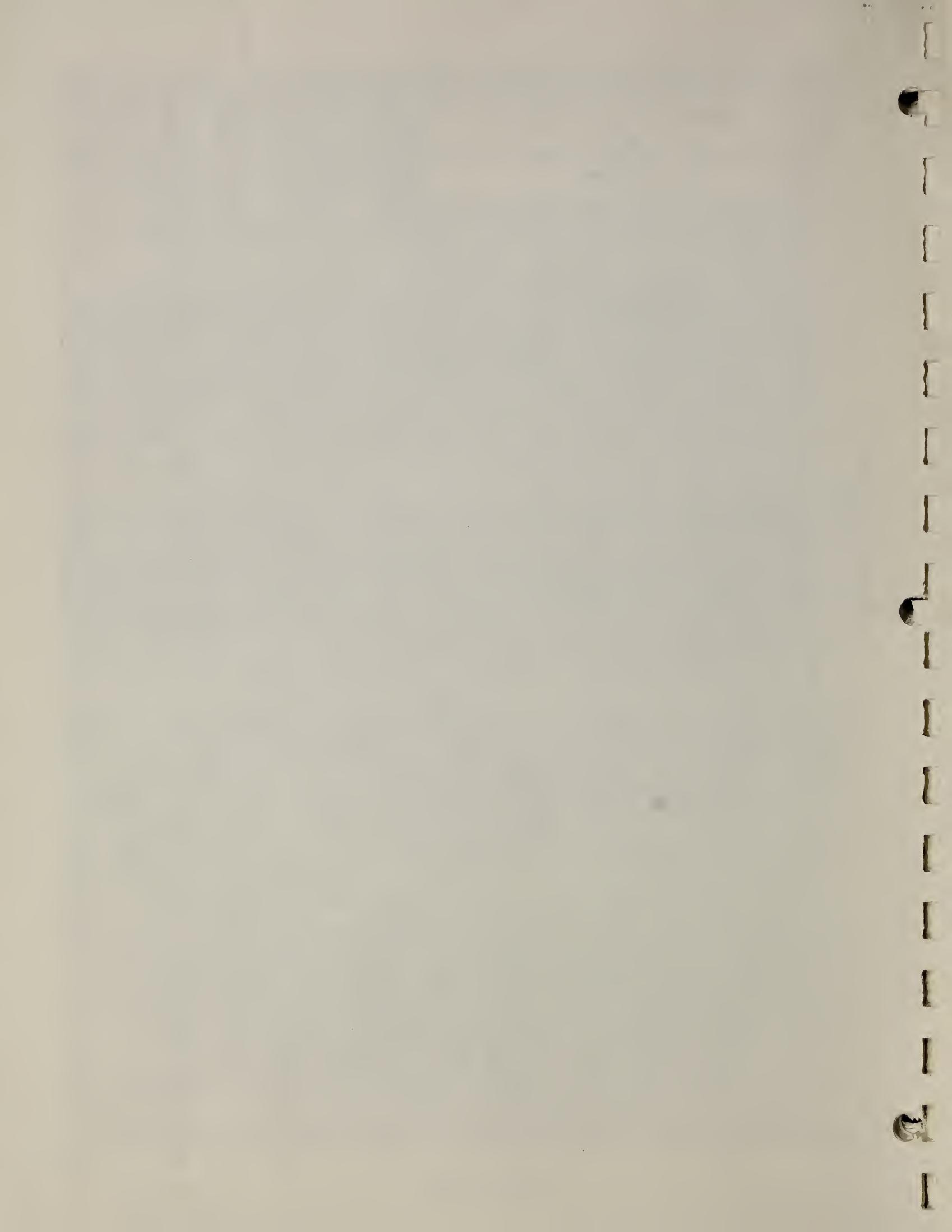


Figure 18b



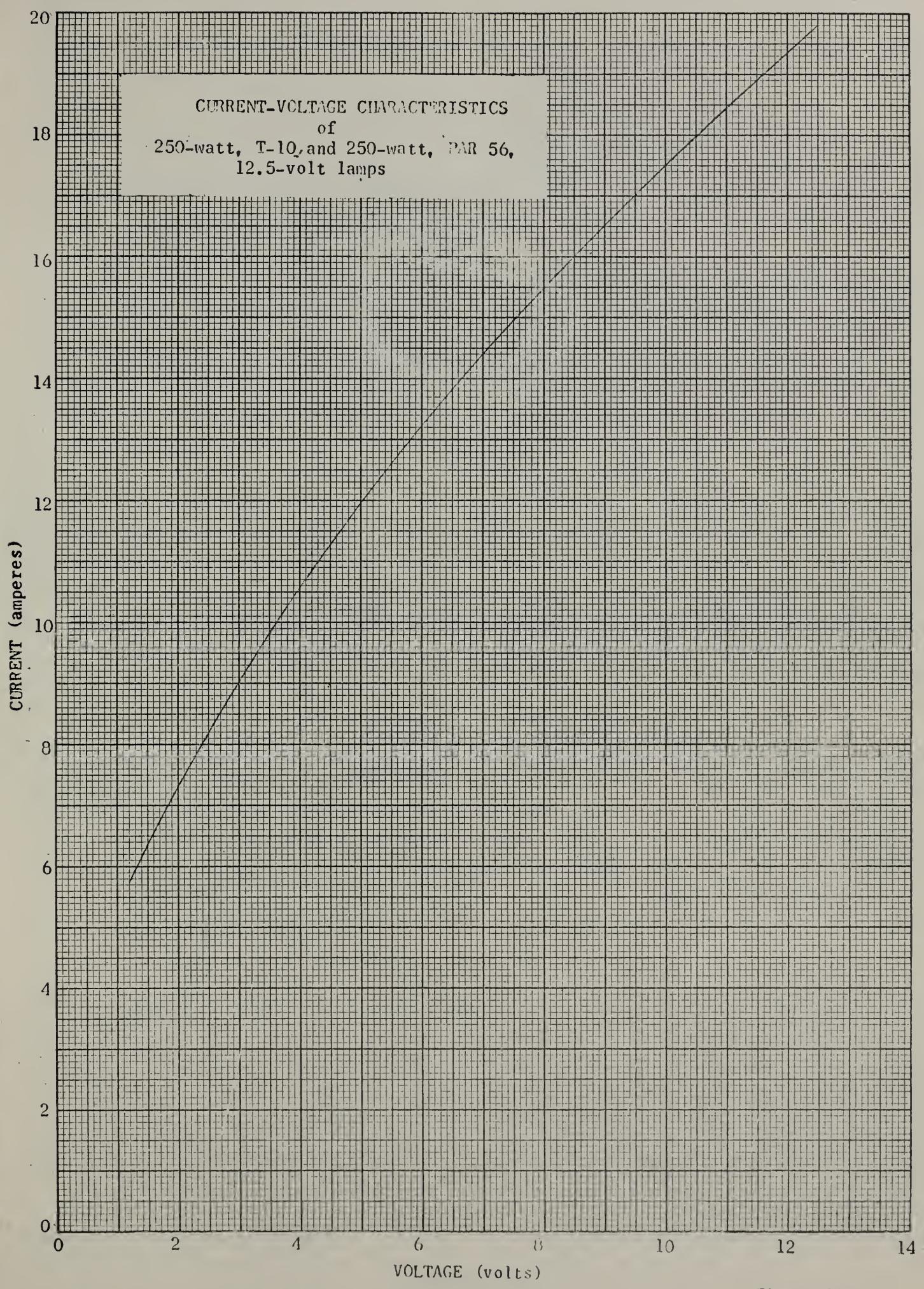
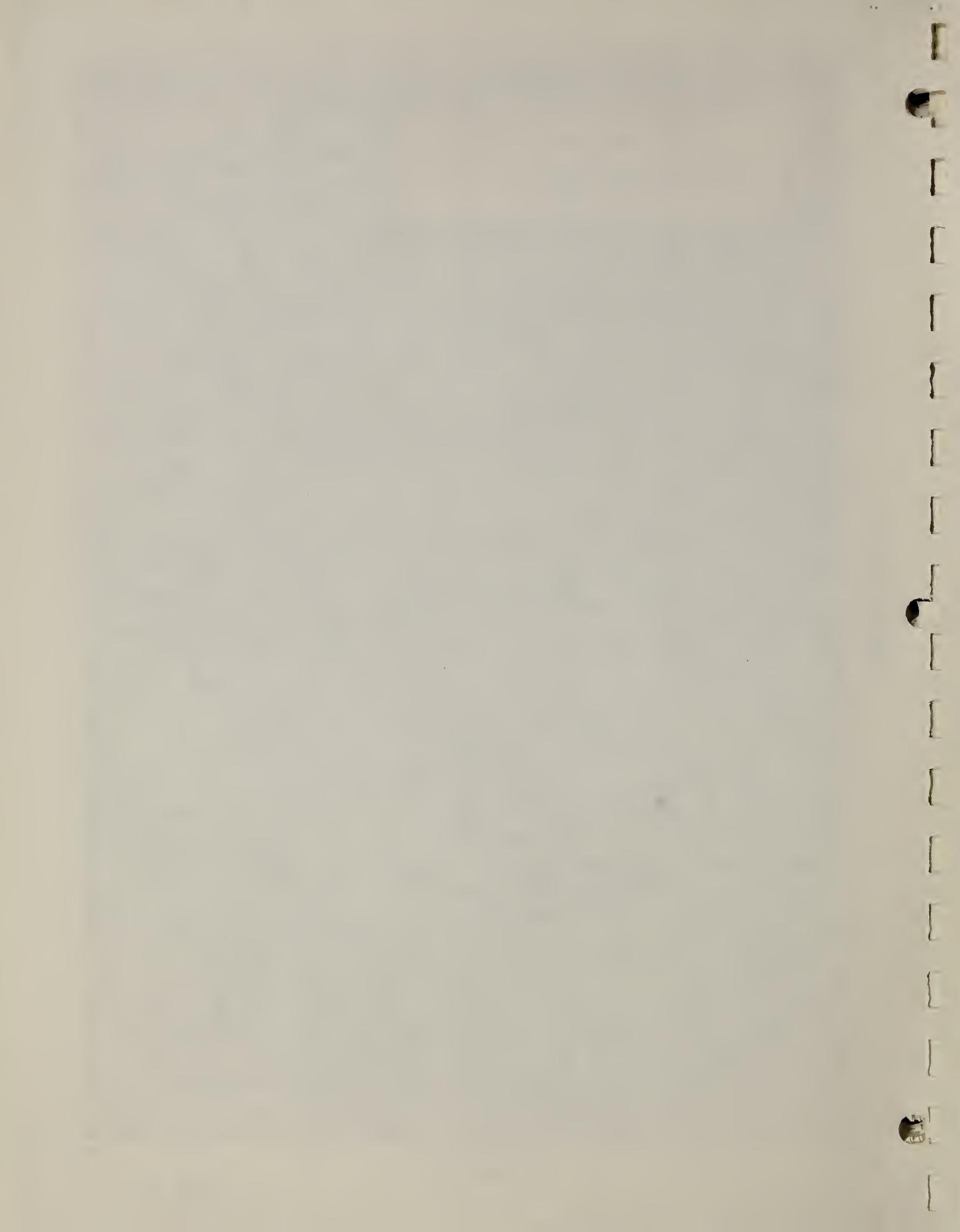


Figure 18c



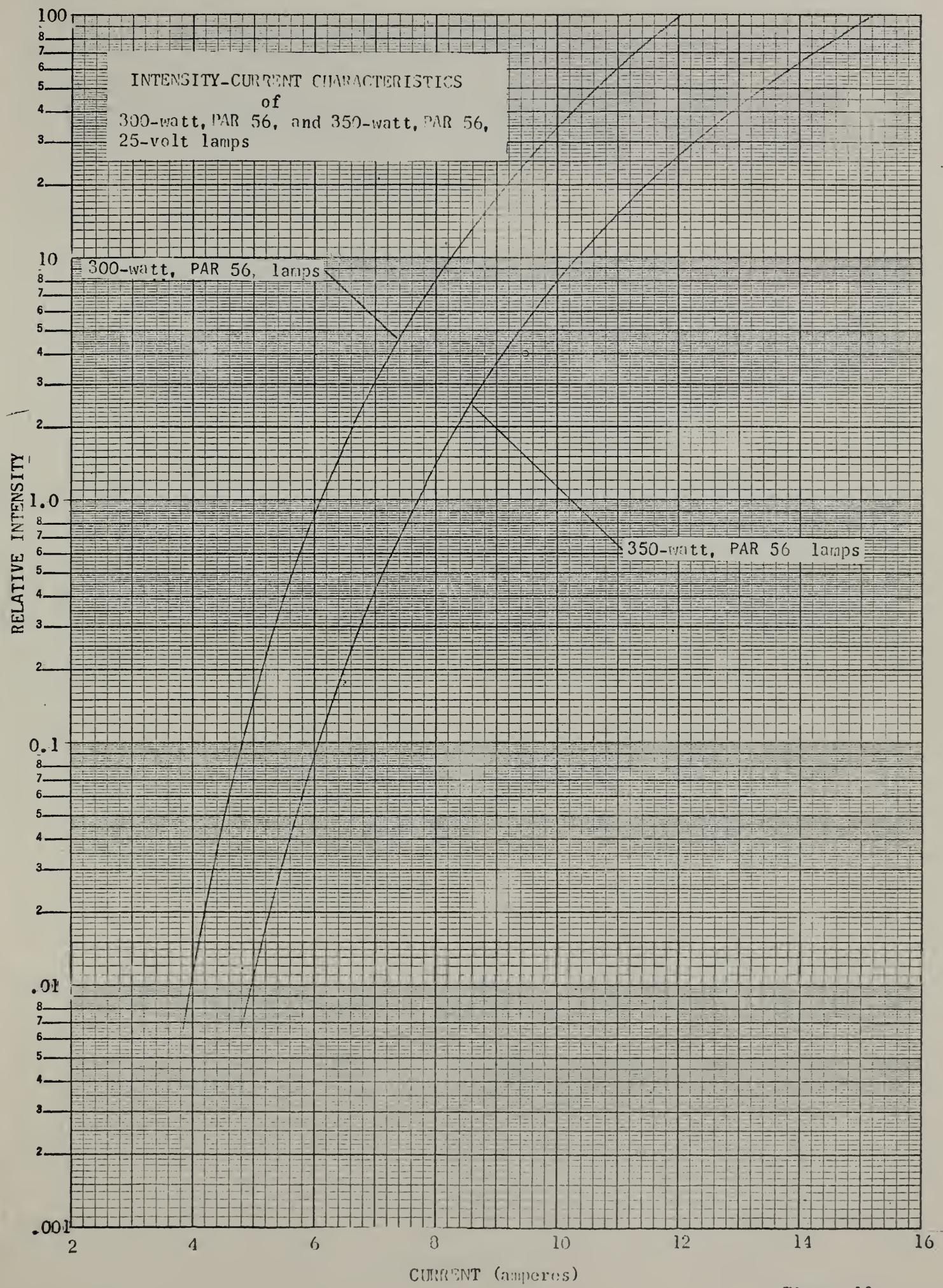
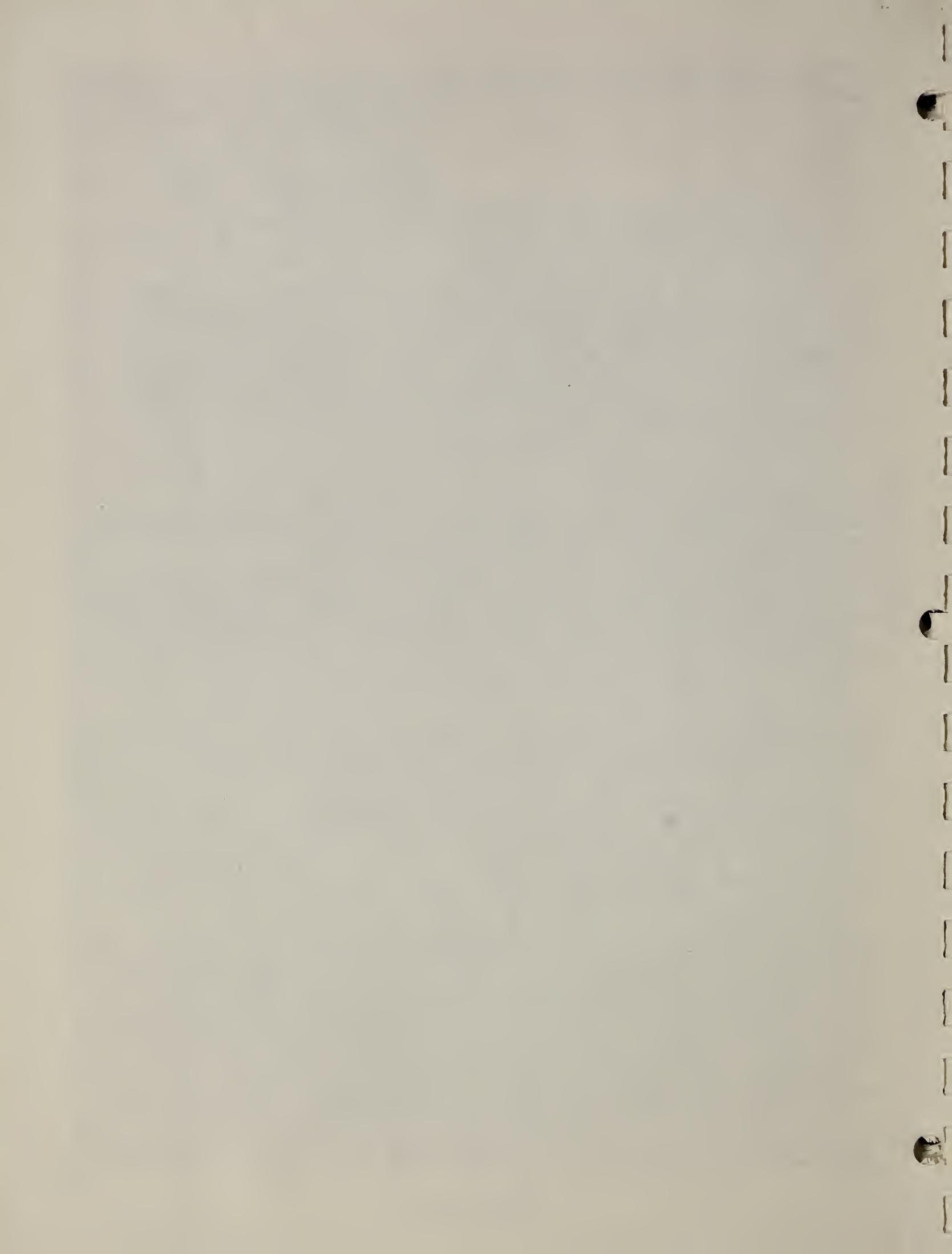


Figure 19a



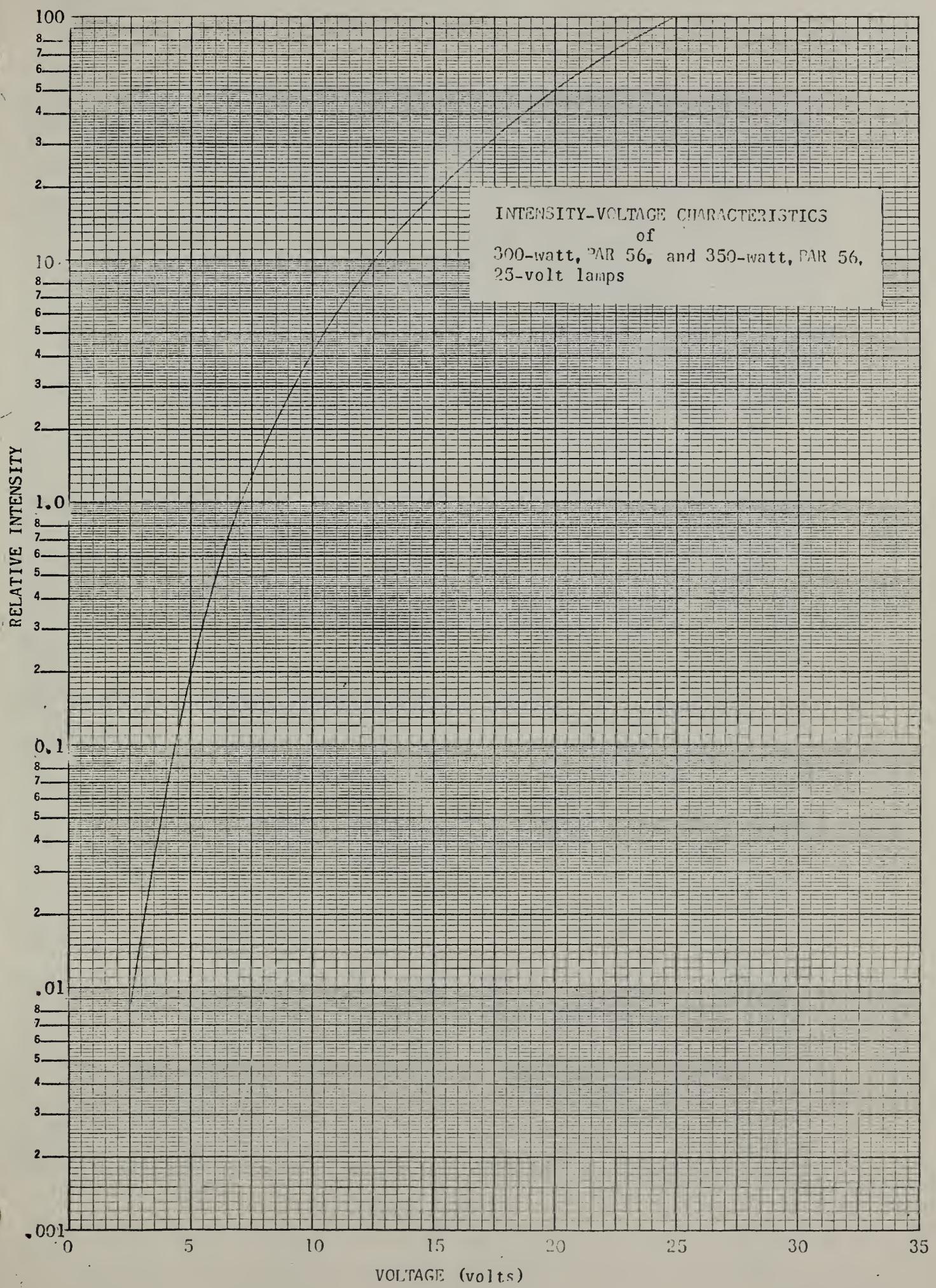
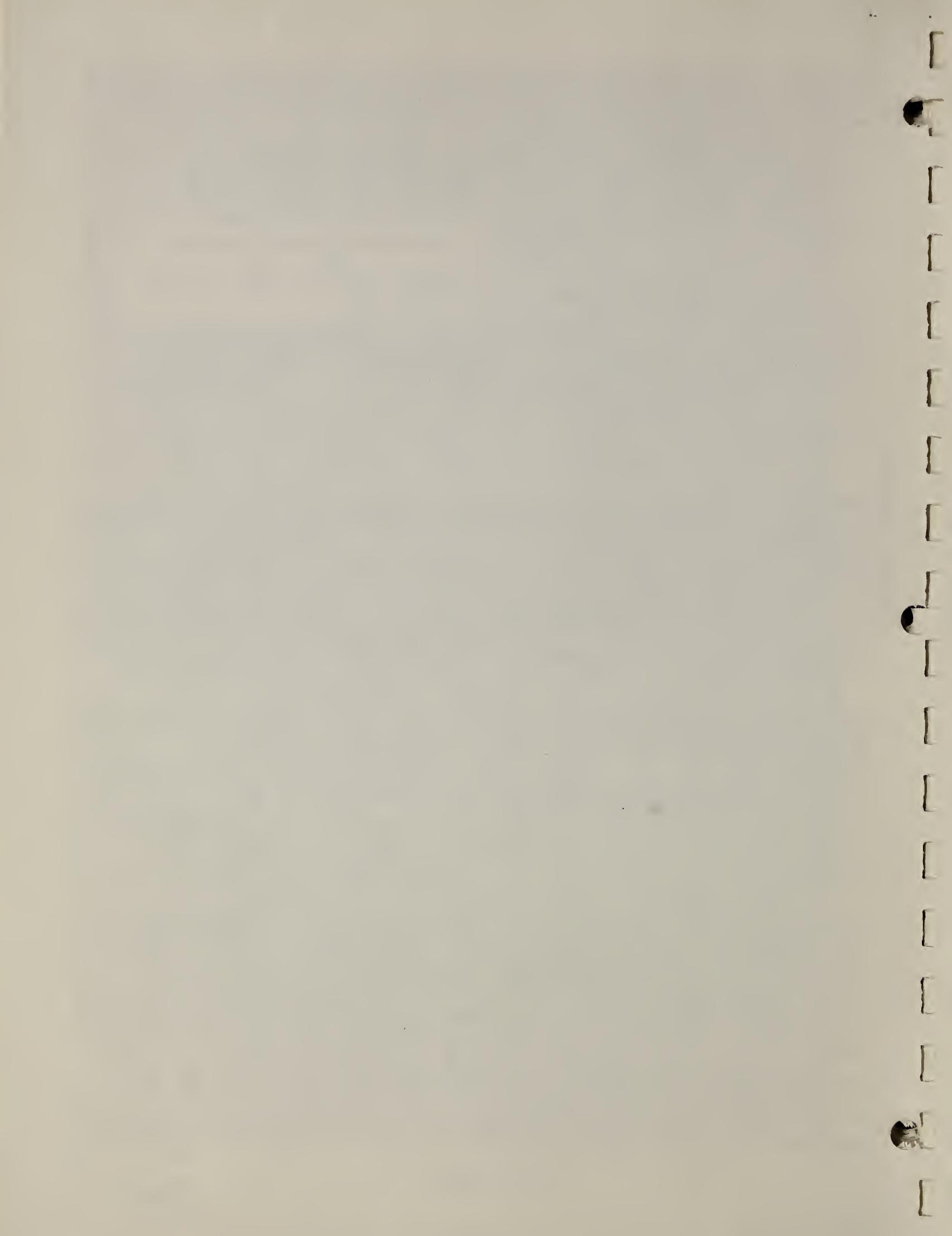


Figure 19b



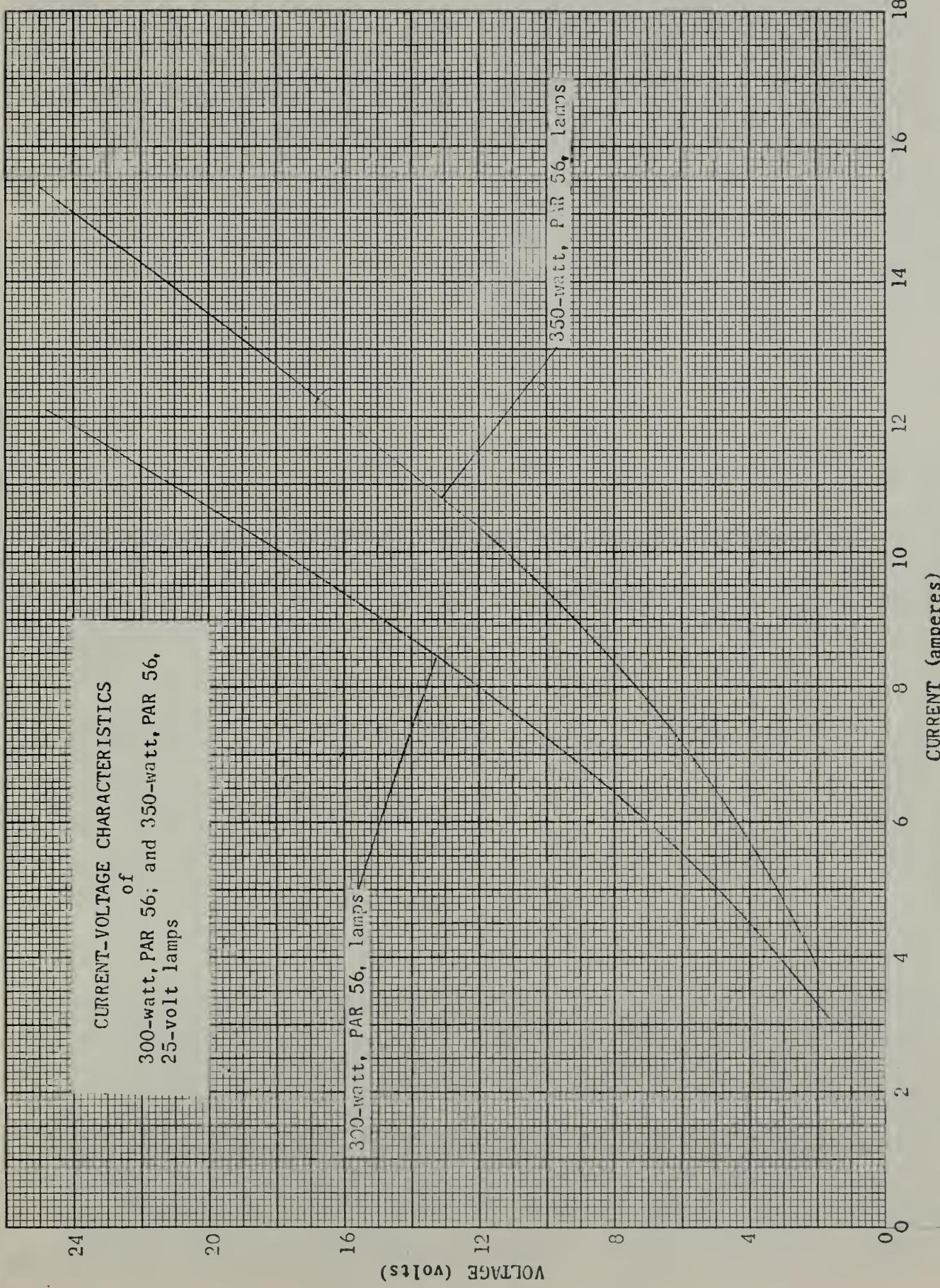
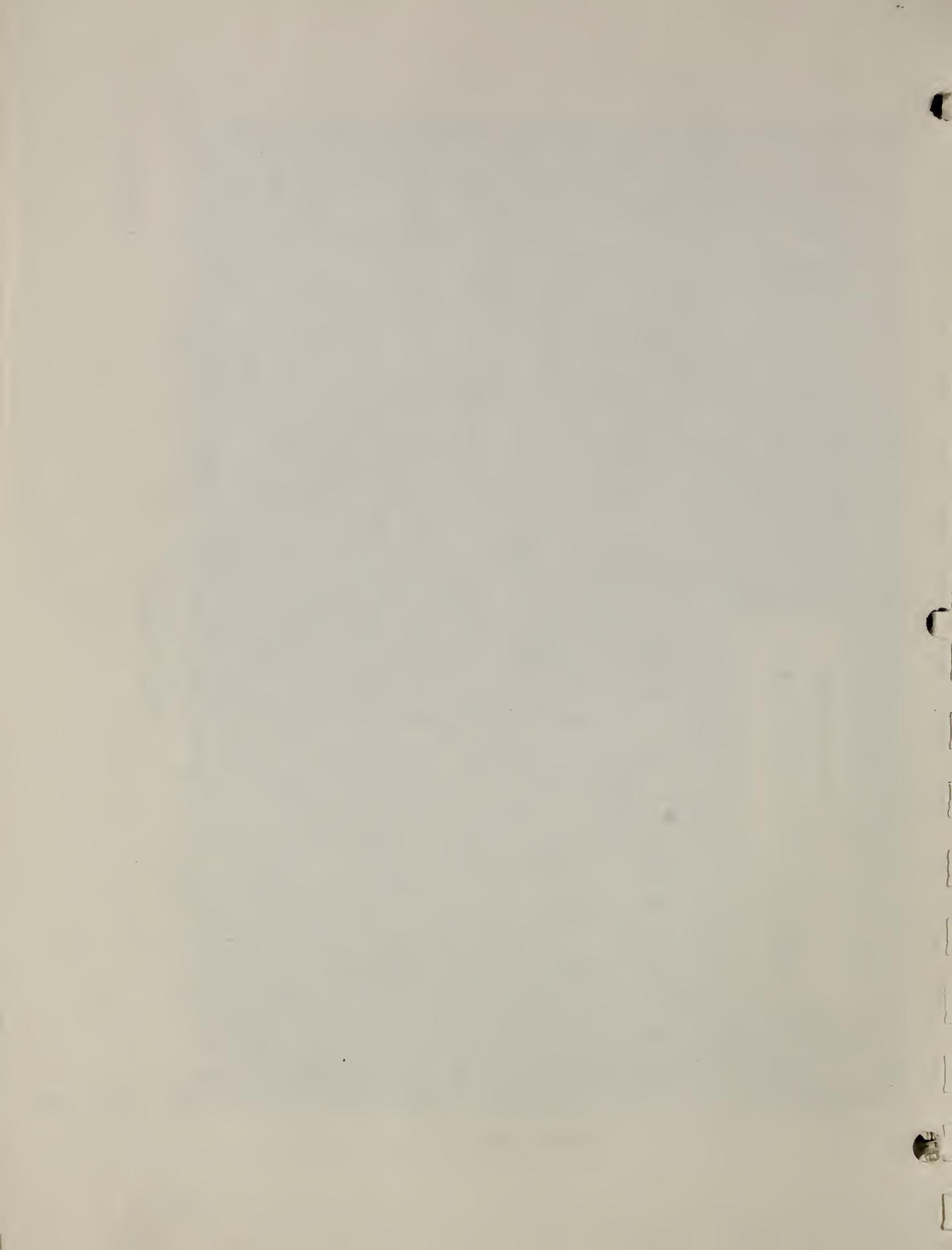


Figure 19c



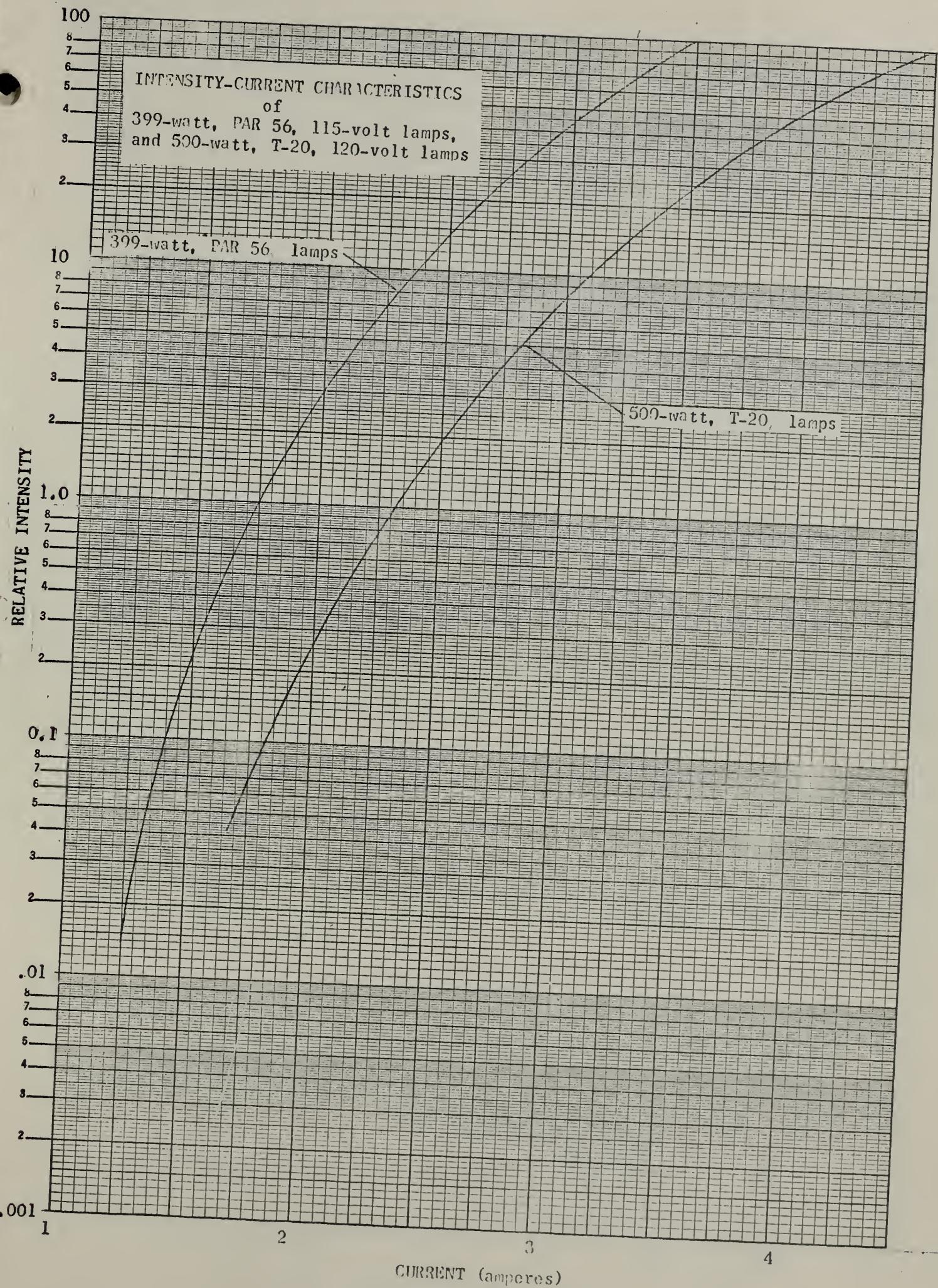
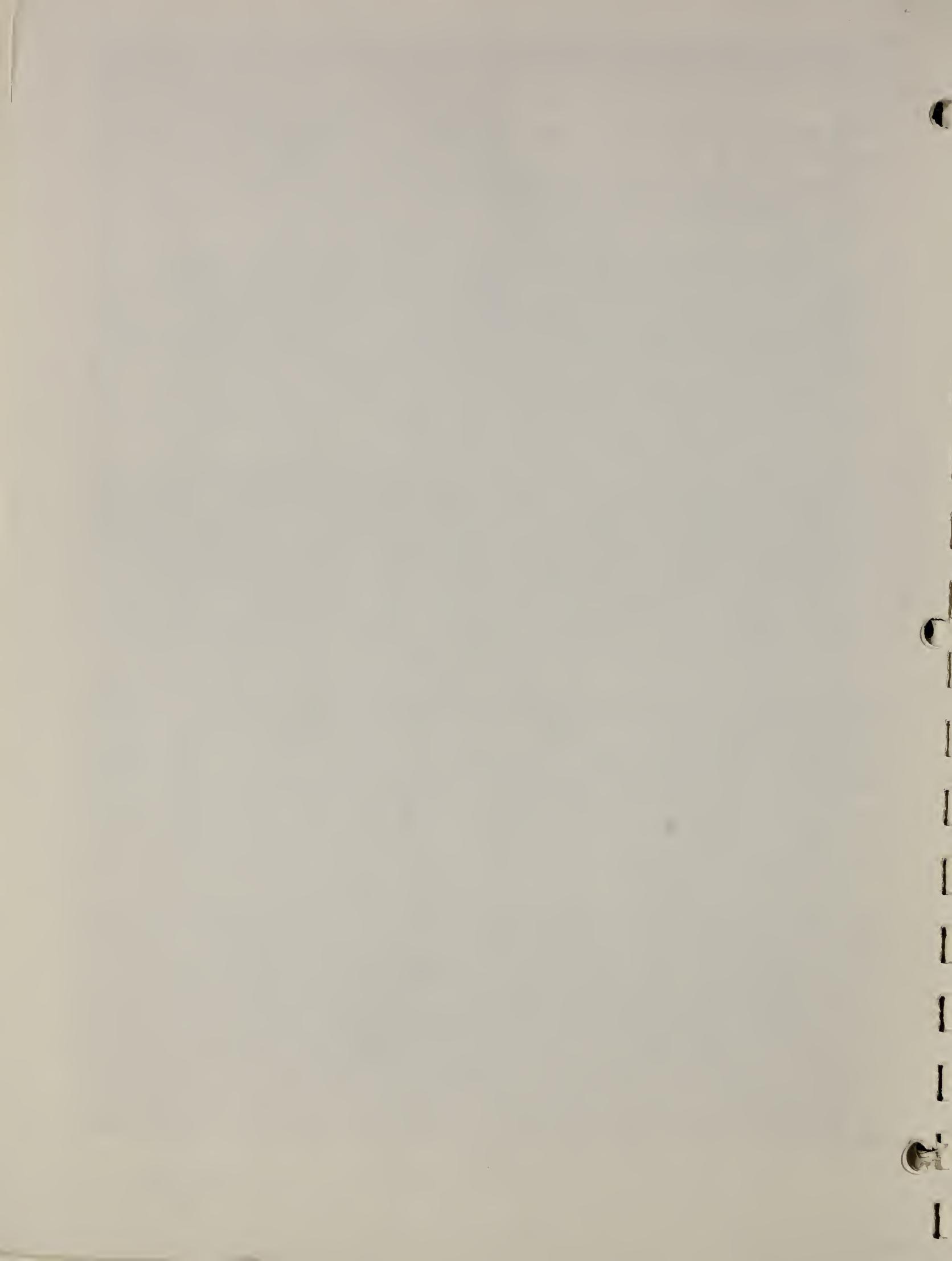


Figure 20a



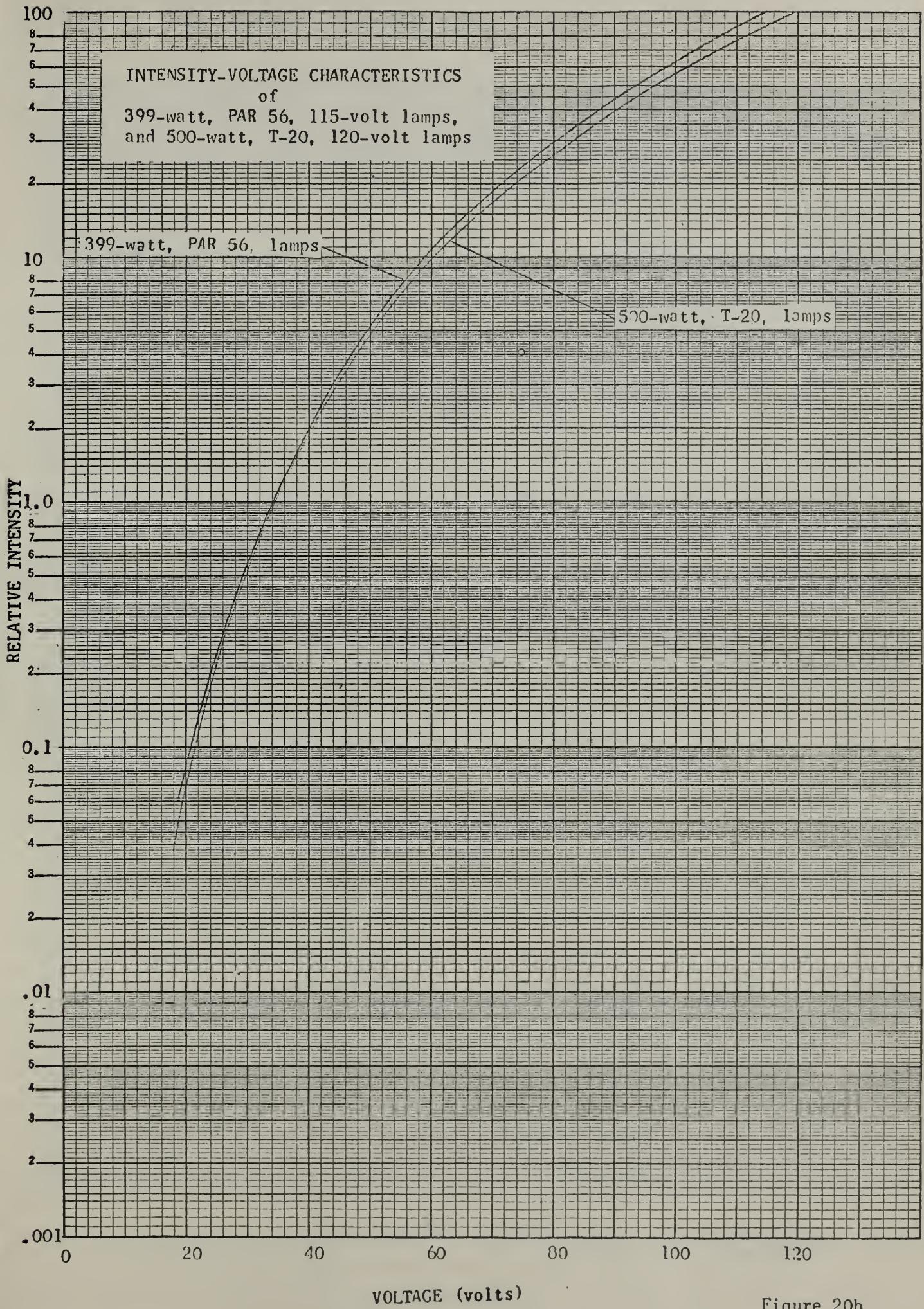


Figure 20b

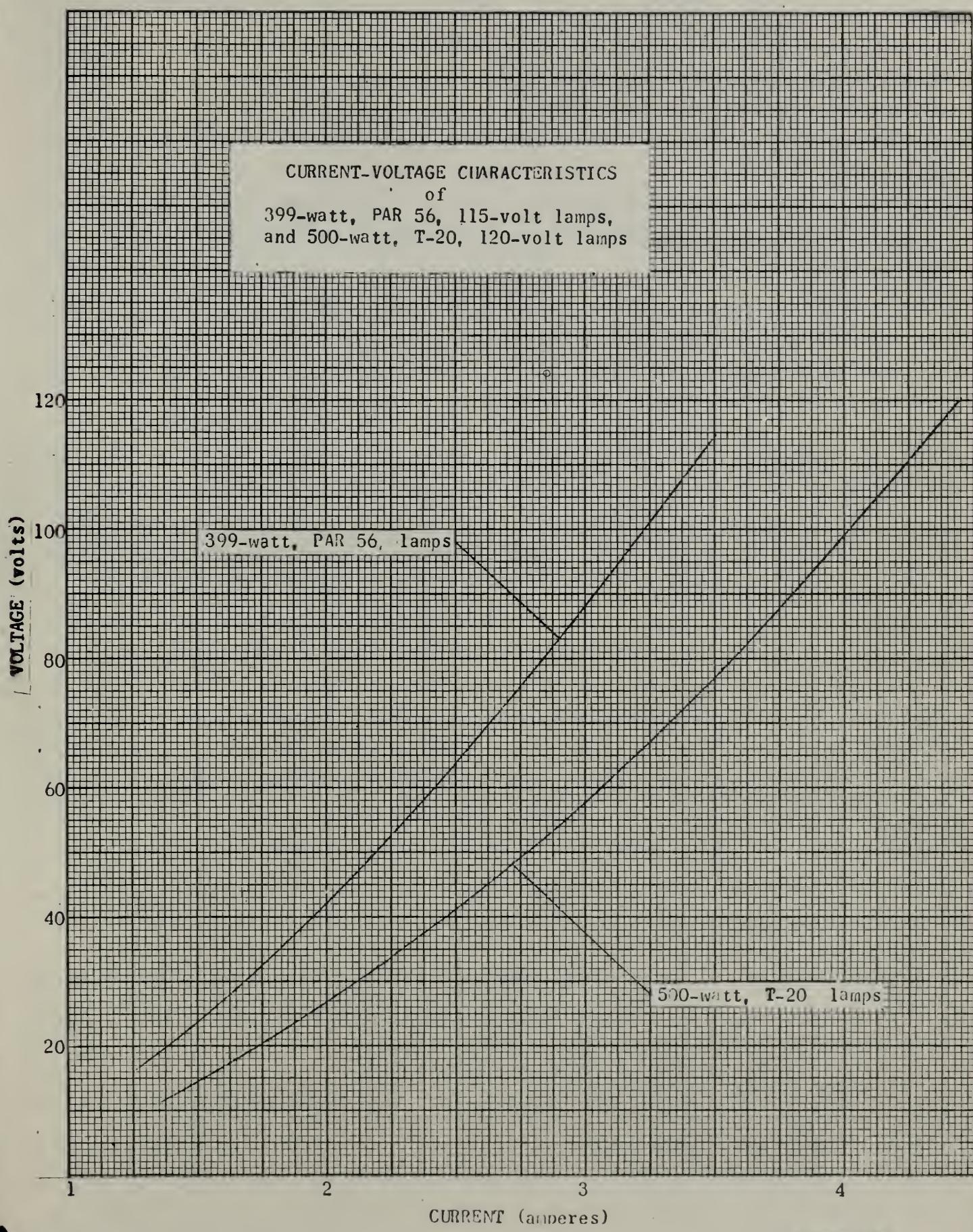
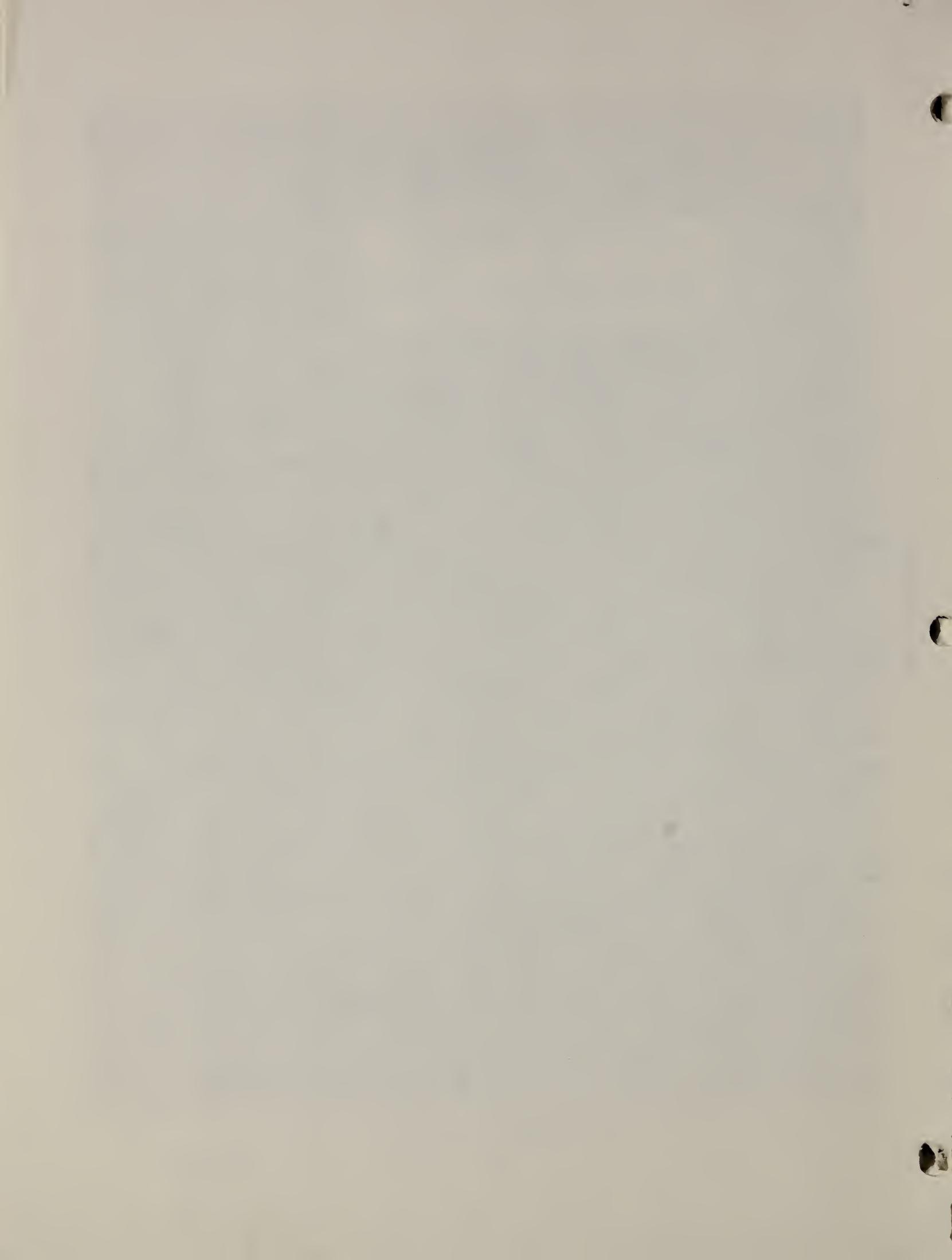


Figure 20c



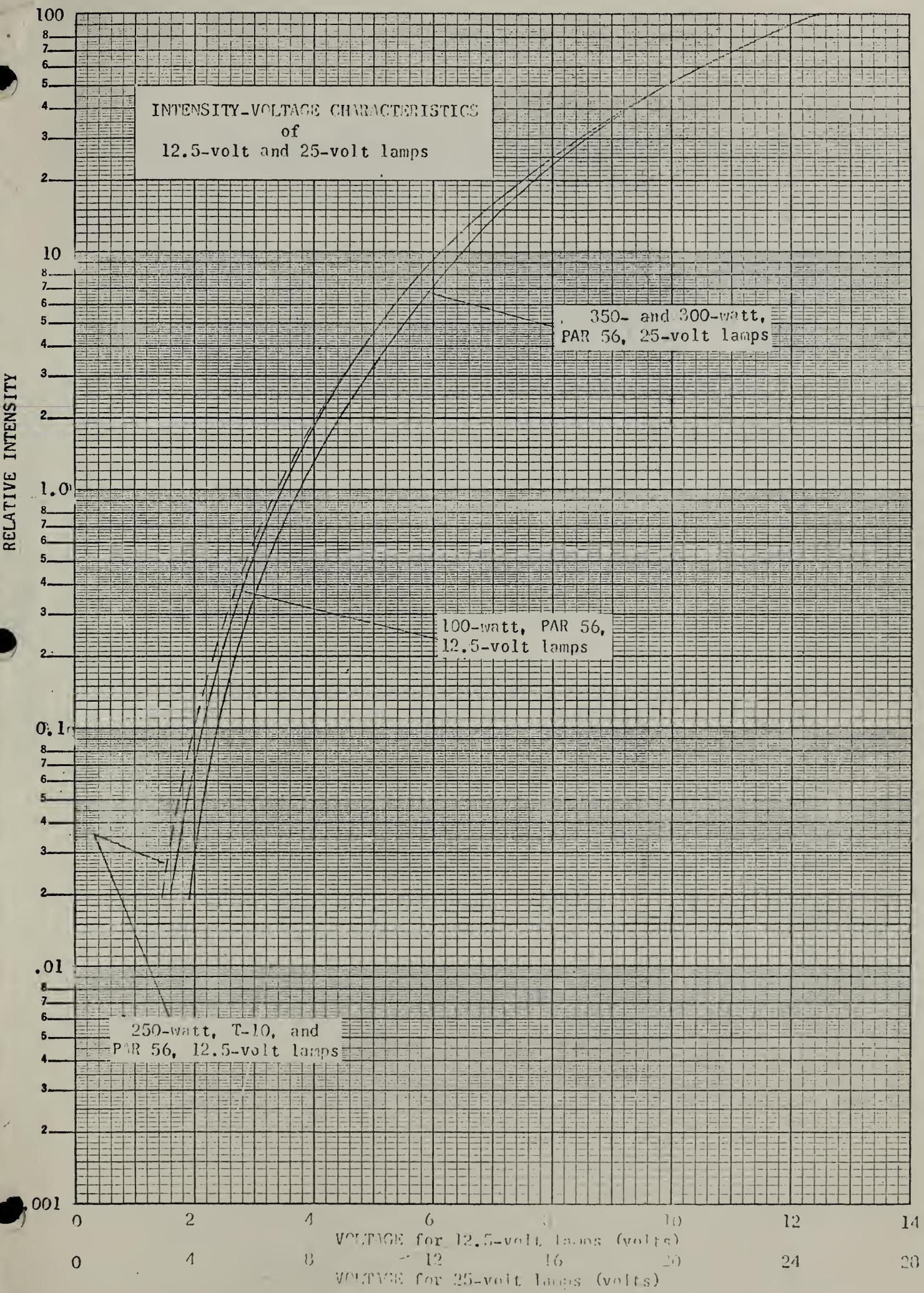
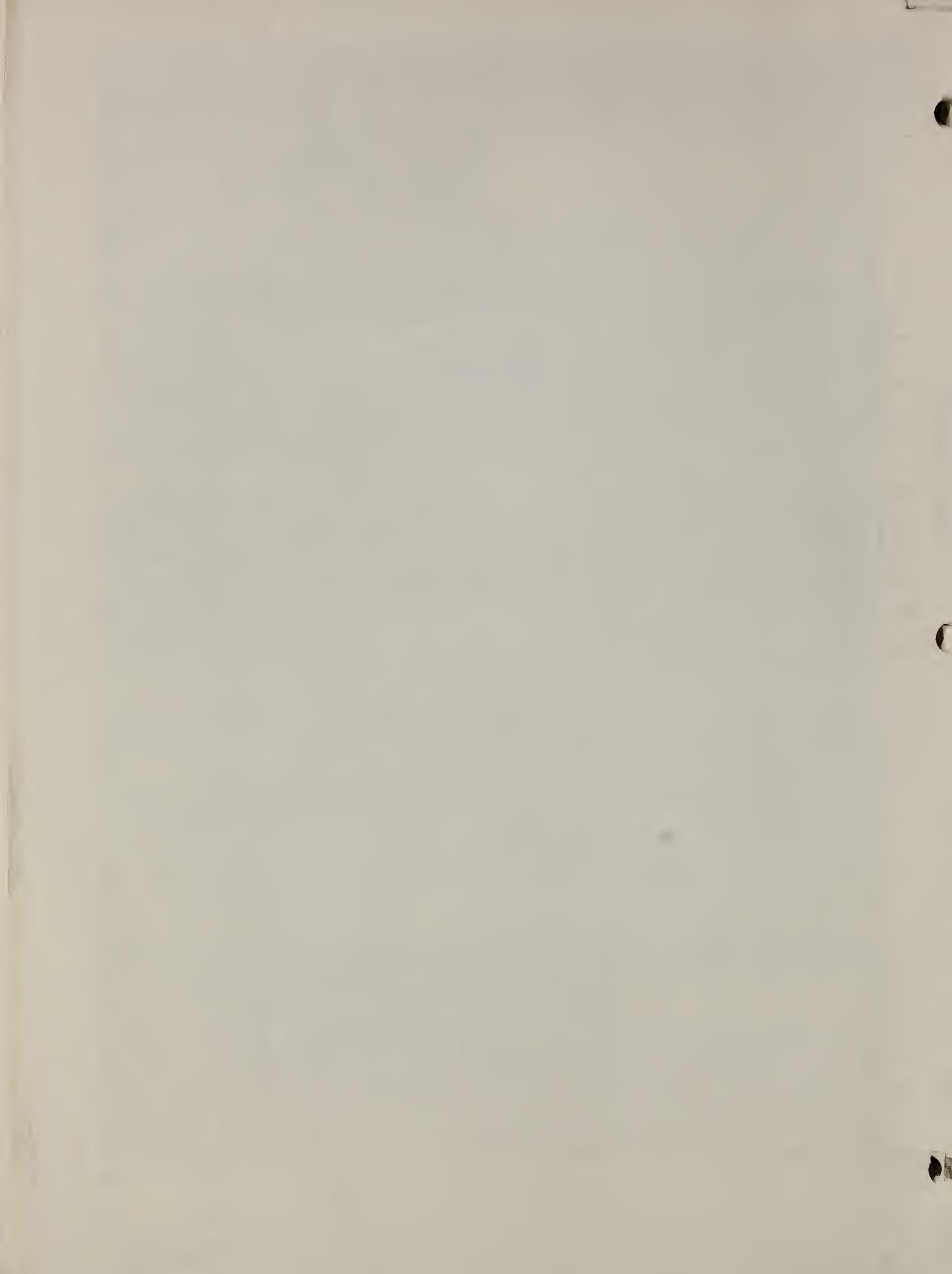


Figure 21



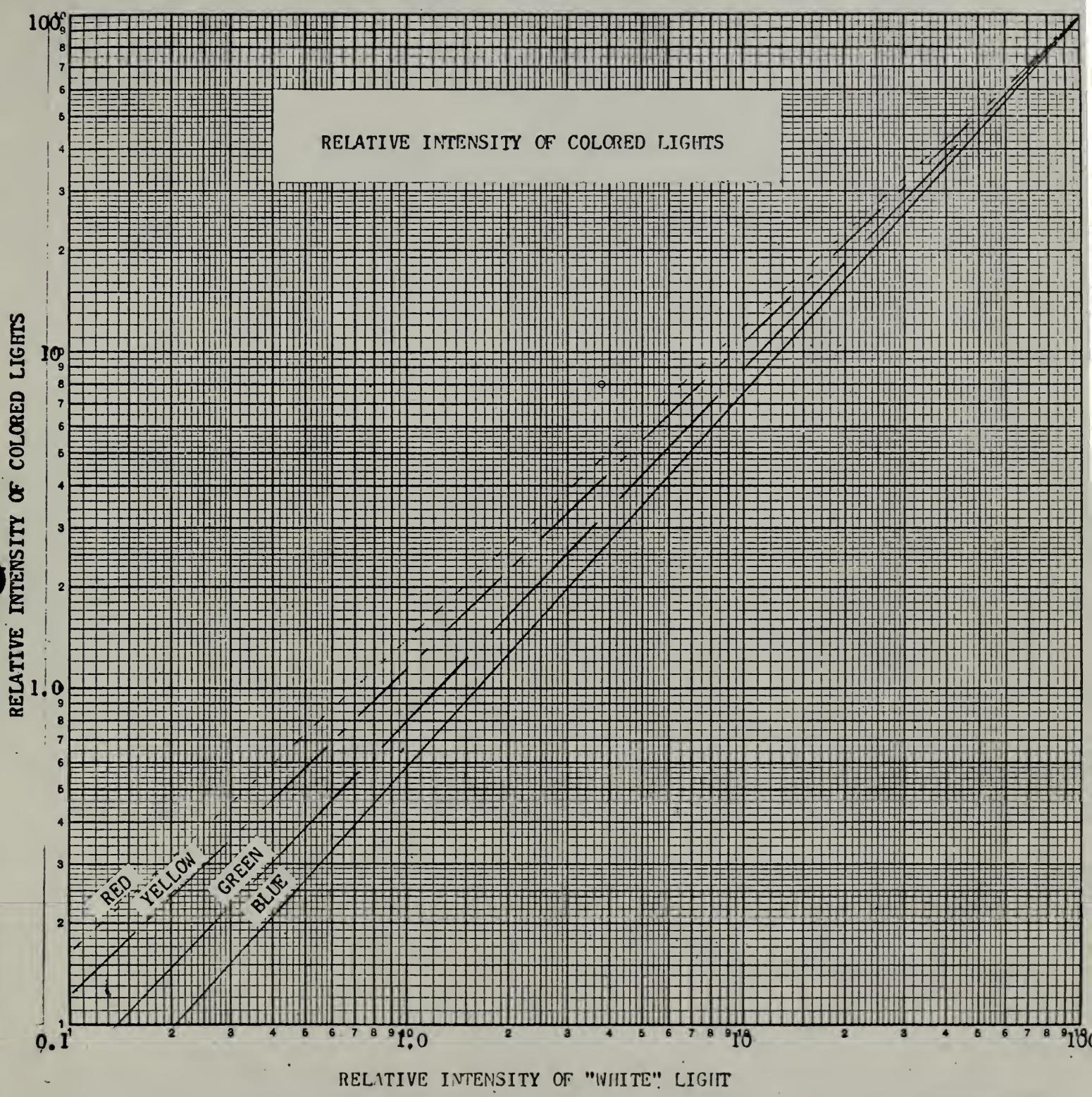


Figure 22

